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MIXING-LAYER ANALYSIS ROUTINE AND TRANSPORT/DIFFUSION APPLICATIONS--ETC(U)

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RESEARCH AND DEVELOPMENT TECHNICAL REPORT

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MIXING-LAYER ANALYSIS ROUTINE AND TRANSPORT/  
DIFFUSION APPLICATION ROUTINE  
FOR EPAMS

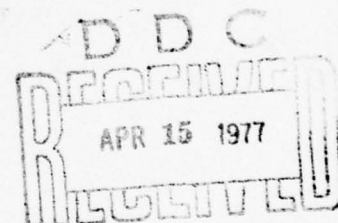
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March 1977

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20. ABSTRACT (Continue on reverse side if necessary and identify by block number) This report describes the development of two subelements of the U. S. Army Experimental Prototype Automatic Meteorological System (EPAMS). One of the subelements is a diagnostic routine (computer program) for the automatic calculation of the mixing depth, as well as the wind velocity and other meteorological parameters in the surface mixing layer, for a mesoscale calculation grid in complex terrain. The output from this routine is used with the second subelement--a transport/diffusion application routine--to calculate concentration/dosage fields		

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## 20. Abstract (cont)

produced by pollutant emissions from selected sources located within the calculation grid. A two-layer shallow-fluid numerical model is used in the diagnostic routine to calculate the mesoscale wind field. The concentration/dosage fields calculated by the transport/diffusion application routine are obtained by solving generalized dispersion models for both continuous and instantaneous sources. In addition to descriptions of the modeling techniques, calculation procedures and computer program operations, example solutions for several case studies at White Sands Missile Range are also presented.

## FOREWORD

This final report is submitted to the Atmospheric Sciences Laboratory, White Sands Missile Range in fulfillment of requirements under Contract No. DAAD07-76-C-0023.

The H. E. Cramer Company, Inc. is indebted to Mr. William Ohmstede, Atmospheric Sciences Laboratory, for the technical guidance and useful suggestions he provided in the development of the computer program routines described in this report.

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## SECTION 1

### INTRODUCTION

#### 1.1 BACKGROUND

The Experimental Prototype Automatic Meteorological System (EPAMS) is part of an overall development program of the U. S. Army to provide a centralized data system for use in supporting future operations of the Field Army. Under the EPAMS development program, the Atmospheric Sciences Laboratory, White Sands Missile Range (WSMR) required implementation of an automated procedure for estimating the cloud trajectory and dispersion characteristics downwind from sources of contaminate material released at any arbitrary point within the atmospheric mixing layer. WSMR wished to implement these automated procedures using available technical approaches to prevent undue delays in the EPAMS development schedule.

The technical problem of estimating wind fields over complex terrain has been under continued investigation at WSMR. Because of the computer space/time criteria established for EPAMS, the model selected for use in EPAMS had to be relatively simple in concept. The computer algorithms developed by Tingle and Bjorklund (1973) for WSMR's use in predicting wind fields in complex terrain were ideally suited for this purpose. The algorithms, based on the shallow-fluid equations of oceanography, have simple input requirements, reach stable solutions in a relatively few iterations and thus conserve computation time, and have been shown to produce wind field estimates agreeing with observed estimates in complex terrain surrounding WSMR and Dugway Proving Ground, Utah. Similar criteria applied to the selection of dispersion models for use in EPAMS. The generalized dispersion models developed under previous Government contracts for predicting concentration, dosage and deposition downwind from nearly-instantaneous and continuous volume sources (Cramer, *et al.*, 1972; Dumbauld, *et al.*, 1970, 1973) had been validated for use in conjunction with military activities. These computerized models were

developed with the intention of providing the U. S. Army with a universally adaptable means of calculating dispersion characteristics for all types of terrain, meteorological conditions and types of sources.

Thus, the technical data base requisite for development of an automated procedure for predicting cloud trajectories and dispersion characteristics in complex terrain existed. The principle technical objectives of the work described below were to utilize the existing technical data base in the:

- Development of a diagnostic/prognostic analysis routine for evaluating the depth and wind velocity of the atmospheric mixing layer in association with complex terrain
- Development of a diagnostic/prognostic application routine for evaluating the transport and diffusion of contaminant material released from a source within the mixing layer

and incorporation of these routines into EPAMS as subordinate elements.

Figure 1-1 is a simplified schematic diagram of the EPAMS functional elements illustrating the interface of the Analysis and Application Routines or Phases with EPAMS. The Applications Phase is called by the EPAMS Executive as a result of a request for information routed through a Message Management Routine. The Applications Phase extracts the necessary meteorological and source information from the Data Base Management Routine and calculates the transport and diffusion of contaminant material released to the atmosphere. The solution is output to the Data Base, where it is made available to the EPAMS Executive for forming a response to the information request. The Analysis Phase is called by the EPAMS Executive as a result of a standing request for a routine analysis of meteorological conditions in the

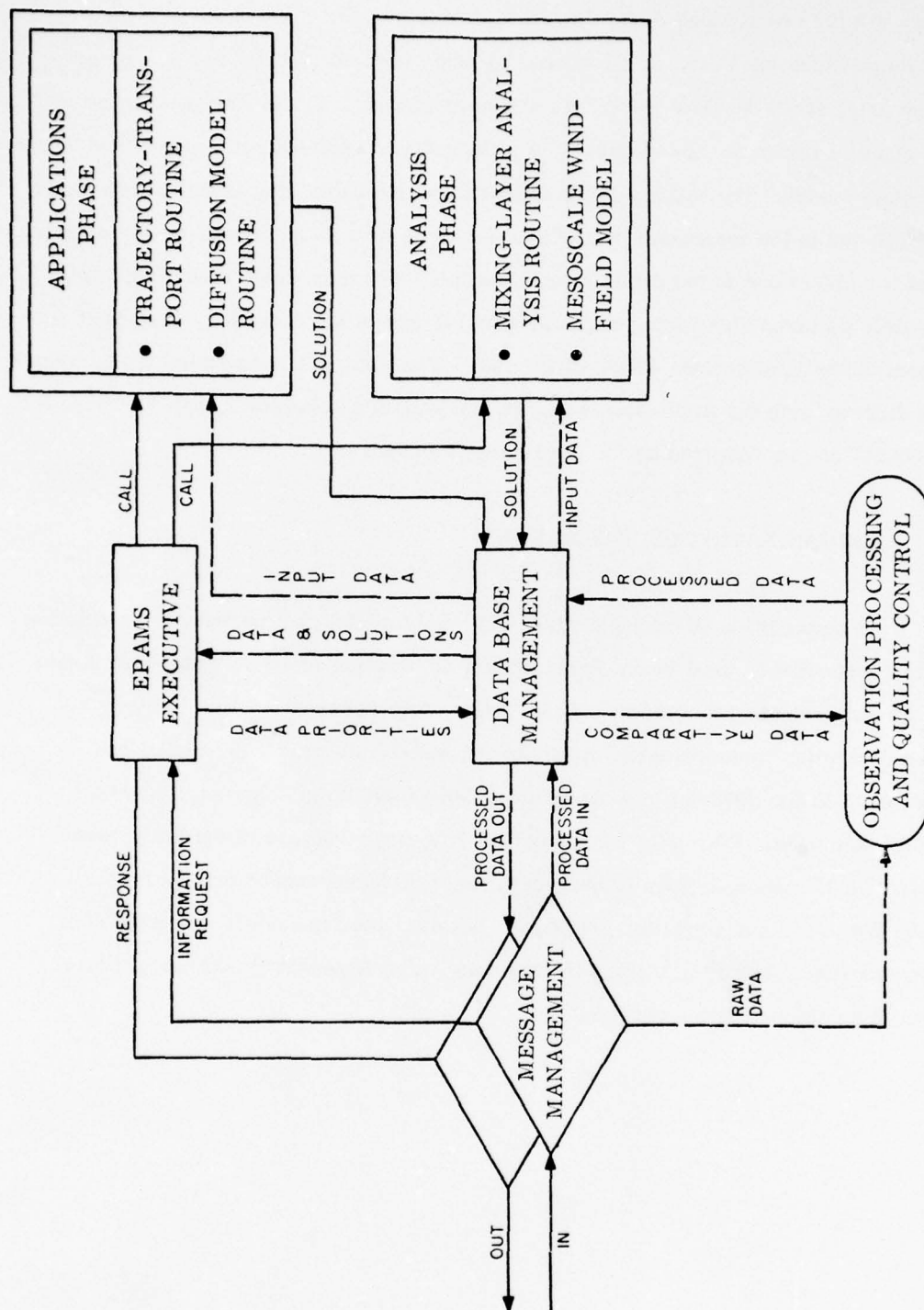


Figure 1-1. Schematic Diagram of the EPAMS Functional Elements.



surface mixing layer. The Analysis Phase extracts upper-air and surface meteorological data, including U. S. A. F. Global Weather Central (GWC) "fine mesh" prediction data, from the Data Base. As shown in Figure 1-1, the Analysis Phase is comprised of two major subelements, a mixing-layer analysis routine and mesoscale wind-field model. The mixing-layer analysis routine calculates initialization parameters for use in the mesoscale wind-field model as well as additional meteorological inputs for direct use in the Applications Routine. The mesoscale model calculates wind-field patterns and mixing-depth heights for use in the trajectory-transport subelement of the Applications Phase of EPAMS. The Analysis Phase does not communicate directly with the Applications Phase, but supplies solutions to the data base for subsequent use as required by the Applications Phase.

## 1.2 ORGANIZATION OF THE REPORT

A description of the mesoscale wind-field model and the transport diffusion models respectively used in the Analysis and Application Phases is provided in Section 2 below. Section 3 contains a description of procedures used in the Analysis Phase to develop meteorological inputs to the mesoscale wind-field model and for direct input to the diffusion models from meteorological data extracted from the EPAMS data base. Details of the computer program structure of the Analysis and Application Phases are given in Section 4. Section 5 contains example cases illustrating the use of the computer program. Detailed user instructions for the computer program routines are given in Appendix A and Appendix B contains a listing of the computer program routines.



## SECTION 2

### MESOSCALE WIND-FIELD AND TRANSPORT/DIFFUSION MODELS

#### 2.1 MESOSCALE WIND-FIELD MODEL

The Analysis Phase developed for EPAMS relies on a numerical modeling technique developed for WSMR by Tingle and Bjorklund (1973) to calculate details of the mesoscale wind-field and depth of the surface-mixing layer over complex terrain. The computer algorithm, based on the shallow-fluid equations of oceanography, describes the motion of fluid in two dimensions by the expressions:

$$\frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} + g' \frac{\partial}{\partial x} (H_m + z_T) = 0 \quad (2-1)$$

$$\frac{\partial v}{\partial t} + u \frac{\partial v}{\partial x} + v \frac{\partial v}{\partial y} + g' \frac{\partial}{\partial y} (H_m + z_T) = 0 \quad (2-2)$$

$$\frac{\partial H_m}{\partial t} + \frac{\partial (uH_m)}{\partial x} + \frac{\partial (vH_m)}{\partial y} = 0 \quad (2-3)$$

where

$u, v$  =  $x, y$  components of the fluid velocity in the layer next to the terrain

$H_m$  = depth of the surface mixing-layer

$z_T$  = height of the terrain

$g'$  = reduced acceleration of gravity

$$= g \left( 1 - \frac{\rho_t}{\rho_o} \right)$$

$g$  = acceleration of gravity

$\rho_o$  = density of fluid in the surface mixing layer

$\rho_t$  = density of fluid in the deep passive layer above the fluid in the surface mixing-layer

Thus the equations can be used to describe mesoscale wind-patterns over complex terrain when the atmosphere above the terrain can be distinctively divided into at least two layers of air of different densities. Such an atmospheric condition arises when the mixing layer above the terrain is capped by an elevated inversion. The warmer upper layer interacts with the cooler lower layer only in that its lesser density reduces the speed of gravity waves introduced into the lower layer. In the algorithm, Tingle and Bjorklund have written Equations (2-1), (2-2) and (2-3) in their momentum form. Mesoscale wind patterns are generated by impulsively accelerating the momentum in the lower layer to a constant value and, after a empirically determined model time (see Section 4), the flow in the region of interest is assumed to be stabilized (steady state).

The computer algorithm utilizes an explicit method of the Lax-Wendroff type of finite differencing technique using nine grid points and one time level in combination with a nine-point low-pass filter. The differencing scheme is designed such that the finite differencing forms are centered to preserve high-order accuracy. The grid arrangement for this centering scheme and finite differencing form of the equations are fully described in the report by Tingle and Bjorklund (1973). As noted above, high-frequency oscillations generated in critical flow situations near regions where hydraulic jumps occur are removed by a filtering technique. The filtering technique used in the algorithm is based on a suggestion from Shapiro (1970) and has the advantage that its smoothing effect is easily determined from its response

function. In the Analysis Phase, the filter is applied every seventh time step. It is well known that the length of the time step  $\Delta t$  used in obtaining the solution also effects the stability of the finite difference solution. The time step is altered automatically in this algorithm in accordance with the expression

$$\Delta t = \frac{\lambda}{\sqrt{2}} \frac{\Delta x_{\min}}{\left[ \sqrt{u^2 + v^2} + \sqrt{g H_m} \right]_{\max}} \quad (2-4)$$

where the stability parameter  $\lambda$  is dependent on the grid spacing  $\Delta x$  and varies between zero and one. For the present application using a minimum spacing ( $\Delta x_{\min}$ ) of 5 kilometers, the stability parameter has been set equal to 0.4. Because the entire solution grid must be searched to determine the maximum wave speed in the denominator of Equation (2-4), the value of  $\Delta t$  is calculated every second time step rather than every time step to save computation time.

A sensitivity analysis of the two-layer mesoscale wind field model currently in progress under separate contract with U. S. Army Dugway Proving Ground has indicated model instability can frequently occur in localized terrain regions where the inversion height  $H_m$  is initialized, or becomes adjusted by the model, to altitudes within a few tens of meters of the higher terrain elevations. The momentum conservation properties of the computational scheme are such that wind velocities in these localized regions may become unreasonably large as the layer thickness approaches a minimum value. In order to prevent this type of solution instability, the computer algorithm has been redesigned so that the  $u$  and  $v$  components of the solution at any given time step are automatically set to zero and the thickness raised to a minimum depth of 30 meters if the calculated depth for a grid point is less than 30 meters. Limited experience in the application of this feature

of the mesoscale model indicates that computational stability is preserved without undue loss of momentum over the entire grid and with the result that wind fields in the immediate vicinity of higher elevations under these conditions appear to be reasonable (see Example in Section 5).

The computerized algorithm uses an expanding grid in the boundary area beyond the terrain region of interest to damp outgoing waves and eliminate incoming waves based on the technique suggested by Lavoie (1972). Grid points in the boundary region are spaced at 10, 20, 40, 80 and 160 kilometers from all four sides of the interior grid. The terrain height at all points in the boundary region are set equal to the minimum elevation within the interior grid. Since the shallow-water equations are written in their momentum form, the initial momentum is set equal to the momentum used in initializing parameters in the interior grid.

Readers interested in the form of the finite-differenced equations and other details on which the mesoscale wind-field computer algorithm is based are referred to the paper by Tingle and Bjorklund (1973).

## 2.2 TRANSPORT-DIFFUSION MODELS

### 2.2.1 Trajectory/Transport Routine

The Trajectory-Transport Routine incorporated in the Applications Phase of EPAMS shown in Figure 1-1 is designed to calculate cloud trajectories and mean-layer winds and mixing-layer depths at fixed intervals along the trajectories using the output from the mesoscale wind-field model described above. The trajectory of a cloud released at any point within the model solution grid is calculated using a simple Euler predictor-corrector scheme and nine-point interpolation procedure. The computer program uses wind vector data from the mesoscale wind-field model solution at nine grid points surrounding the source (point of release) and,



through the interpolation procedure, estimates the  $u$  and  $v$  components of the wind at the point of release. The first approximation to the first point on the trajectory curve is then determined by resolving the components and placing a point at a fixed interval along the resultant vector. The fixed distance interval is set at one-tenth the grid spacing used in the mesoscale wind-field solution matrix so that in the present program a fixed interval of 500 meters is used. Wind velocity components at this point are again estimated from the nine-point interpolation procedure. These new  $u$  and  $v$  components are then averaged with the previously determined components at the starting point. The final estimate of the first point on the trajectory is then calculated by resolving the averaged components and moving a fixed interval along the resultant vector. This final estimate of the first point on the trajectory is then treated in the same manner as the initial starting point (source) and the interpolation and iteration scheme repeated to find the second point on the trajectory. This procedure is repeated until the trajectory passes outside the grid area containing wind-vector data or the number of iterations exceeds a predetermined limit.

The interpolation method is based on an evaluation of a truncated two-dimensional Taylor's expansion formula (Carnahan, Luther and Wilkes, 1969, p. 430) given by

$$f(x,y) \cong f_{i,j} + hf_x + kf_y + \frac{h^2}{2} f_{xx} + hkf_{xy} + \frac{k^2}{2} f_{yy} \quad (2-4)$$

where

$$h = x - x_i$$

$$k = y - y_j$$



and  $f_{i,j}$  is either the u or v component at  $x_i, y_j$ , the nearest grid point to the point of interpolation  $(x, y)$ . The partial derivatives  $f_x, f_y, f_{xx}, f_{xy}$  and  $f_{yy}$  are estimated by divided differences.

The depth of the mixing layer at fixed intervals along the trajectory is also interpolated from data provided by the mesoscale wind-field model using a four-point bivariate interpolation formula given by

$$\begin{aligned} H_m(x, y) = & (1 - p)(1 - q) H_{m_{i,j}} + p(1 - q) H_{m_{i+1,j}} \\ & + q(1 - p) H_{m_{i,j+1}} + pq H_{m_{i+1,j+1}} \end{aligned} \quad (2-5)$$

where

$$\begin{aligned} p &= (x - x_i) / (x_{i+1} - x_i) \\ q &= (y - y_j) / (y_{j+1} - y_j) \end{aligned}$$

and  $H_{m_{i,j}}$ ,  $H_{m_{i+1,j}}$ ,  $H_{m_{i,j+1}}$ , and  $H_{m_{i+1,j+1}}$  are the mixing layer depths at the four surrounding grid points.

### 2.2.2 Diffusion Models Routine

The Diffusion Models Routine shown in Figure 1-1 as an element of the Applications Phase of EPAMS is comprised of volume source diffusion models for instantaneous and continuous sources and models for use in predicting the buoyant rise of plumes from continuous sources. These models are used in the Diffusion Models Routine to estimate isopleths of dosage and concentration, with or without

depletion due to simple decay, gravitational settling and precipitation scavenging, along the cloud trajectory determined by application of the Trajectory-Transport Routine.

#### Instantaneous Volume-Source Model

The volume-source model for use in EPAMS is similar to the models for instantaneous sources described by Cramer, et al. (1972) and by Dumbauld, Bjorklund and Bowers (1973). The concentration for an instantaneous volume-source can be expressed as the product of four terms:

$$\chi_n = \{\text{Peak Term}\} \{\text{Lateral Term}\} \{\text{Vertical Term}\} \{\text{Depletion Term}\} \quad (2-6)$$

The Peak Term describes the concentration at the cloud centerline and is given by the expression

$$\text{Peak Term} = \frac{Q}{(2\pi)^{3/2} \sigma_{xn} \sigma_{yn} \sigma_{zn}} \quad (2-7)$$

where

- $Q$  = total source strength
- $\sigma_{xn}$  = standard deviation of the concentration distribution in the alongwind direction at the  $n^{\text{th}}$  distance along the cloud trajectory
- $\sigma_{yn}$  = standard deviation of the concentration distribution in the crosswind direction at the  $n^{\text{th}}$  distance along the cloud trajectory
- $\sigma_{zn}$  = standard deviation of the concentration distribution in the vertical at the  $n^{\text{th}}$  distance along the cloud trajectory

The Vertical Term describes the vertical distribution of material at the  $n^{\text{th}}$  distance along the cloud trajectory as modified by reflections of material at the top of the surface mixing layer and at the earth's surface and by gravitational settling of particulates

$$\begin{aligned}
 \text{Vertical Term} = & \sum_{a=0}^{\infty} \left\{ r^a \exp \left[ -\frac{1}{2} \left( \frac{2a H_{m,n} - H' + z + V_s \sum_{n=1}^N \frac{\Delta x_n}{\bar{u}_n} \right)^2}{\sigma_{z,n}} \right] \right. \\
 & + r^{a+1} \exp \left[ -\frac{1}{2} \left( \frac{2a H_{m,n} + H' + z - V_s \sum_{n=1}^N \frac{\Delta x_n}{\bar{u}_n} \right)^2}{\sigma_{z,n}} \right] \left. \right\} \\
 & + \sum_{a=1}^{\infty} \left\{ r^a \exp \left[ -\frac{1}{2} \left( \frac{2a H_{m,n} + H' - z - V_s \sum_{n=1}^N \frac{\Delta x_n}{\bar{u}_n} \right)^2}{\sigma_{z,n}} \right] \right. \\
 & + r^{a-1} \exp \left[ -\frac{1}{2} \left( \frac{2a H_{m,n} - H' - z + V_s \sum_{n=1}^N \frac{\Delta x_n}{\bar{u}_n} \right)^2}{\sigma_{z,n}} \right] \left. \right\} \quad (2-8)
 \end{aligned}$$

where, for convenience in writing the Vertical Term,  $0^0$  (zero to the zeroeth power) is set equal to unity and

- $H'$  = effective release height (see Equation (2-20))
- $z$  = calculation height
- $H_{m,n}$  = mixing layer depth from mesoscale model for  $n^{\text{th}}$  distance along the trajectory
- $r$  = fraction of material reflected at the surface (1 for complete reflection and 0 for no reflection)

- $V_s$  = settling velocity for material in a given size category  
 $\Delta x_n$  = incremental distance along the cloud trajectory  
 $\bar{u}_n$  = mean wind speed in the layer containing the cloud at the  $n^{\text{th}}$  point along the trajectory (see Equation (2-17) below)

The Lateral Term is given by

$$\text{Lateral Term} = \exp \left[ -\frac{1}{2} \left( \frac{y}{\sigma_{yn}} \right)^2 \right] \quad (2-9)$$

where

$y$  = crosswind distance from the centerline of the cloud trajectory

The Depletion Term refers to the loss of material by simple decay processes and by precipitation scavenging. The form of the Depletion Term for each of these processes is:

$$\text{(Decay)} \quad \exp \left[ -k \sum_{n=1}^N \frac{\Delta x_n}{\bar{u}_n} \right] \quad (2-10)$$

$$\text{(Precipitation Scavenging)} \quad \exp \left[ -\Lambda \sum_{n=1}^N \frac{\Delta x_n}{\bar{u}_n} \right] \quad (2-11)$$



where

$k$  = decay coefficient or fraction of material lost per unit time

$\Lambda$  = washout coefficient or fraction of material removed by scavenging per unit time

The subset of equations describing the standard deviations of the alongwind  $\sigma_{xn}$ , crosswind  $\sigma_{yn}$  and vertical  $\sigma_{zn}$  concentration distributions is:

$$\sigma_{xn} = \frac{L \{x_n\}}{4.3} + \sigma_{x(n-1)} = \frac{0.6 \Delta \bar{u}_n}{4.3 \bar{u}_n} \Delta x_n + \sigma_{x(n-1)} \quad (2-12)$$

where

$L \{x_n\}$  = alongwind dimension of the cloud

$\Delta \bar{u}_n$  = wind speed shear at the  $n^{\text{th}}$  point along the trajectory

$$= \frac{\bar{u}_{5,n}}{5^{p_n}} \left( z_{T,n}^{p_n} - z_{B,n}^{p_n} \right) \quad (2-13)$$

$\bar{u}_{5,n}$  = wind speed at a height of five meters at the  $n^{\text{th}}$  point along the trajectory

$p_n$  = wind power-law coefficient at the  $n^{\text{th}}$  point along the trajectory

$z_{T,n}$  = top of the cloud at the  $n^{\text{th}}$  point

$$= \begin{cases} H' + 2.15 \sigma_{zn} ; & z_{T,n} < H_{m,n} \\ H_{m,n} ; & z_{T,n} \geq H_{mn} \end{cases} \quad (2-14)$$

$z_{B,n}$  = base of the cloud at the  $n^{\text{th}}$  point



$$= \begin{cases} H' - 2.15 \sigma_{zn} & ; z_{B,n} \geq 0 \\ 0 & ; z_{B,n} \leq 0 \end{cases} \quad (2-15)$$

$$\bar{u}_{5,n} = \frac{\bar{u}_n (H_{m,n} - 5) 5^{p_n} (1 + p_n)}{H_{m,n}^{(1+p_n)} - 5^{(1+p_n)}} \quad (2-16)$$

$\bar{u}_n$  = mean layer wind speed from mesoscale model at  $n^{\text{th}}$  point

$\bar{u}_n$  = mean wind speed in the layer containing the cloud

$$= \frac{\bar{u}_{5,n} (z_{T,n}^{(1+p_n)} - z_{B,n}^{(1+p_n)})}{(1+p) 5^{p_n} (z_{T,n} - z_{B,n})} \quad (2-17)$$

$\Delta x_n$  = incremental distance between the  $n$  points equal to 500 meters

$$\sigma_{yn} = \sigma'_{A,n} \left[ \Delta x_n + \left( \frac{\sigma_{y,n-1}}{\sigma'_{A,n}} \right)^{1/\alpha} \right]^\alpha \quad (2-18)$$

where

$\sigma'_{A,n}$  = standard deviation of the wind azimuth angle at the  $n^{\text{th}}$  point

$$= \sigma_{A,n} \left( \frac{\pi}{180} \right) \left( \frac{H'}{5} \right)^m \left( \frac{\tau}{600} \right)^{0.2} \quad (2-19)$$

$$H' = \begin{cases} H & ; H \geq 5 \\ 5 & ; H < 5 \end{cases} \quad (2-20)$$

$\tau$  = source function time  $\cong 2.5$  seconds for instantaneous sources

$\sigma'_{A,n}$  = ten-minute standard deviation of the wind azimuth angle

$$\sigma_{z,n} = \sigma'_{E,n} \left[ \Delta x_n + \left( \frac{\sigma_{z,n-1}}{\sigma_{E,n}} \right)^{1/\beta} \right]^\beta \quad (2-21)$$

where

$$\sigma'_{E,n} = \sigma_{E,n} (\pi/180) (H'/5)^n \quad (2-22)$$

$\sigma_{E,n}$  = standard deviation of the wind elevation angle

The cloud expansion coefficients  $\alpha$  (lateral) and  $\beta$  (vertical) in the above equations are set to unity for instantaneous sources.

The concentration  $\chi_n$  is calculated under the additional restriction that  $\chi_n \leq \chi_{n-1}$ . If  $\chi_n > \chi_{n-1}$ , the values of  $\sigma_{y,n}$  and  $\sigma_{x,n}$  are increased proportionately so that  $\chi_n = \chi_{n-1}$  and the calculations continued.

Dosage for an instantaneous source is obtained from the expression

$$D_n = \frac{\chi_n \sqrt{2\pi} \sigma_{xn}}{\bar{u}_{z,n}} \quad (2-23)$$

where

$\bar{u}_{z,n}$  = mean wind speed at the calculation height  $z$  and  $n^{\text{th}}$  point on the trajectory

$$= \begin{cases} \bar{u}_{5,n} \left(\frac{z}{5}\right)^{p_n} & ; z > 1 \\ \bar{u}_{5,n} \left(\frac{1}{5}\right)^{p_n} & ; z \leq 1 \end{cases} \quad (2-24)$$

#### Continuous Source Model

The continuous-source model for use in EPAMS is a modified version of the Gaussian model for continuous sources described by Pasquill (1962) in which the concentration is also expressed as the product of four terms:

$$\chi_{c,n} = \{\text{Peak Term}\} \{\text{Lateral Term}\} \{\text{Vertical Term}\} \{\text{Depletion Term}\} \quad (2-25)$$

The Peak Term of the continuous source concentration model is given by the expression

$$\text{Peak Term} = \frac{Q'}{2\pi \sigma_{zn} \sigma'_{yn} \bar{u}_n} \quad (2-26)$$

where

- $Q'$  = source strength expressed as a rate
- $\sigma'_{yn}$  = standard deviation of the concentration distribution in the crosswind direction for a continuous source at the  $n^{\text{th}}$  distance along the plume trajectory

and  $\bar{u}_n$  and  $\sigma_{zn}$  are respectively defined by Equations (2-17) and (2-19). The Vertical, Depletion and Lateral Terms (with  $\sigma_{yn}$  replaced by  $\sigma'_{yn}$  where appropriate)

are identical to the similar terms described for the instantaneous volume source.

The subset of equations describing  $\sigma'_{yn}$  is:

$$\sigma'_{yn} = \sigma'_{Ac,n} \left[ \Delta x_n + \left( \frac{\sigma'_{y,n-1}}{\sigma'_{Ac,n}} \right)^{1/\alpha} \right]^\alpha \quad (2-27)$$

where

$$\sigma'_{Ac,n} = \sigma_{A,n} \left( \frac{\pi}{180} \right) \left( \frac{H'}{5} \right)^m \quad (2-28)$$

and the remaining parameters have previously defined. The default values of  $\alpha$  and  $\beta$  used in the program for continuous sources are  $\alpha = 0.9$  and  $\beta = 1$ .

#### Plume-Rise Models

The effective height  $H$  of a buoyant plume is given by the sum of the physical stack height  $h$  and the buoyant rise  $\Delta h$ . For a neutral or unstable atmosphere, the effective stack height is given by (after Briggs, 1971; 1972)

$$H = h + f \left\{ \frac{15.98}{\bar{u}\{h\}} \left[ r_s^2 w \left( 1 - \frac{T_s}{T_c} \right) \right]^{1/3} h^{2/3} \right\} \quad (2-29)$$

where

$r_s$  = the inner radius of the stack at the exit (m)



$$\begin{aligned}
w &= \text{the stack exit velocity (m/sec}^{-1}\text{)} \\
T_c &= \text{the stack exit temperature (}^{\circ}\text{K) for the continuous source} \\
T_s &= \text{ambient air temperature (}^{\circ}\text{K)} \\
f &= \text{empirical correction factor} \\
h &= \text{actual stack height} \\
\bar{u}\{h\} &= \text{mean wind speed at stack height} \\
&= \bar{u}_{5, n=1} \left(\frac{h}{5}\right)^{p_{n=1}} \quad (2-30)
\end{aligned}$$

The factor  $f$ , which limits the plume rise as  $\bar{u}\{h\}$  approaches the stack exit velocity  $w$ , is defined by

$$f = \left\{ \begin{array}{ll} 1 & ; \bar{u}\{h\} \leq w/1.5 \\ \left(\frac{3w - 3\bar{u}\{h\}}{w}\right) & ; w/1.5 < \bar{u}\{h\} < w \\ 0 & ; \bar{u}\{h\} \geq w \end{array} \right\} \quad (2-31)$$

Equation (2-29) is used in the EPAMS program when the net radiation index equals or exceeds 2,  $\bar{u}\{h\}$  equals or exceeds 5 meters per second, or the potential temperature lapse rate  $\bar{\Phi}$  is equal to or less than 0. When these conditions are not met, the program uses the corresponding Briggs (1971) rise formula for a stable atmosphere given by

$$H = \left\{ \begin{array}{l} h + 2.397 f \left[ \frac{w r_s^2 T_s}{\bar{u}\{h\} \Phi} \left( 1 - \frac{T_s}{T_c} \right) \right]^{1/3} ; \frac{\pi u\{h\}}{10 S^{1/2}} < h \\ h + 1.903 f \left\{ \frac{w r_s^2 T_s}{\bar{u}\{h\} \Phi} \left[ 1 - \cos \left( \frac{10 S^{1/2} h}{\bar{u}\{h\}} \right) \right] \right\}^{1/3} ; \frac{\pi \bar{u}\{h\}}{10 S^{1/2}} \geq h \end{array} \right\} \quad (2-32)$$

where

$$\begin{aligned} S &= \text{stability parameter} \\ &= \frac{9.8}{T_s} \bar{\Phi} \end{aligned} \quad (2-33)$$

$\bar{\Phi}$  = height-weighted mean potential temperature lapse rate over an approximately 200-meter interval above  $h$

$$\begin{aligned} & \frac{\sum_{z=h}^{z=h+200} \Phi_z \Delta Z_z}{\sum_{z=h}^{z=h+200} \Delta Z_z} \end{aligned} \quad (2-34)$$

$$\Phi_z = \frac{T_{A,z+1} - T_{A,z}}{\Delta Z_z} \quad (2-35)$$

$$\Delta Z_z = Z_{z+1} - Z_z \quad (2-36)$$

$T_{A,z}$  = potential temperature at height  $Z_z$

$T_{A,z+1}$  = potential temperature at height  $Z_{z+1}$

### SECTION 3

#### DATA ANALYSIS PROCEDURES

The EPAMS data base contains data blocks of rawinsonde, USAF GWC predicted wind and temperature data, and surface meteorological information. Section 3 describes the automated data analysis procedures required to utilize this data in the development of parametric inputs to the mesoscale wind-field and diffusion models. The Mixing-Layer Analysis Routine described in Section 3.1 below is designed to provide initialization parameters required by the mesoscale wind-field model. The Diffusion Model Routine, described in Section 3.2, uses surface meteorological data and mixing layer parameters provided by the mesoscale wind-field model as direct inputs to the diffusion model and for use in defining other model input parameters.

#### 3.1 MIXING-LAYER ANALYSIS ROUTINE

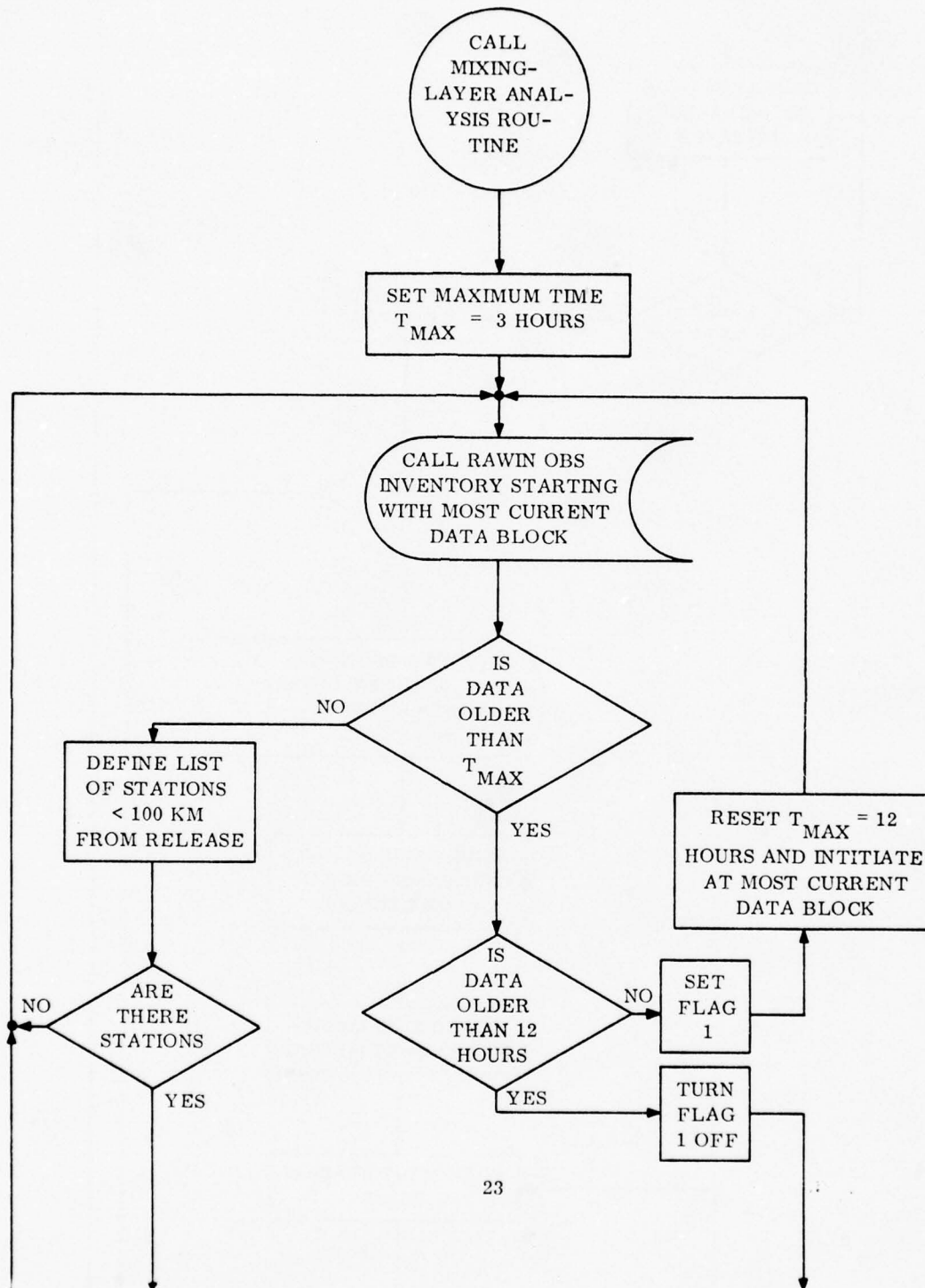
The Mixing-Layer Analysis Routine uses a relatively simplistic approach to utilize the various types of data available for the EPAMS data base in the calculation of initialization parameters for the mesoscale wind-field model. The decision to maintain a simple approach in this initial effort to develop a comprehensive prediction program was made so that the effects of logic decisions on the derived parameters could be easily traced and analyzed. Based on this reasoning, the analysis routine is currently designed to perform a modified "single-station analysis" rather than a more complex analysis of the pressure, wind and temperature fields over the entire region of interest. It should also be noted that some of the logic decisions made in accepting, rejecting and analyzing the data are somewhat arbitrary at this point in the development of the program. Where time has permitted, we have attempted to study the effects of the various decision processes. However, until the program is used to predict dosage and concentration fields under a wide variety of meteorological conditions, the total implications of many of the decision processes will remain unknown.

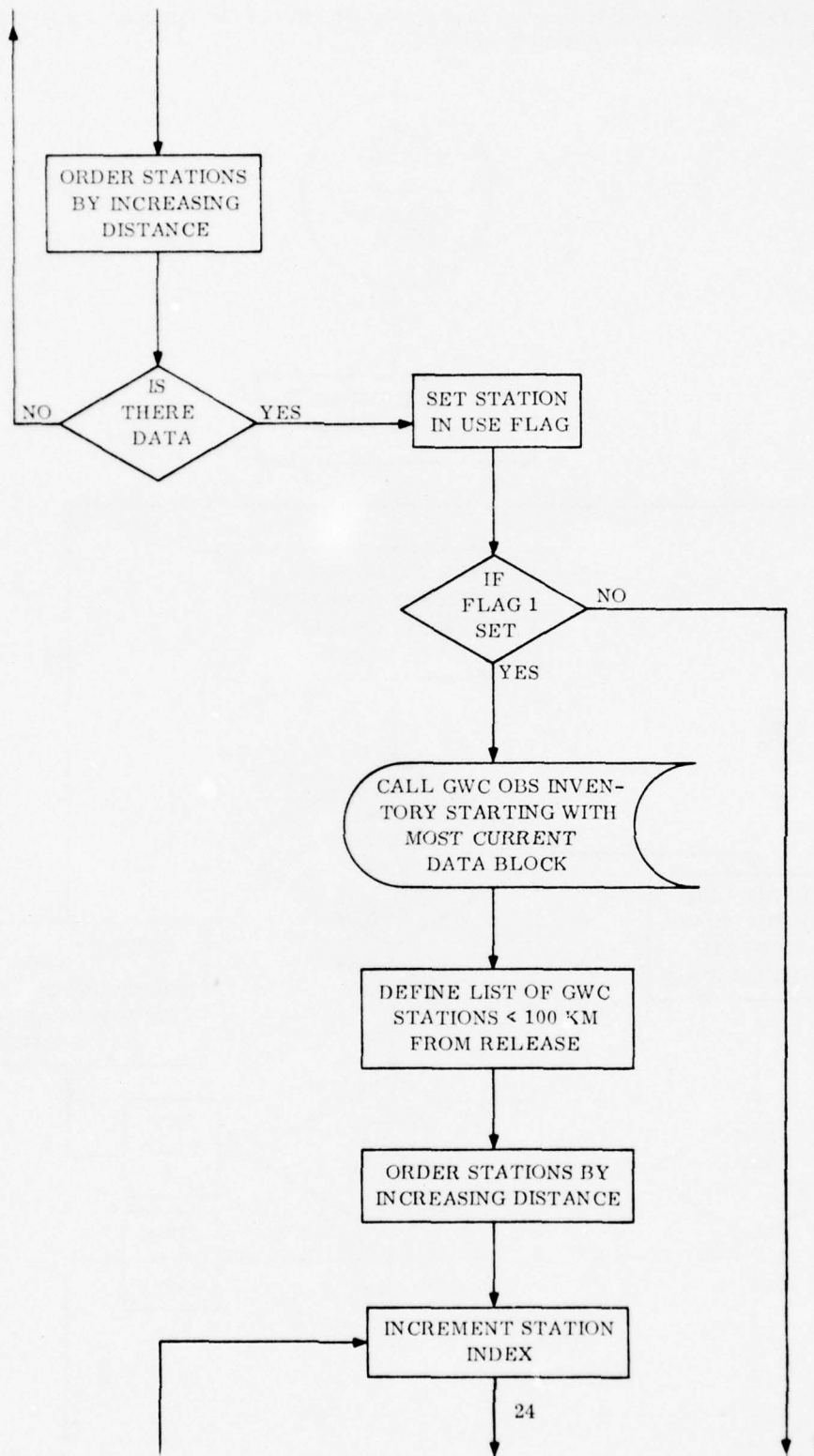
Features of the Mixing-Layer Analysis Routine are portrayed in the schematic logic diagram shown in Figure 3-1. Inspection of Figure 3-1 shows that the key features of the procedure are:

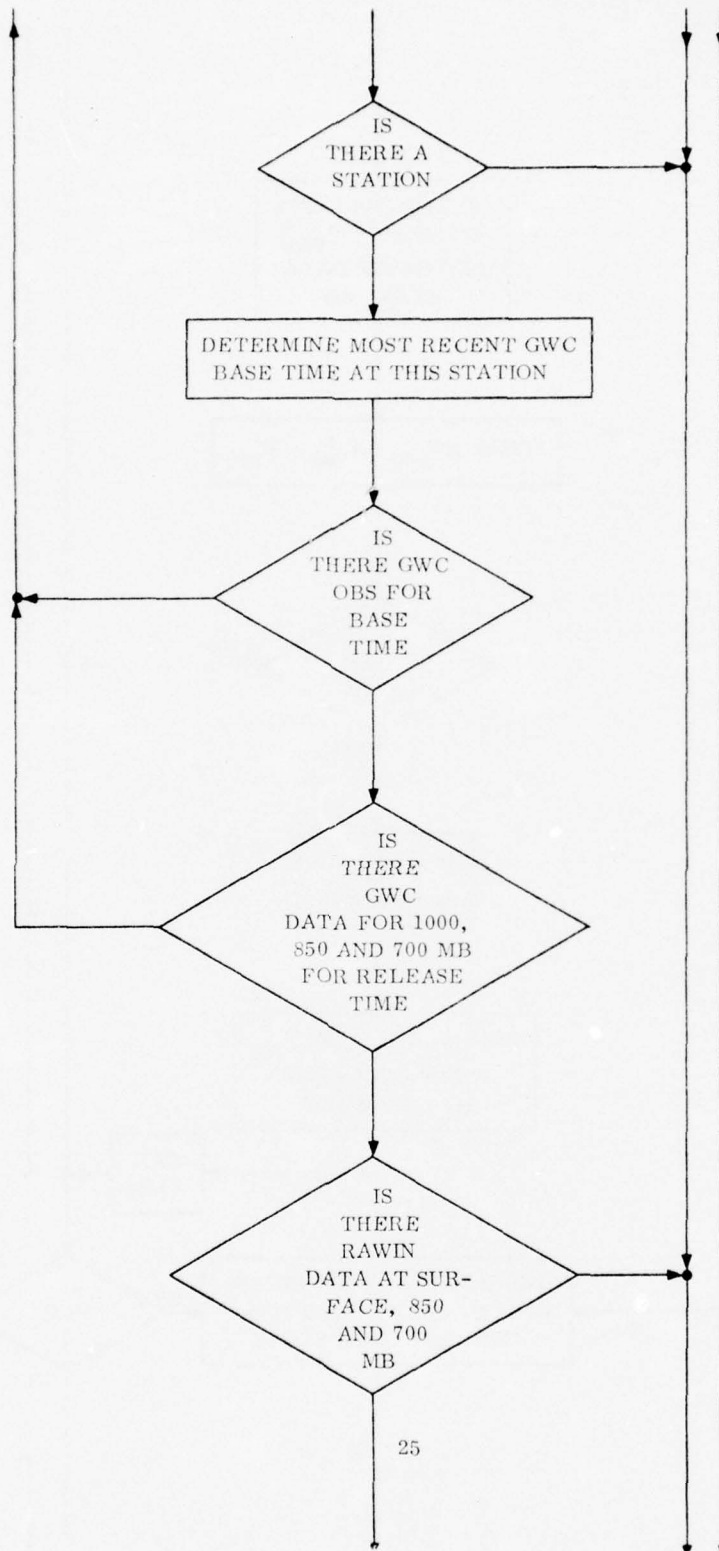
- Rawinsonde data from the closest station with a radius of less than 100 kilometers from the release point and less than three-hours old at the time of request will be used without modification to obtain estimates of the input parameters to the mesoscale model
- Rawinsonde data measured at the closest station less than 100 kilometers from the release point, greater than three-hours old and less than twelve-hours old are subject to modification using GWC predicted and surface winds and temperatures
- Climatological estimates of mixing-layer depths and surface wind speeds are used as mesoscale model inputs if all rawinsonde data is more than twelve hours old or if there are no stations within a 100 kilometer radius of the release point
- Climatological estimates are also used if the rawinsonde data is greater than six-hours old and the rawinsonde surface temperature and 850 millibar temperatures have not been modified because of unavailable or inadequate GWC and surface data
- GWC data is used to modify the rawinsonde temperatures and winds at the 700 and 850 millibar levels; rawinsonde

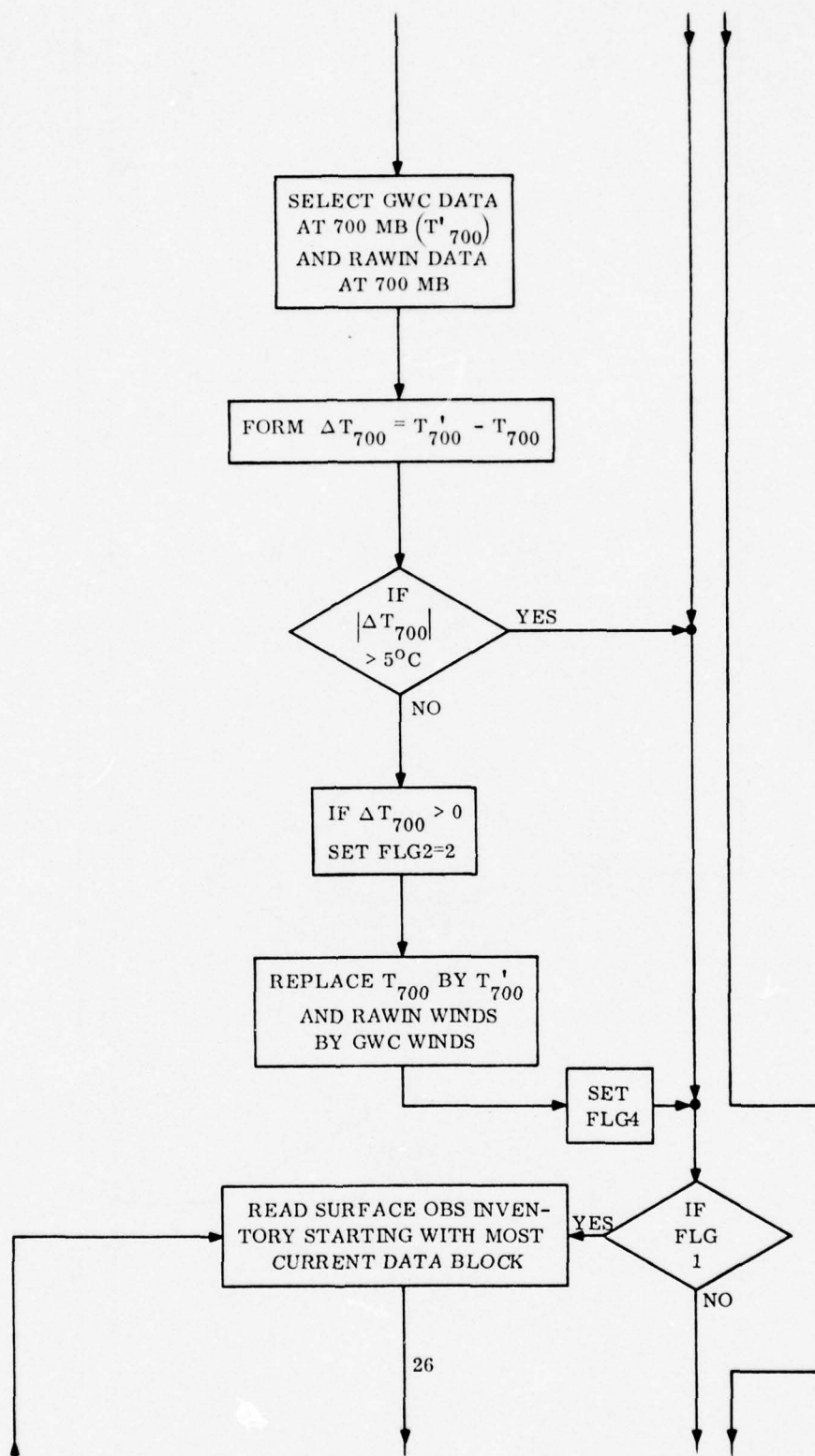


Figure 3-1. Schematic diagram illustrating procedures for obtaining inputs to the mesoscale wind field model.

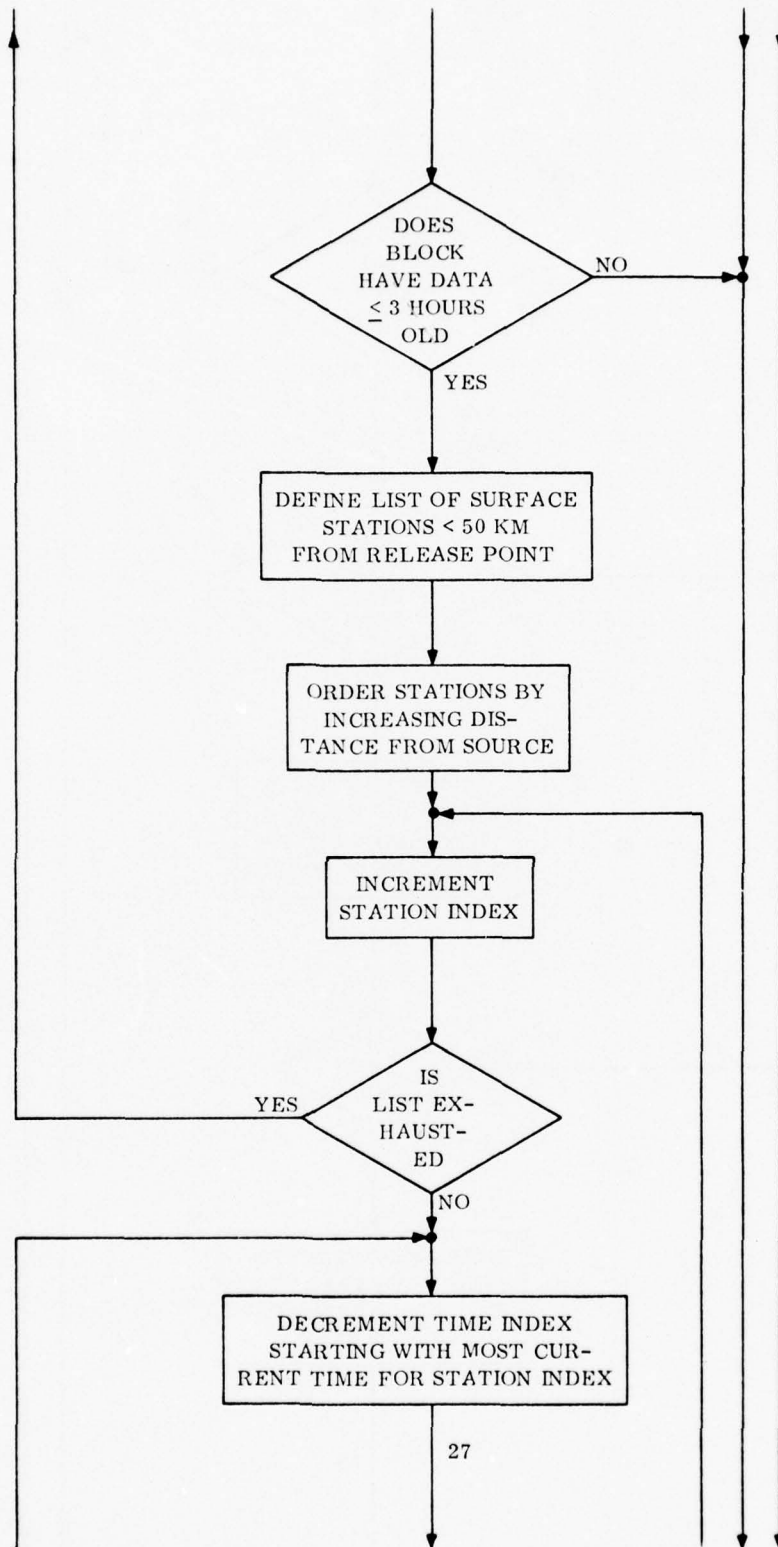


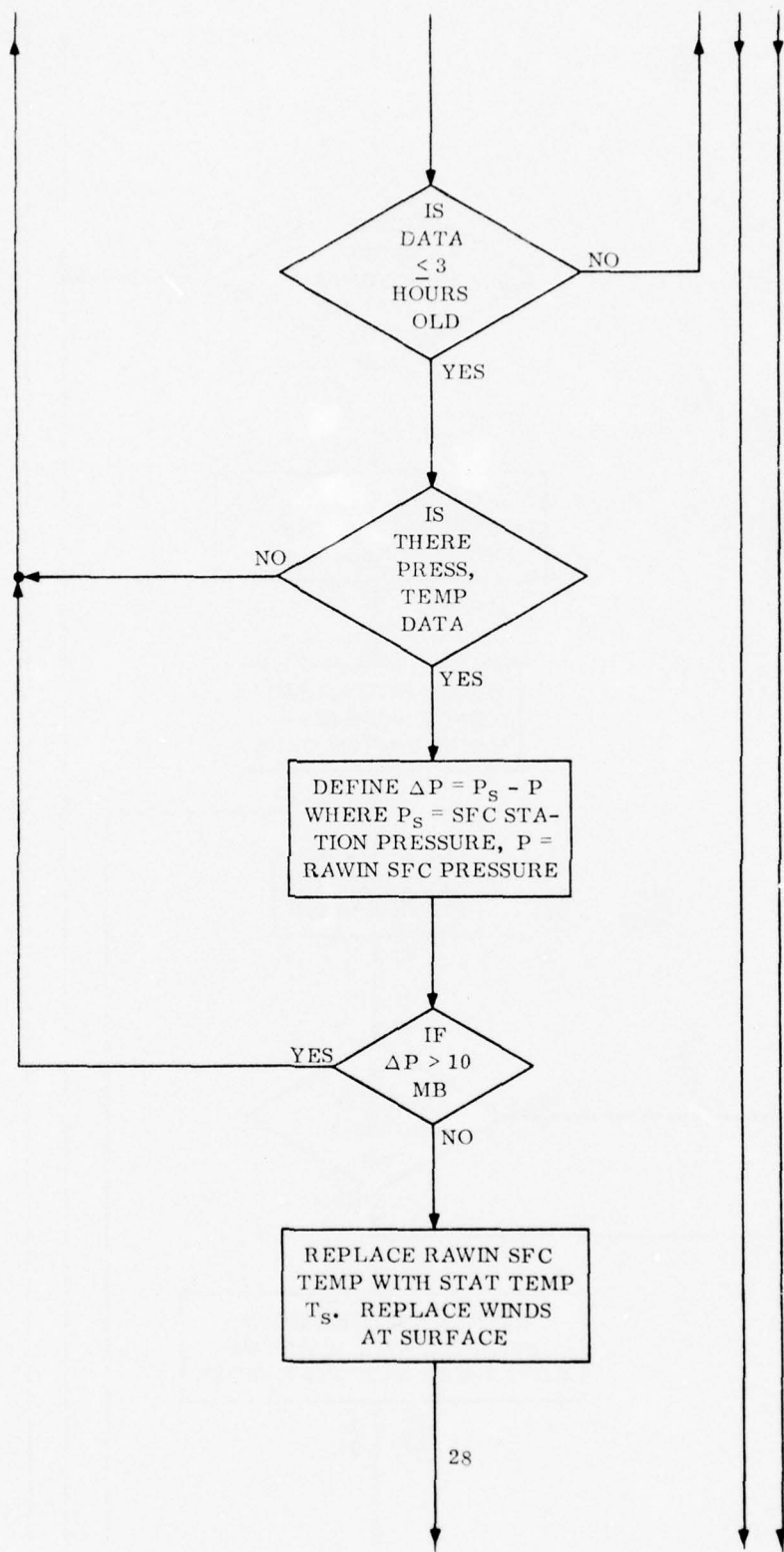


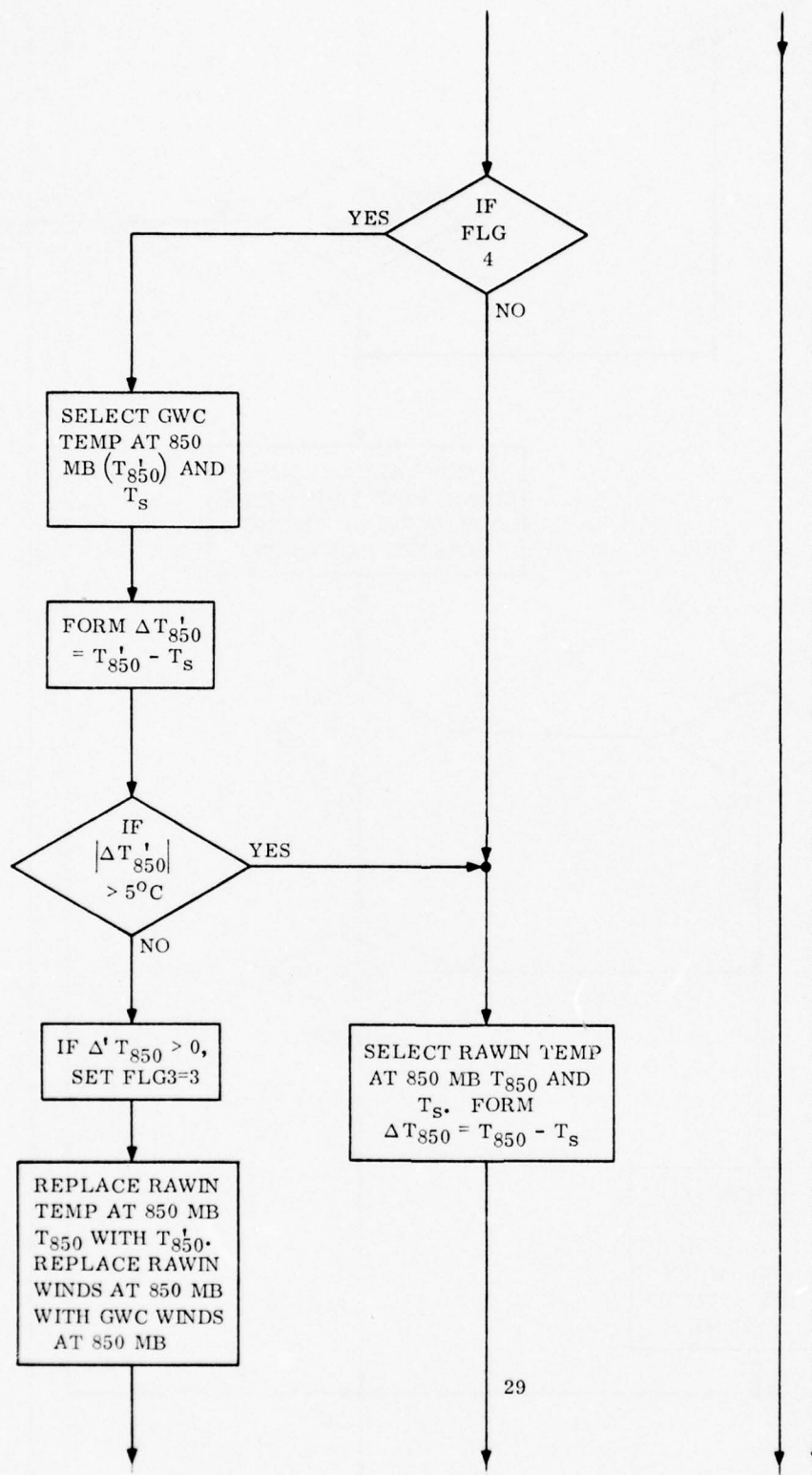


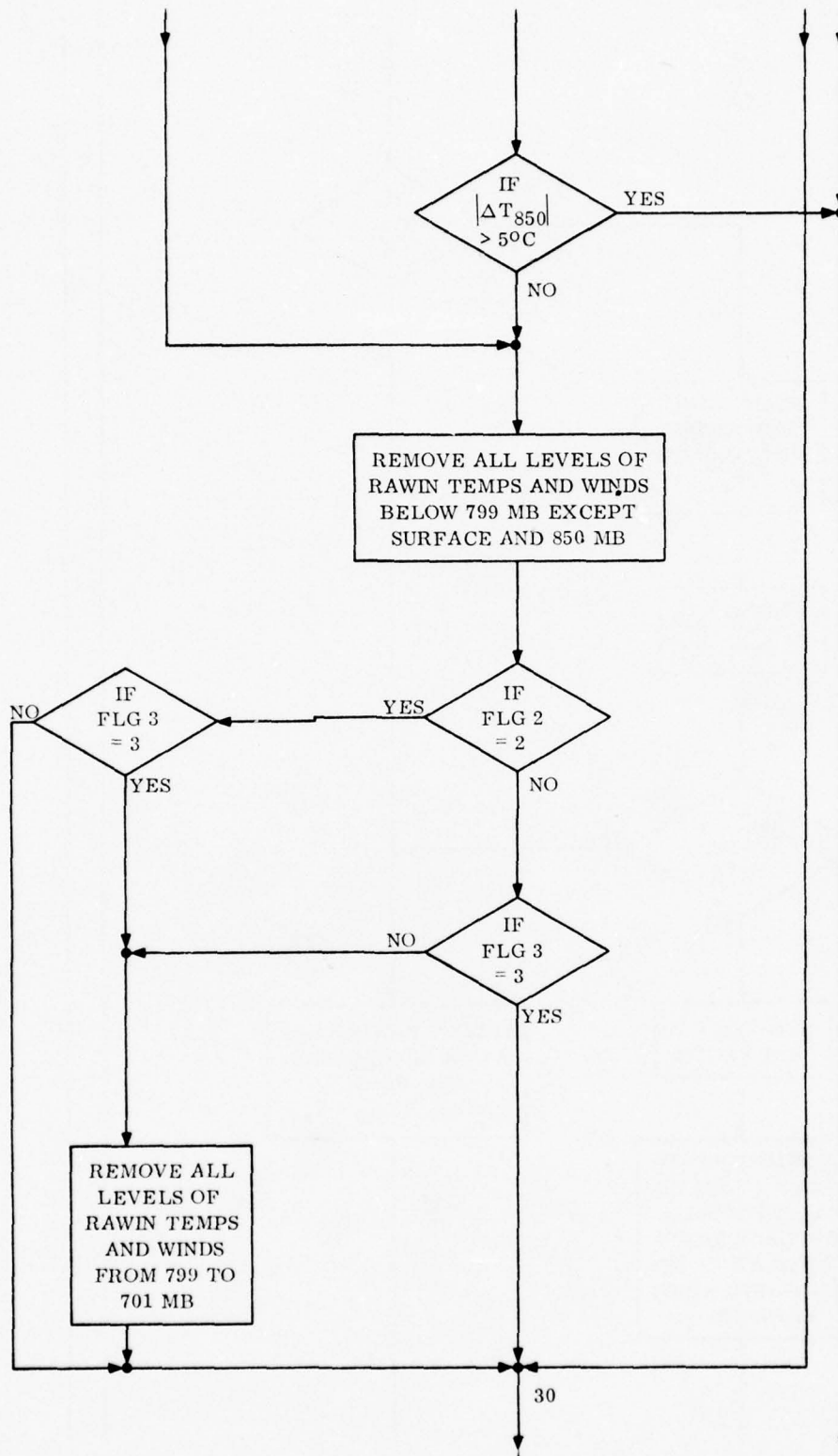




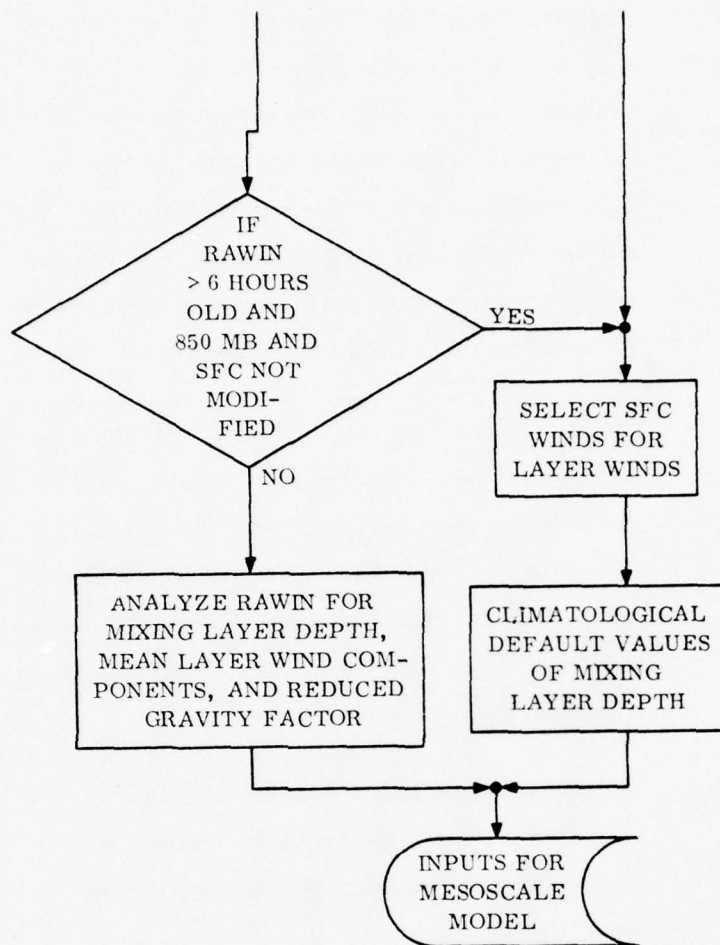












temperatures and winds at the 700 millibar are replaced if the GWC predicted temperature for the hour of interest is within 5 degrees Celsius; rawinsonde temperatures and winds at 850 millibars are replaced if the temperature from the reporting surface station nearest the time and point of release is within 5 degrees Celsius of the GWC predicted temperature at the 850 millibar level for the hour of interest

- Surface temperature and wind data from the closest station less than 50 kilometers from the release point, less than three-hours old, and with a surface pressure within 10 millibars of the surface pressure from the rawinsonde observation, is used to modify the surface rawinsonde observation when it is more than three-hours old
- Surface wind speeds from the closest station to the point of release are used as default values for the mean-layer wind speed if the rawinsonde data is not analyzed

Climatological estimates of the mixing layer depth shown in Table 3-1 are used as default values where the rawinsonde data is not available or is not analyzed for some reason. These estimates of the median mixing depths as a function of month and time-of-day are based on the work of Norton and Hoidale (1975), who analyzed 8,236 rawinsonde observations made at WSMR between 1961 and 1972 using the technique described by Holzworth (1967).

As shown in Figure 3-1, the rawinsonde is analyzed to determine the mixing-layer depth, mean-layer wind direction and speed and reduced gravity

TABLE 3-1  
CLIMATOLOGICAL ESTIMATES OF THE MEDIAN SURFACE MIXING  
DEPTH  $H_m$  IN METERS (AFTER NORTON  
AND HOIDALE, 1975)

Local Time (Hour Ending)	Month											
	Jan	Feb	Mar	Apr	May	June	July	Aug	Sept	Oct	Nov	Dec
0700	30	30	30	50	30	30	30	30	30	30	30	30
0800	30	30	30	107	110	139	103	35	30	30	30	30
0900	30	30	114	326	467	403	329	238	129	89	30	30
1000	64	122	387	740	865	691	688	615	490	271	165	96
1100	232	329	832	1255	1298	1274	1034	1042	933	539	400	239
1200	434	639	1247	1761	1907	2053	1342	1431	1343	873	593	369
1300	645	1054	1518	2177	2521	2654	1868	1840	1708	1217	792	533
1400	822	1363	1804	2513	2915	2983	2388	2347	1896	1554	1025	734
1500	907	1543	2145	2872	3195	3162	2503	2749	1940	1711	1126	718
1600	753	1586	2276	2843	3292	3144	2116	2484	2038	1344	1039	435
1700	386	1148	1835	1954	2727	3065	1279	1572	1762	696	669	206
1800	102	436	946	824	1578	2606	516	816	932	280	231	102
1900	30	68	255	229	549	1466	191	398	252	181	71	35
2000	30	111	30	63	77	427	172	115	30	164	45	30
2100	30	142	30	30	30	30	153	30	30	77	30	30
2200-0600	30	30	30	30	30	30	30	30	30	30	30	30

factor. In developing an automated procedure for determining the mixing-layer depth, we studied the use of four methods for establishing that a surface-based or elevated inversion was indicated by the rawinsonde observations. The simple criteria associated with the four methods for determining the base of an inversion were:

<u>Method</u>	<u>Criteria</u>
1	$\frac{\Delta \theta}{\Delta z} > .01$
2	$\frac{\Delta T}{\Delta z} \geq 0$
3	$\frac{\Delta \theta_w}{\Delta z} \geq 0$
4	$\frac{\Delta T_v}{\Delta z} \geq -5 \times 10^{-4}$

where

$$\frac{\Delta \theta}{\Delta z} = \text{lapse rate of potential temperature}$$

$$\frac{\Delta T}{\Delta z} = \text{lapse rate of temperature}$$

$$\frac{\Delta \theta_w}{\Delta z} = \text{lapse rate of wet-bulb potential temperature}$$



$$\frac{\Delta T_v}{\Delta z} = \text{lapse rate of virtual temperature}$$

The computer program incorporating these criteria was used to analyze twice daily rawinsonde observations from Salt Lake City, Utah for the first five days of each month during the period June 1972 through May 1973 and for all the month of January 1973. The heights of the bases of stable layers obtained from the computer program were then qualitatively compared with those selected by meteorologists from plots of the data. All the criteria produced bases of stable layers in agreement with those selected by the meteorologists for cases in which clearly-defined stable layers were present. In our view, however, the criteria based on the lapse rate of virtual temperature (Method 4) performed more consistently than the other criteria when stable layers were not as clearly defined and for all seasons of the year. For this reason, the procedure finally used in the program is based on this criteria.

The program accepts the raw or modified rawinsonde data and begins the selection process by checking

$$\frac{\Delta T_{v,n}}{\Delta z_n} = \frac{T_{v,n+1} - T_{v,n}}{z_{n+1} - z_n} \quad (3-1)$$

in the first height interval above the surface. If the criterion for the base of a stable layer is met (e.g., if  $\Delta T_{v,1}/\Delta z_1 \geq -5 \times 10^{-4}$ ) and the height interval  $\Delta z$  is greater than or equal to 100 meters, the program defines a surface-based inversion and sets, by default, the surface mixing depth to 30 meters. If  $\Delta z_1$  is less than 100 meters but  $\Delta T_{v,1}/\Delta z_1 \geq -5 \times 10^{-4}$ , the program then checks  $\Delta T_{v,2}/\Delta z_2$ . If  $\Delta T_{v,2}/\Delta z_2 \geq -5 \times 10^{-4}$  and  $(\Delta z_1 + \Delta z_2) \geq 100$  meters, the program checks the quantity

$$\left(\frac{\Delta T}{\Delta z}\right)' = \frac{T_{v,n+2} - T_{v,n}}{z_{n+2} - z_n} = \frac{T_{v,3} - T_{v,1}}{z_3 - z_1} \quad (3-2)$$

If  $(\Delta T/\Delta z) \geq -5 \times 10^{-4}$ , the program again defines a surface-based inversion. If no surface based inversion is found, the program increments  $n$  and proceeds through the same operations until the base of an elevated inversion is found or until  $z_{n+1}$  exceeds 3000 meters AGL. If  $z_{n+1}$  exceeds 3000 meters AGL, the surface mixing depth is defaulted to 3000 meters.

After the depth of the surface mixing-layer  $H_m$  is established, the program analyzes the rawinsonde data between the surface and  $H_m$  to obtain estimates of the mean-layer wind components and the reduced gravity factor using the expressions:

$$u_{H_m} = \frac{\sum_{n=1}^{H_m} u_n (z_{n+1} - z_n)}{\sum_{n=1}^{H_m} (z_{n+1} - z_n)} \quad (3-3)$$

$$v_{H_m} = \frac{\sum_{n=1}^{H_m} v_n (z_{n+1} - z_n)}{\sum_{n=1}^{H_m} (z_{n+1} - z_n)} \quad (3-4)$$

$$g' = g \left[ 1 - \frac{\left( \sum_{n=1}^{H_m} T_n (z_{n+1} - z_n) / \sum_{n=1}^{H_m} (z_{n+1} - z_n) \right)}{T_{I, \max}} \right] \quad (3-5)$$

where  $T_{L, \max}$  is the maximum temperature in the stable layer above  $H_m$ . In the program,  $g'$  is restricted so that if it exceeds 0.3 it is set to 0.3 and if less than 0.1 is set to 0.1.

### 3.2 DIFFUSION MODEL ROUTINE

The meteorological and source parameters required by the diffusion models are given in Table 3-2. Of the meteorological parameters shown in the table, the user need only supply the program with values of  $r$  and  $A$  if they differ from the default values of 1 and 0, respectively. The program user must supply all the source input parameters to the program and, in addition, denote whether the source is instantaneous or continuous. For program test purposes, the program now contains two default continuous sources corresponding to the American Smelting and Refining Company stacks associated with their lead and copper refineries in El Paso, Texas. The source inputs for these stacks were supplied by WSMR. Default values of  $V_s$  and  $k$  equal to zero are used in the program.

Since the turbulence parameters  $\sigma'_{A,n}$  and  $\sigma'_{E,n}$ , their power-law coefficients for height dependency  $m$  and  $n$ , and the power-law coefficient  $p_n$  are not routinely measured at meteorological stations, a means of assigning appropriate values to these meteorological parameters was required. Swanson and Cramer (1965) made a comprehensive study of the height dependence of  $\sigma_A$  as a function of wind speed and time-of-day using measurements from a 62-meter tower at WSMR. The decision was made to use the results of this study in conjunction with a stability classification system, similar to the Pasquill definition of stability categories (Turner, 1964) used by the Environmental Protection Agency, to select and assign values to these parameters. Figure 3-2 is a schematic diagram showing the logic sequence used by the program in defining the parameters and their use in the diffusion models.

TABLE 3-2  
METEOROLOGICAL AND SOURCE INPUTS  
FOR THE DIFFUSION MODELS

Parameter	Definition
(a) Meteorological Inputs	
NR	Net radiation index
$H_{m,n}$	Depth of the surface mixing layer at the $n^{\text{th}}$ point in the trajectory
$\bar{u}_n$	Mean layer wind speed in the surface mixing layer at the $n^{\text{th}}$ point on the trajectory
$\sigma'_{A,n}$	Standard deviation of the wind azimuth angle at the $n^{\text{th}}$ point on the trajectory
m	Power-law coefficient used to describe the height dependency of $\sigma_{A,n}$ in the surface mixing layer
$\sigma'_{E,n}$	Standard deviation of the wind elevation angle at the $n^{\text{th}}$ point on the trajectory
n	Power-law coefficient used to describe the height dependency of $\sigma_{E,n}$ in the surface mixing layer
$p_n$	Power-law coefficient used to describe the height dependency of wind speed in the surface mixing layer
r	Fraction of material reflected at the surface
$\Lambda$	Washout coefficient or fraction of material removed by precipitation scavenging per unit time



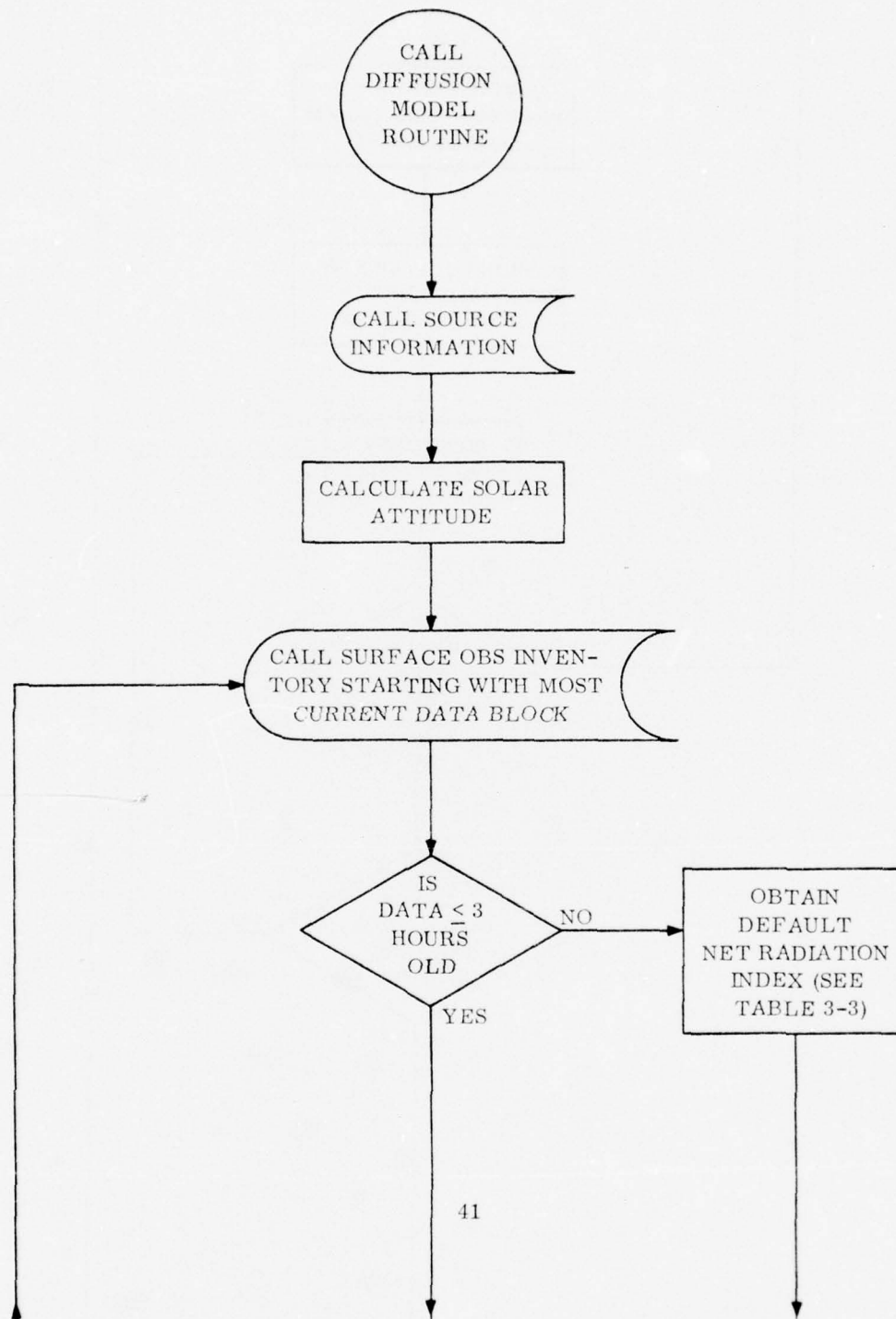
TABLE 3-2 (Continued)

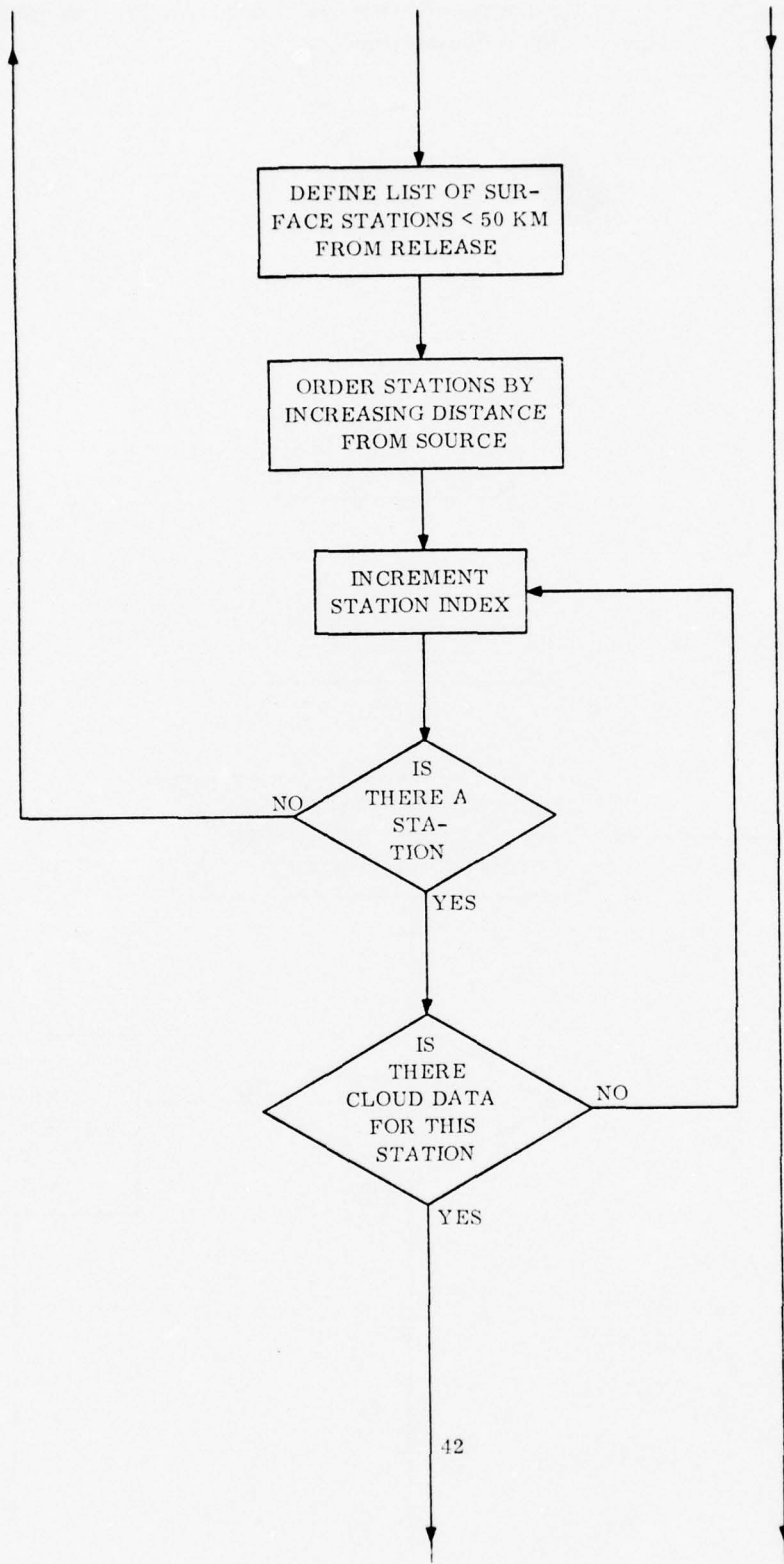
Parameter	Definition
(b) Source Inputs	
$x, y, h$	Coordinates of the source
$Q$	Source Strength
$T_c$	Stack exit temperature ( $^{\circ}\text{K}$ ) for the continuous source
$r_s$	Inner radius of the stack at the exit
$w$	Stack exit velocity
$V_s$	Settling velocity for material in a given size category
$k$	Decay coefficient or fraction of material lost per unit time

Key features of the logic sequence shown in Figure 3-2 are that:

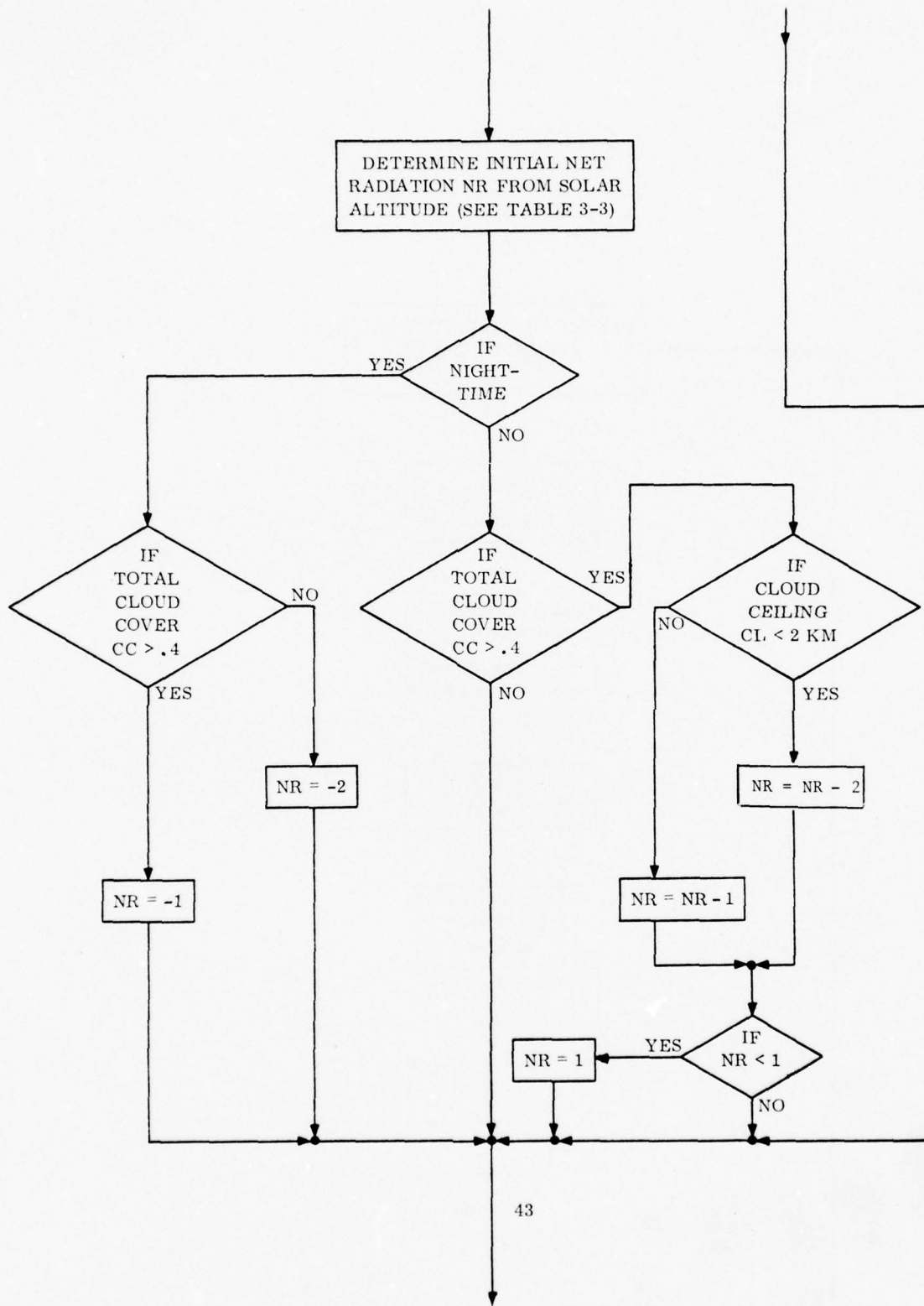
- Solar altitudes for the release point and time of request are calculated using an algorithm suggested by Woolf (1968)
- The program then seeks the most recent cloud and ceiling data from the nearest reporting station to the release point
- If there are no stations reporting cloud and ceiling data within a 50-kilometer radius from the release point or the data is more than three-hours old, the program selects a default net radiation index from Table 3-3
- When cloud data is available, the program calculates an initial net radiation index based on solar altitude (also see Table 3-3) and adjusts the index based on the time-of-day total cloud cover, and ceiling height
- The net radiation index and the wind speeds from the mesoscale wind-field prediction model for the release point and points along the cloud trajectory are used to select turbulent input parameters and wind power-law coefficients for the diffusion models
- Values of the surface mixing depth  $H_{m,n}$  for each  $n^{\text{th}}$  point along the cloud trajectory are obtained from the mesoscale wind-field solution using the interpolation procedure given by Equation (2-5)

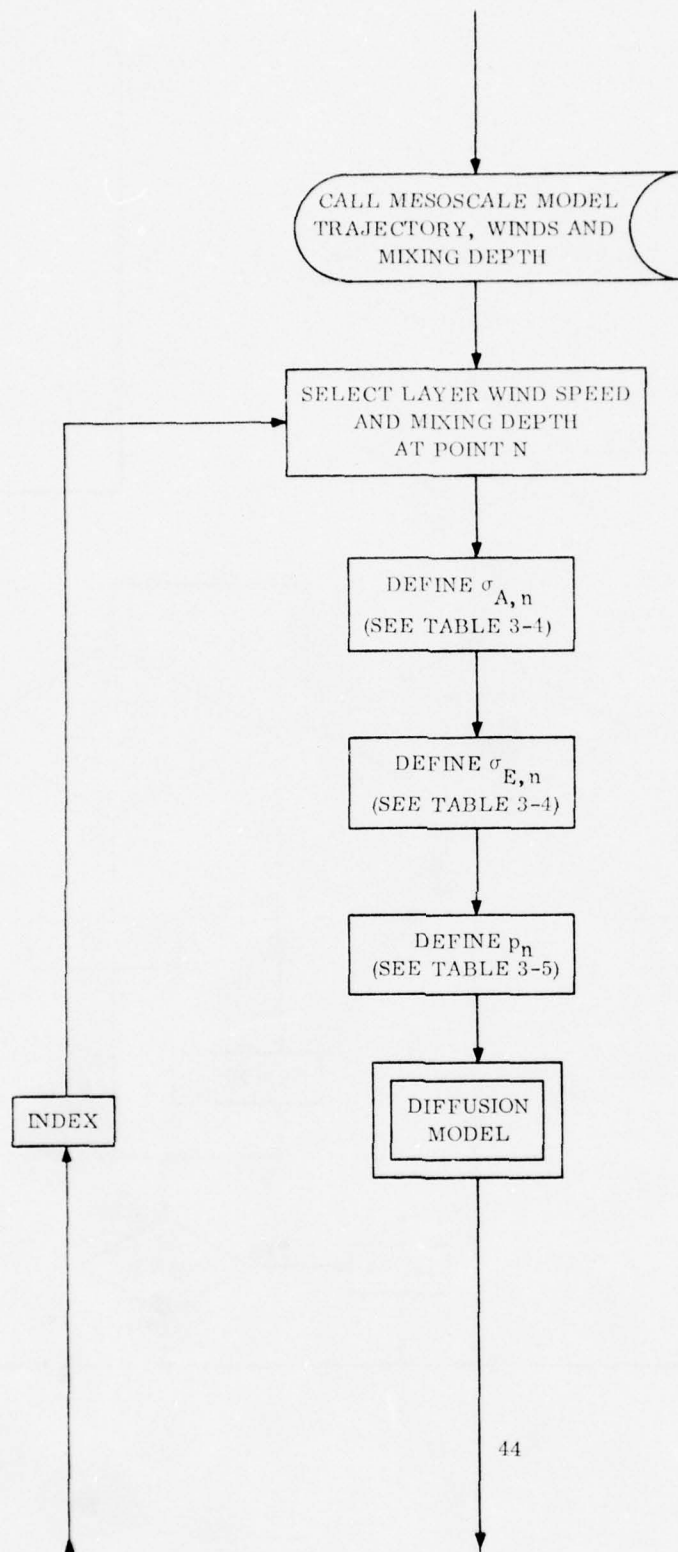
Figure 3-2. Schematic diagram illustrating procedures for obtaining inputs to the diffusion models.











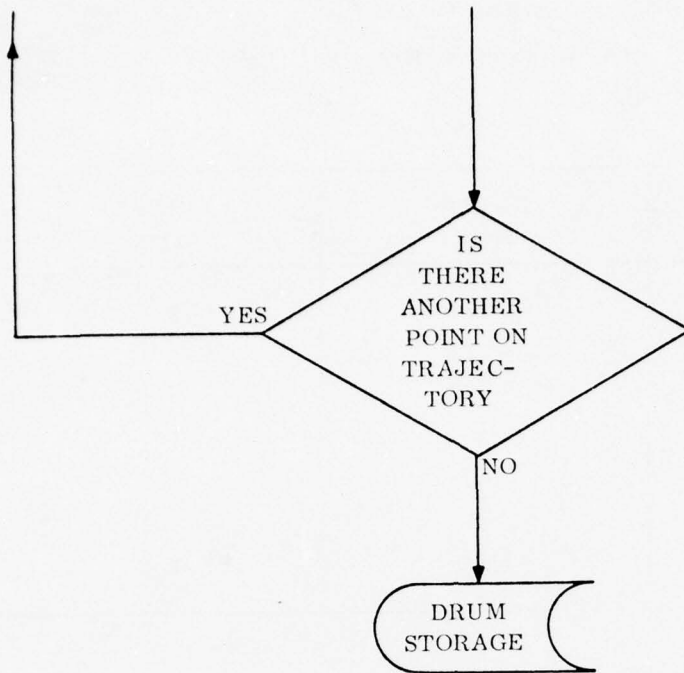


TABLE 3-3  
NET RADIATION INDICES

Solar Altitude $\eta$ In Degrees	Daytime Index	Default Index
$\eta > 60$	4	3
$35 < \eta \leq 60$	3	2
$15 < \eta \leq 35$	2	1
$0 < \eta \leq 15$	1	0
Nighttime	N/A	-1



Table 3-4(a) shows values of the ten-minute standard deviations of the wind azimuth angle in degrees  $(\sigma_A \{ \tau = 10 \text{ min} \})$  and associated values of the power-law coefficient  $m$  for describing  $\sigma_A$  variation with height above the surface based on the study of Swanson and Cramer. Values of the standard deviation of the wind elevation angle in degrees and the power-law coefficient  $n$  describing the variation of  $\sigma_E$  with height above the surface are shown in Figure 3-4(b). These values of  $\sigma_E$  were assigned under the assumption that (after Cramer, et al., 1972) turbulence is isotropic for short averaging times and that the one-fifth power law can be used as a scale factor to adjust  $\sigma_A$  for averaging times less than 10 minutes. Thus,

$$\sigma_E \cong \sigma_A \{ \tau = 10 \text{ min} \} \left( \frac{2.5}{600} \right)^{1/5} \quad (3-6)$$

$$\cong \sigma_A \{ \tau = 10 \text{ min} \} / 2.99 \quad (3-7)$$

The values of the power-law coefficient  $n$  were assigned under the assumptions that:

- Under stable conditions (NR = -1, -2)

$$\sigma_{E,z} \sim \sigma_{E,z_R} \left( \frac{z}{z_R} \right)^{-p_n} \quad (3-8)$$

- Under near-neutral conditions (NR = 0, 1)

TABLE 3-4  
TURBULENCE PARAMETERS FOR  
TRANSPORT/DIFFUSION MODELS

(a) Ten-Minute Standard Deviations of the Wind Azimuth Angle in Degrees ( $\sigma_A$ ) and Corresponding Values of the Power-Law Exponent m

Wind Speed at 5 Meters (m/sec)	Net Radiation Index							
	4		3		2		1	
	$\sigma_A$	m	$\sigma_A$	m	$\sigma_A$	m	$\sigma_A$	m
$\bar{u} < 1$	26	-.109	26	-.109	21	-.133	15	-.112
$1 \leq \bar{u} < 3$	26	-.109	22	-.128	16	-.123	11	-.112
$3 \leq \bar{u} < 5$	19	-.122	16	-.123	13	-.103	9	-.120
$5 \leq \bar{u} < 7$	14	-.105	11	-.117	11	-.117	8	-.148
$7 \leq \bar{u}$	9	-.100	9	-.117	8	-.110	8	-.148

(b) Standard Deviation of the Wind Elevation Angle in Degrees ( $\sigma_E$ ) and Corresponding Values of the Power-Law Exponent n

Wind Speed at 5 Meters (m/sec)	Net Radiation Index							
	4		3		2		1	
	$\sigma_E$	n	$\sigma_E$	n	$\sigma_E$	n	$\sigma_E$	n
$\bar{u} < 1$	8.7	.10	8.7	.10	7.0	.07	5.0	0
$1 \leq \bar{u} < 3$	8.7	.10	7.4	.13	5.3	.07	3.7	0
$3 \leq \bar{u} < 5$	6.3	.15	5.3	.15	4.3	.13	3.0	0
$5 \leq \bar{u} < 7$	4.7	.20	3.7	.20	3.7	.15	2.7	0
$7 \leq \bar{u}$	3.0	.25	3.0	.20	2.7	.20	2.7	0

$$\sigma_{E,z} \sim \sigma_{E,z_R} \quad (3-9)$$

- Under unstable conditions (NR = 2, 3, 4)

$$\sigma_{E,z} \sim \sigma_{E,z_R} \left( \frac{z}{z_R} \right)^{0.3-p_n} \quad (3-10)$$

The values of the wind power-law coefficient  $p_n$  as a function of net radiation index and mean layer wind speed used in the program are shown in Table 3-5. These values are similar to those suggested for use at WSMR by Swanson and Hoidale (1962) and for Dugway Proving Ground by Cramer, et al., (1972).

The plume-rise models described in Section 2.2.2 above require estimates of the ambient air temperature and, under stable conditions, the lapse-rate of potential temperature. If surface meteorological data are available, the program automatically selects the ambient air temperatures according to the logic shown in Figure 3-2 and the lapse-rate of potential temperature is calculated from the rawinsonde sounding established using the logic described in Figure 3-1. If no surface data is available, the default values of surface temperature shown in Table 3-6 are used. The temperatures in the table are based on the monthly normal and maximum temperatures at El Paso extracted from the report "Climatic Atlas of the United States" published by the U. S. Department of Commerce in June 1968. The values shown for a net radiation index of -1 and -2 correspond to the normal minimum temperature for each month. Similarly, the values shown for net radiation indices of 0 and 1 and for indices of 2 and 3 respectively correspond to the normal average and normal maximum temperatures for each month. Finally, the surface temperatures for a net radiation index of -4 were obtained by taking an average of

TABLE 3-5  
WIND POWER-LAW EXPONENT  $p$  FOR  
TRANSPORT/DIFFUSION MODELS

Mean Layer Wind Speed $\bar{u}$ (m/sec)	Net Radiation Index						
	4	3	2	1	0	-1	-2
$\bar{u} < 1$	.2	.2	.20	.20	.20	.20	.3
$1 \leq \bar{u} < 3$	.2	.17	.20	.20	.20	.20	.25
$3 \leq \bar{u} < 5$	.15	.15	.17	.17	.20	.20	.20
$5 \leq \bar{u} < 7$	.10	.10	.15	.15	.15	.15	.15
$7 \leq \bar{u}$	.05	.10	.10	.10	.15	.15	.15



the recorded maximum temperature and the normal maximum temperature at El Paso for each month.

If no rawinsonde data are available, the program selects default values of the lapse rate of potential temperature from Table 3-7 based on the net radiation index and the calculated wind speed at stack height. The potential temperature lapse rates shown in Table 3-6 are based on our experience in applying the Briggs stable plume rise formula in predicting plume rise from industrial stacks located in relatively warm and dry climates. No values of the default potential temperature lapse rates are given for wind speeds greater than 5 meters per second and for net radiation indices greater than 1 because plume rise is calculated from Equation (2-29) rather than Equation (2-32) under these conditions.

TABLE 3-6  
DEFAULT VALUES OF SURFACE TEMPERATURE  $T_s$  ( $^{\circ}\text{K}$ )

Month	Net Radiation Index			
	4	3, 2	1, 0	-1, -2
Jan	292	286	279	272
Feb	296	290	282	275
Mar	300	294	286	277
Apr	303	299	290	282
May	308	304	295	287
Jun	312	308	300	292
Jul	312	308	301	294
Aug	310	307	300	293
Sep	308	304	297	289
Oct	303	299	291	283
Nov	297	292	284	275
Dec	293	287	280	272

TABLE 3-7  
 DEFAULT VALUES OF THE LAPSE RATE OF  
 POTENTIAL TEMPERATURE  $\bar{\Phi}$  (deg K/m)

Wind Speed $\bar{u}\{h\}$ (m sec <sup>-1</sup> )	Net Radiation Index			
	1	0	-1	-2
0 - 1.4	0.005	0.015	0.030	0.040
1.5 - 2.9	0.003	0.010	0.020	0.030
3.0 - 4.9	0.001	0.005	0.015	0.020

## SECTION 4

### ANALYSIS, APPLICATION AND GRAPHICS PHASES OF EPAMS

Figure 4-1 shows the executive components, in the form of a block diagram, of the EPAMS System. The EPAMS executive system manager, labeled XECAMS in Figure 4-1, is where all processing begins and ends. The executive systems manager on option passes control to the supervisors labeled ANALIZ, APPLY and PLTPRG which were designed and developed by the H. E. Cramer Company, Inc. to accomplish the technical objectives of the contract.

The analysis supervisor ANALIZ controls all processing in the Analysis Phase of EPAMS and passes control to the mixing layer and wind-field analysis foreman MIXLYR or to other meteorological analysis routines. The operational elements of MIXLYR are described in Section 4.1 below. The application supervisor APPLY passes control on option to the transport/diffusion application foreman TRYDIF or to other application routines. The operational elements of TRYDIF are described in Section 4.2. At the completion of either the Analysis or Application Phases, or at the completion of both phases, program control is returned to XECAMS. The executive systems manager can then address, on option, the graphics supervisor PLTPRG to obtain either printed or plotted solutions, or both types of solutions, developed in the application routines. Further details of the graphics supervisor PLTPRG are described in Section 4.3 below.

#### 4.1 ANALYSIS PHASE OF EPAMS

As shown in Figure 4-1, the foreman MIXLYR of the Analysis Phase of EPAMS is comprised of the two operational elements MXOBAN and SOLVMX. The operational subroutines of MXOBAN are shown in the form of a block diagram in Figure 4-2. The operational element MXOBAN controls the analysis of all meteor-



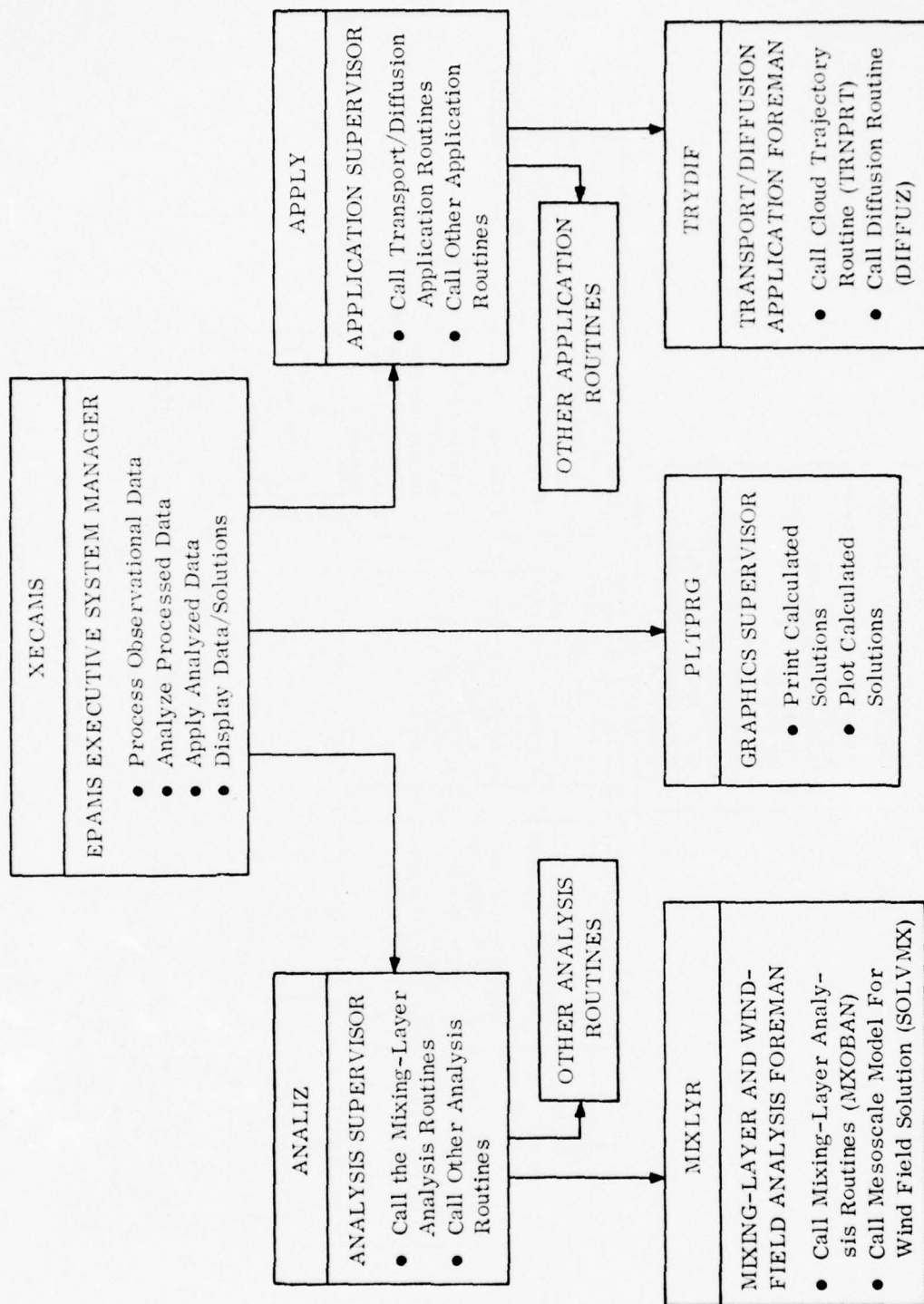


Figure 4-1. Executive System and Supervisors of the Analysis, Application and Graphics Phases of EPAMS.

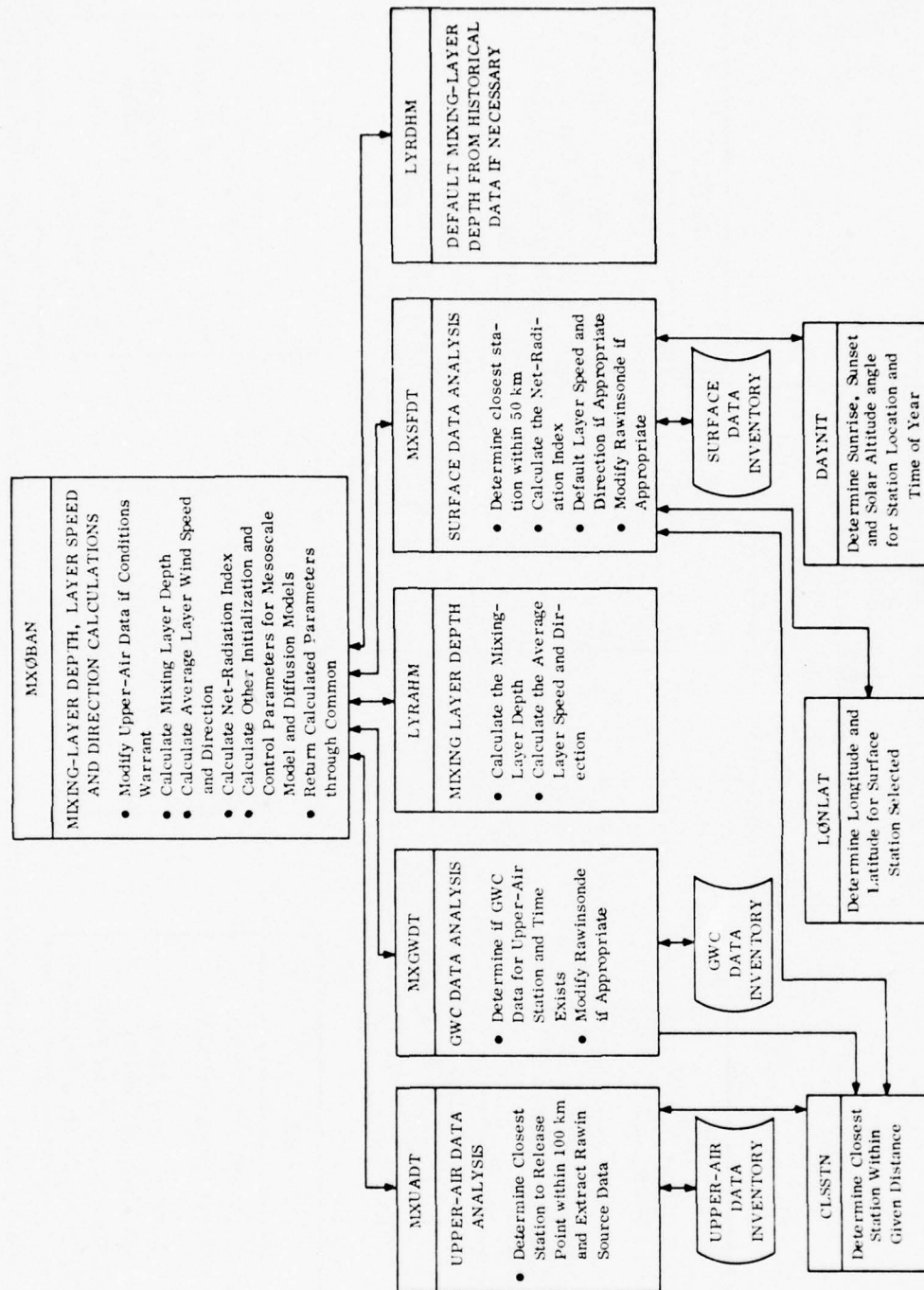


Figure 4-2. Operational Elements of MXQBAN Analysis Phase.

ological data and passes the results of the data analysis to the subroutine SOLVMX at the completion of execution. The EPAMS System user requests transport and diffusion information for a given time and source, which is then passed to MXOBAN via XECAMS. The MXOBAN mixing-layer analysis routine then proceeds to analyze rawinsonde, GWC and surface meteorological data according to the logic process described in Section 3.1. The subroutine MXUADT obtains rawinsonde data from the EPAMS data base for the desired solution time and source location. GWC prediction data and surface weather observations for use in the analysis are obtained from the data base via the subroutines MXGWDT and MXSFDT. These subroutines also use the GWC and surface data to modify the rawinsonde data if appropriate. The subroutine MXSFDT also calculates the net-radiation index for the surface meteorological station using information obtained from the LONLAT and DAYNIT subroutines. The rawinsonde data is then used in the subroutine LYRAHM to calculate the depth of the surface mixing layer and the mean wind components in the layer as described in Section 3.1. If insufficient data are available for calculating the mixing-layer depth or wind components, default data is supplied via the LYRDHM and MXSFDT subroutines. Control is then returned to the operational element MIXLYR and processing continues by branching to the subroutine SOLVMX.

A block diagram showing operational subelements of SOLVMX is given in Figure 4-3. Processing begins through examination of the mesoscale model input parameters passed to SOLVMX from MIXLYR to determine which of two procedures are to be used in initializing the mesoscale model. Thus, the input parameters from MIXLYR are compared in the subroutine MXSTRT with the input parameters used to generate the last solution of the mesoscale model resident in the EPAMS data base. The mesoscale model is initialized with the new inputs from MXOBAN if the mean layer wind speeds and elevation of the mixing depth above mean sea level (MSL) differ by more than twenty-five percent and the mean wind directions differ by more than ten degrees (cold start). The initial layer depth and momentum components for a cold start are given by the expressions

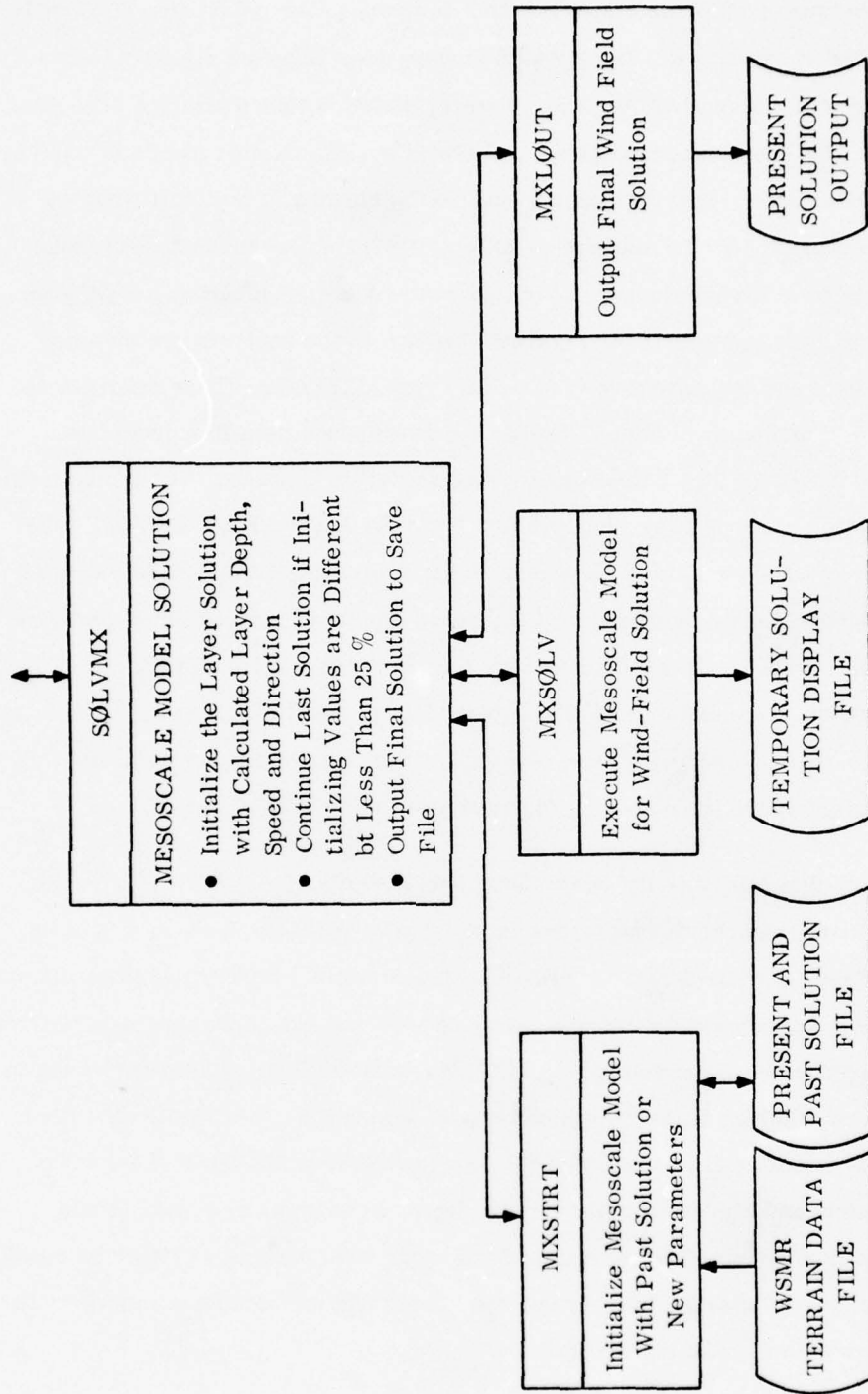


Figure 4-3. Operational Elements of SØLVVMX Analysis Phase.



$$H_{m;i,j} = H'_n - h'_{i,j} \quad (4-1)$$

$$M_{i,j} = U_n (H'_n - h'_{\min}) \quad (4-2)$$

$$N_{i,j} = V_n (H'_n - h'_{\min}) \quad (4-3)$$

where

$H'_n$  = mixing depth (MSL) calculated for the present hour

$h'_{i,j}$  = terrain elevation (MSL) at each solution matrix grid point

$U_n$  = easterly component of the mean layer wind for the present hour

$h'_{\min}$  = minimum terrain elevation (MSL) in the solution matrix

$V_n$  = northerly component of the mean layer wind for the present hour

If the differences are less than those specified above, subroutine MXSTRT calculates initialization parameters for a "hot" start from the expressions

$$H_{m;i,j} = (H'_{i,j} - h'_{i,j}) + H'_n - H'_o \quad (4-4)$$



$$M_{i,j} = (H'_{i,j} - h'_{i,j}) U_{i,j} + (H'_o - h'_{min})(U_n - U_o) \\ + U_n (H'_n - H'_o) \quad (4-5)$$

$$N_{i,j} = (H'_{i,j} - h'_{i,j}) V_{i,j} + (H'_o - h'_{min})(V_n - V_o) \\ + V_n (H'_n - H'_o) \quad (4-6)$$

where

$H'_{i,j}$  = mixing depth (MSL) at each solution matrix grid point for the previous wind-field solution

$H'_o$  = mixing depth (MSL) used to initialize the previous wind-field solution

$U_{i,j}$  = easterly component of the mean layer wind at each solution matrix grid point for the previous wind-field solution

$U_o$  = easterly component of the mean layer wind used to initialize the previous wind-field solution

$V_{i,j}$  = northerly component of the mean layer wind at each solution matrix grid point for the previous wind-field solution

$V_o$  = northerly component of the mean layer wind used to initialize the previous wind-field solution

After the initialization procedure has been completed, the input parameters are passed to the subroutine MXSOLV via SOLVMX for execution of the mesoscale wind-field model described in Section 2.1.

Subroutine MXSOLV will allow the mesoscale model to execute for a maximum model time of approximately 7200 seconds for a cold start and 1800 seconds for a hot start or until the solution converges, whichever occurs first. The subroutine begins to check convergence criteria after 1200 seconds model time has elapsed for a cold start or 600 seconds for a hot start. The convergence criteria is then checked after every application of the nine-point filter (after every seventh time-step if the default value is used). Subroutine MXSOLV begins the convergence check by calculating the relative variance of the change in mixing layer depth  $V_R(\Delta H_m)$  over the solution matrix according to the expression

$$V_R \Delta H_m = \left\{ \sum_{i=1}^n \sum_{j=1}^m (H'_{m;i,j} - H_{m;i,j})^2 - n \cdot m \left[ \sum_{i=1}^n \sum_{j=1}^m (H'_{m;i,j} - H_{m;i,j}) \right]^2 \right\} / \quad (4-7)$$

$$\left\{ \sum_{i=1}^n \sum_{j=1}^m (H'_{m;i,j})^2 - n \cdot m \left[ \sum_{i=1}^n \sum_{j=1}^m (H'_{m;i,j}) \right]^2 \right\}$$

where

$H'_m$  = layer depth calculated for the present time step at each point in the n by m matrix

$H_m$  = layer depth for the previous time step at each point in the n by m matrix

The subroutine determines the slope of the curve describing  $V_R(\Delta H_m)$  as a function of time and the difference between  $V_R(H_m)$  at the present and previous application of the filter. The solution is assumed to have converged if the

- Slope of the curve describing  $V_R(\Delta H_m)$  as a function of time is equal to or less than zero
- Present value of  $V_R(\Delta H_m)$  is less than the previous value and the difference between the values is less than or equal to  $1 \times 10^{-5}$

The program saves the converged mesoscale wind field solution and other parameters calculated in the mixing-layer routines by passing them to the EPAMS data base. At this point the Analysis Routine is terminated and control is returned to XECAMS.

#### 4.2 APPLICATION PHASE OF EPAMS

Inspection of Figure 4-1 above shows the foreman TRYDIF of the Applications Phase of EPAMS is comprised of the two operational elements TRNPRT and DIFFUZ. These operational elements perform the calculations outlined in the block diagram shown in Figure 4-4 after receiving program control through the foreman TRYDIF from XECAMS and the supervisor APPLY.

The subroutine TRNPRT calculates the trajectory of the cloud centroid downwind from the source location using the output from the mesoscale wind-field model and the procedures outlined in Section 2.2.1 above. The program calculates a point on the trajectory at intervals equal to one-tenth the spacing of the solution matrix of the mesoscale model (500 meters in the present case). At each of the calculated points on the trajectory, the program also determines the appropriate mixing-layer depth and wind speed for use in the diffusion models using the interpolation techniques described in Section 2.2.1. After completion of the calculations, program control is passed to subroutine DIFFUZ via TRYDIF.

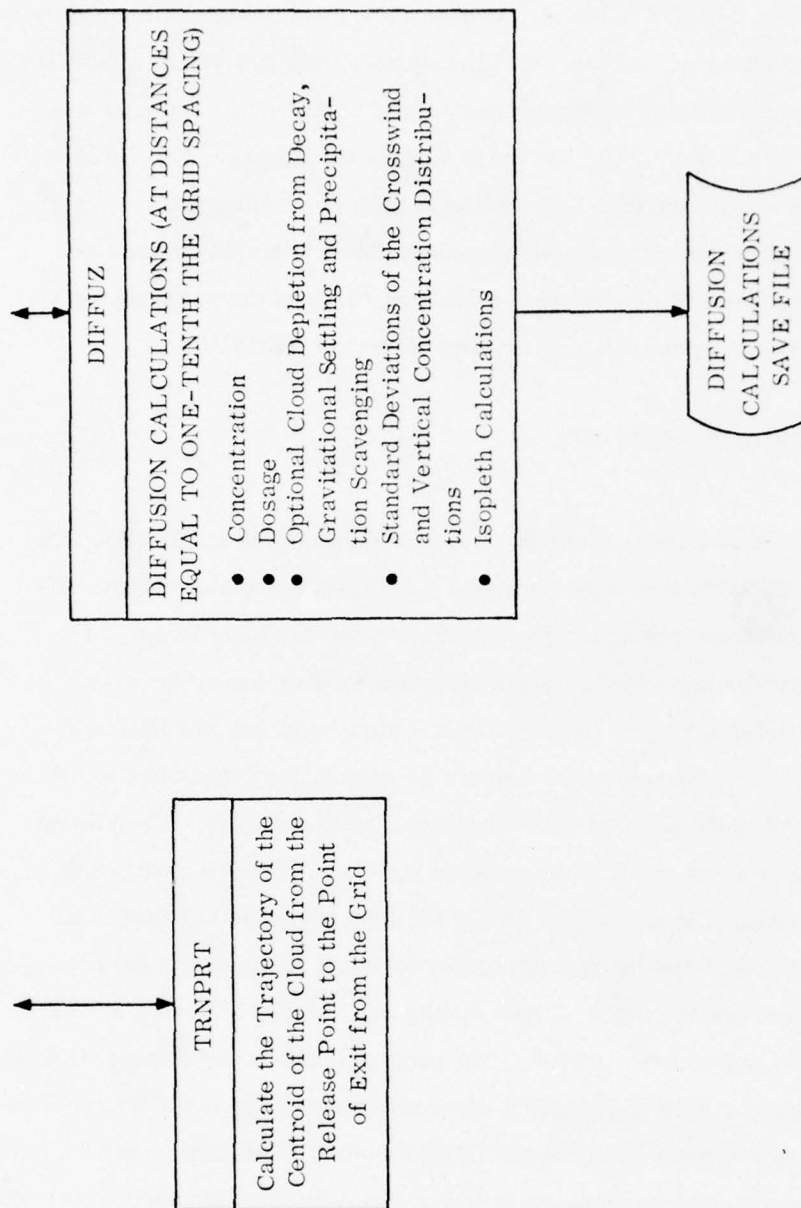


Figure 4-4. Application Phase of EPAMS.



The subroutine DIFFUZ calculates concentration and dosage with optional cloud depletion due to decay and either deposition losses from gravitational settling or precipitation scavenging using the instantaneous and continuous source models described in Section 2.2.2 above. At the users option, the program also calculates concentration and/or dosage isopleth half-widths at each point along the trajectory for instantaneous sources and concentration isopleth half-widths for continuous sources. At the completion of the diffusion model calculations the program writes the solutions to the EPAMS print file and returns control to XECAMS.

#### 4.3 GRAPHICS PHASE OF EPAMS

Figure 4-5 shows a block diagram of the Graphics Phase of EPAMS. The program routine PLTPRG is the supervisor that controls all graphics output. The program retrieves solutions created in the application and Analysis Phases of EPAMS and prints and/or plots the solutions on option as directed by the user through XECAMS. Options include the printing and plotting of intermediate and final wind-field patterns produced by the mesoscale model, isopleths of concentration and dosage, cloud trajectories and mixing-layer depth contours. The plotted solutions are shown on a base map of the solution matrix grid with a background of terrain-height contours. The subroutine labeled HEC004 in Figure 4-5 plots and labels the axes of each plot and the terrain height contours are added to the plot by subroutines HEC005 and HEC009. Wind velocity and direction vectors are calculated and plotted by subroutine HEC006. The program can, in subroutine HEC008, recalculate (at the user's option) additional cloud trajectories for other source locations using the solution wind-field in the EPAMS data base. The supervisor PLTPRG can also calculate and display concentration and dosage isopleths for additional levels at the user's option. This feature is useful if the initially requested levels do not show details in which the user is interested or if the initial levels were either so large or so small that they do not occur in the solution matrix. It should be noted



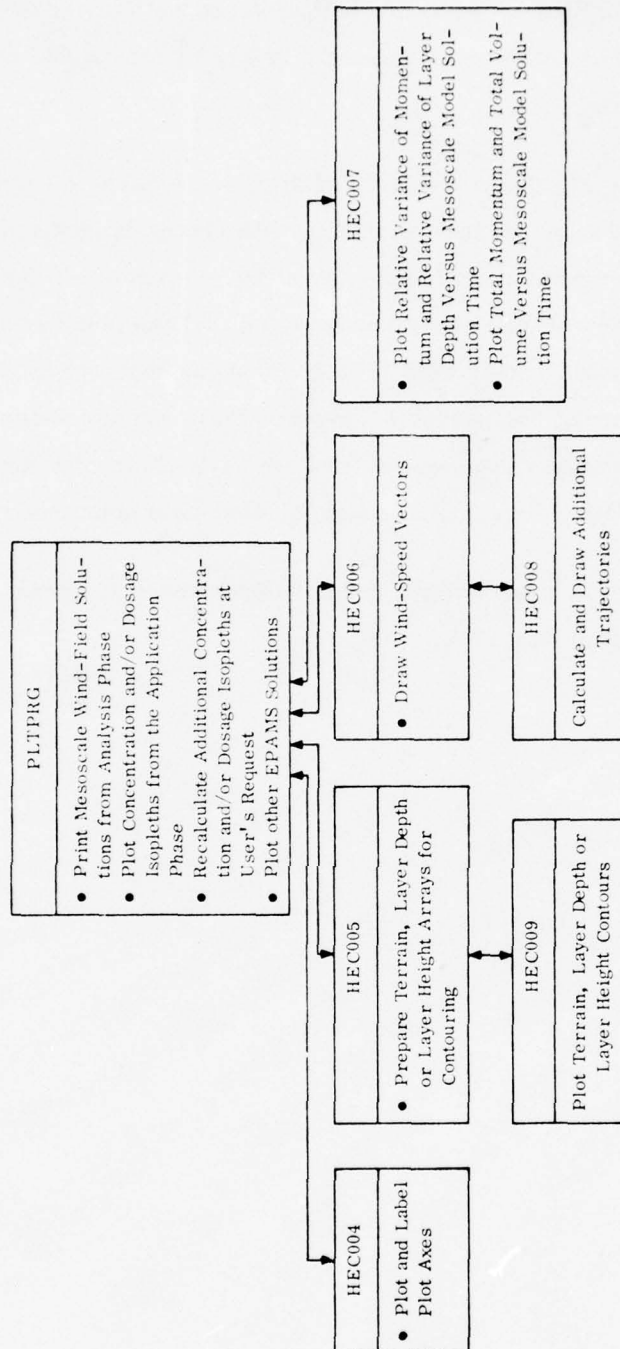


Figure 4-5. Operational elements of PLTPRG Graphics Phase.

that PLTPRG or its subroutines do not recalculate the wind-field nor the diffusion parameters, but use information from the last solutions to recalculate additional trajectories and isopleths.

The subroutine HEC007 controls the plotting of the relative variance of the change in layer depth, the relative variance of the change in momentum, the total mass and total momentum as a function of model solution time. As noted in Section 4.1, the relative variance of the change in layer depth is used as criteria for establishing that the mesoscale wind-field solution has converged. Since the mesoscale wind-field model theoretically conserves mass and momentum, the plots of total mass and momentum versus model time are useful in monitoring the effects of numerical approximations in calculations of the wind-field solutions.

At the completion of the plotting and print operations, program control is returned from PLTPRG to XECAMS.

## SECTION 5

### EXAMPLE CALCULATIONS

The Analysis and Application Phases of EPAMS were used to produce concentration and dosage isoplith plots for four example cases. The calculations were made for meteorological conditions that occurred in the vicinity of WSMR during the 14th and 15th of November 1974.

The surface weather pattern in the western United States on the 12th of November was characterized by a high-pressure ridge extending from the Pacific Northwest southeastward to Texas. The high-pressure ridge began to break down on the 13th of November with the rapid approach of a low-pressure system moving into the central U.S. from western Canada. The cold front associated with this system tended to remain east of the Rocky Mountains as it pushed south and east during the day. By the morning of the 14th, the low-pressure cell had moved into the northeast and the cold front extended southwestern through the eastern U.S., into Texas and northeast Mexico, then abruptly northward along the eastern slopes of the Rockies. The cold front had actually passed El Paso during the night from the "back-door", or moving from east to west. The passage was not accompanied by significant weather at WSMR, but broken middle and high clouds were reported. The high-pressure system behind the cold front had moved over WSMR by the morning of the 15th of November and calm winds were reported at many surface stations in the area.

The temperature profiles from rawinsonde observations made at El Paso during the period are shown in Figure 4-1. Inspection of Figure 4-1 shown that the cold front had not reached El Paso by 1700 L on the 13th of November. By 0500 L on the 14th, the cold front had passed El Paso and the thermal inversion occurring at about 800 millibars and associated with the frontal surface persisted in the rawinsonde observations made at 1700 L on the 14th and 0500 L on the 15th of November. Surface observations made at El Paso indicate that relatively shallow

surface-based inversions formed during the nighttime and were eliminated by surface heating during the early morning hours.

Three of the example cases were calculated for 0700 L, 0900 L and 1300 L on the 14th of November to illustrate the performance of the Analysis Phase in analyzing and modifying the 0500 L rawinsonde observation made at El Paso on the 14th and the resulting effects on the concentration and dosage isoplith patterns produced by the Applications Phase of EPAMS. The fourth case was calculated for 0300 L, 15 November to illustrate program performance for very stable light-wind conditions at the surface. These calculations were all made for a hypothetical point source located about 31 kilometers southeast of WSMR using the default values for point source parameters given in Appendix A except the source strength  $Q$  was set to 100 units. The major terrain features of the solution grid are identified in Figure 4-2. The results of the calculations are described below.

5.1 INSTANTANEOUS POINT SOURCE CALCULATIONS FOR 0700L, 0900L  
AND 1300L, 14 NOVEMBER 1974

Program requests were made for dosage and concentration calculations downwind from the hypothetical instantaneous point source southeast of WSMR for 0700L, 0900L and 1300L, 14 November 1974.

Because the request for a solution at 0700L was made for a time less than three hours after the 0500L rawinsonde observation at El Paso, the program used the temperature profile for 0500L shown in Figure 5-1 without modification of the surface, 850 millibar and 700 millibar temperatures and winds to calculate inputs to the mesoscale model. The rawinsonde analysis routine (MIXLYR) ignored the surface-based inversion indicated by the 0500L rawinsonde temperature profile because it was less than 100 meters in depth. Since the elevated inversion with a base at 832 millibars meets the criteria set for determining inversion bases described in Section 3.1, the analysis routine defines the mixing depth as 1697 meters MSL or 491 meters above ground-level (AGL). The height-weighted mean wind components determined from the rawinsonde data below this level were  $u$  equal to  $-4.78 \text{ m sec}^{-1}$  and  $v$  equal  $2.30 \text{ m sec}^{-1}$  or a wind direction of 116 degrees at  $4.8 \text{ m sec}^{-1}$ .

The mesoscale wind-field model solution for 0700L is shown in Figure 5-3. Inspection of Figure 5-3 shows that southeasterly winds dominate the flow pattern in the southern portions of the Tularosa Valley and the valley Jornada Del Muerto west of the Organ Mountains. Since the highest elevations of the San Andres, Organ and Sacramento Mountains extend above the depth of the surface mixing layer, they form an effective barrier to the southeasterly flow and divert the wind flow northward in the northern portion of the Tularosa Valley. The mesoscale wind-field model has set the wind components to zero and reduced the mixing layer to 30 meters above terrain height in the higher elevations, which has resulted in down-



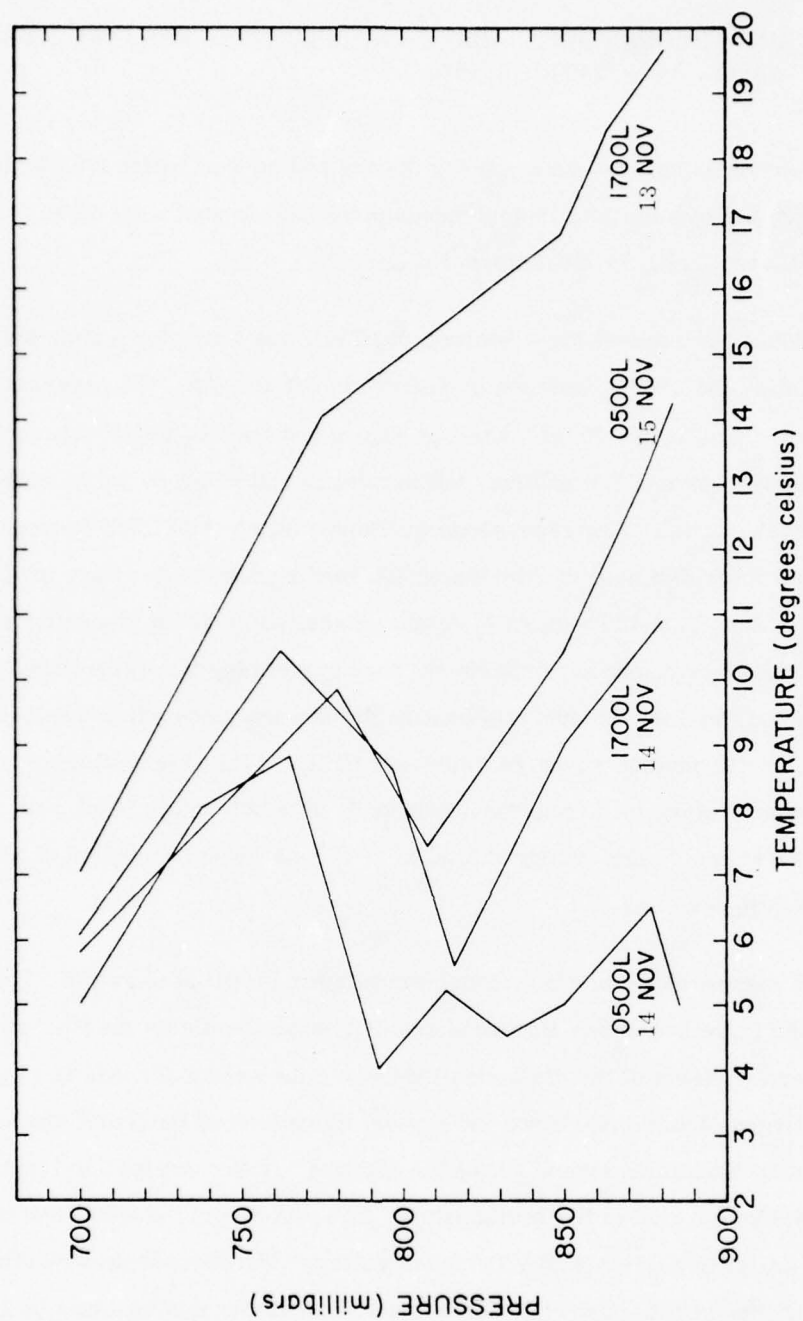


Figure 5-1. Temperature profiles from El Paso, Texas rawinsonde observations for 13, 14 and 15 November 1974.

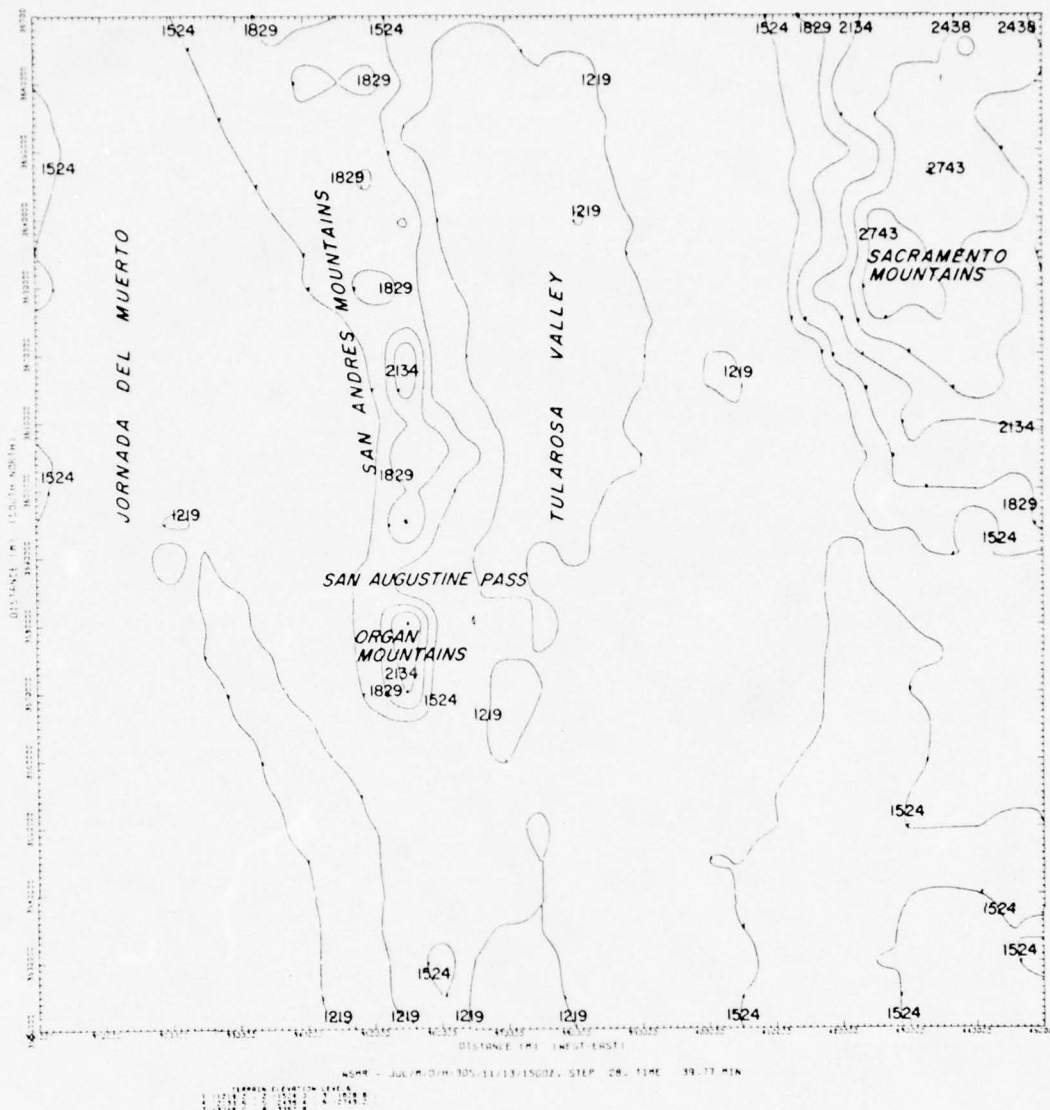


Figure 5-2. Map showing major topographic features of the mesoscale wind-field solution grid.

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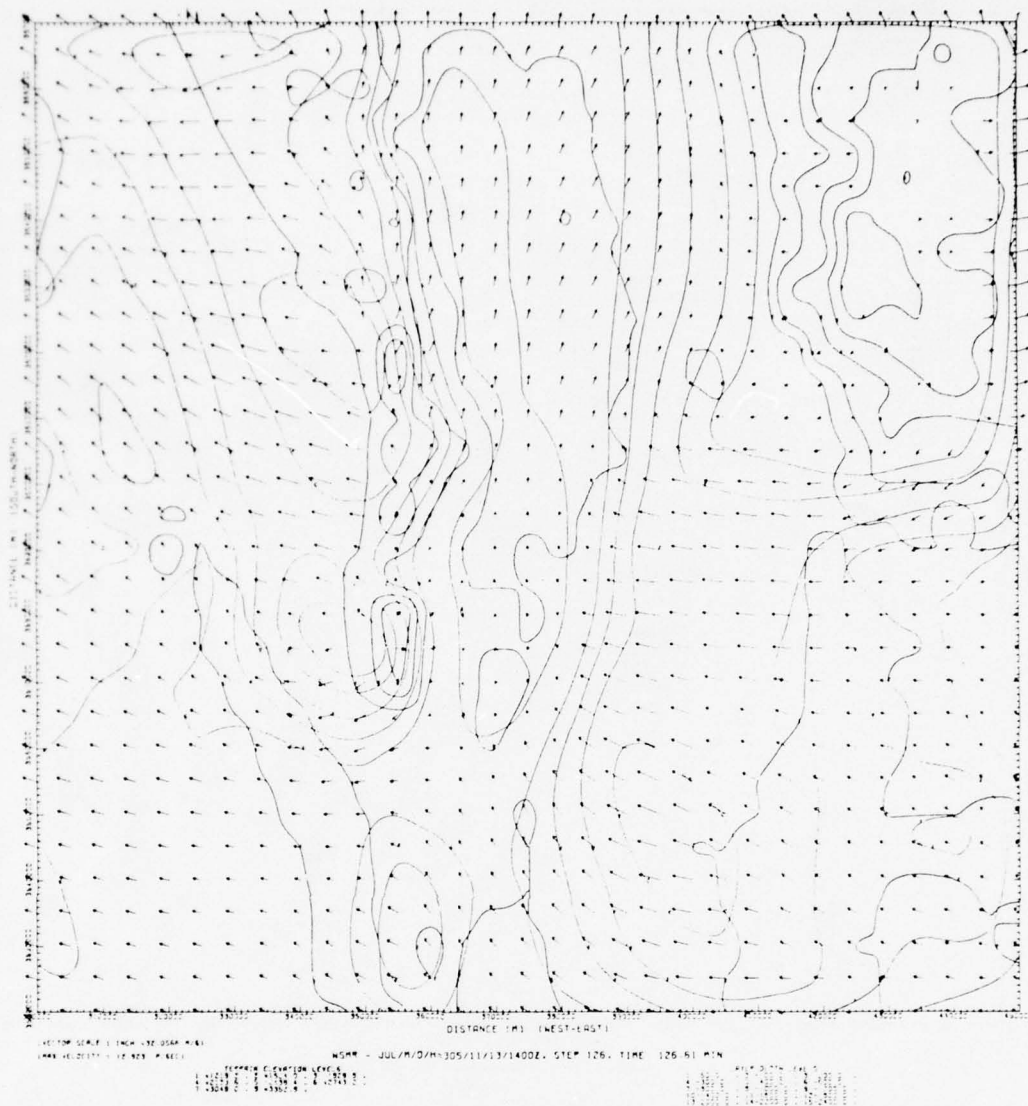


Figure 5-3. Mesoscale wind-field model solution for 0700L, 14 November 1974.

slope flow as evidenced by the flow pattern just east of the Organ Mountains. A typical leeside depression of the mixing depth has formed to the west of the San Andres and Organ Mountains due to hydraulic jump effects and layer thickening has occurred east of the mountains.

The results of the transport/diffusion model calculations for 0700L are shown in Figure 5-4. The cloud trajectory is diverted northward by the downslope flow occurring in the vicinity of the Organ Mountains and follows the south-south-westerly flow through the Tularosa Valley. Concentration isopleths, indicated by the heavier lines in Figure 5-4, are drawn for  $1 \times 10^{-4}$ ,  $1 \times 10^{-6}$  and  $1 \times 10^{-12}$  source units per cubic meter. The dosage isopleths indicated by the thinner lines are drawn for  $1 \times 10^{-4}$ ,  $1 \times 10^{-6}$  and  $1 \times 10^{-12}$  source units per cubic meter. The isopleths were calculated using the diffusion model parametric inputs described in Section 3.2 associated with a net radiation index of -1 since the hour was nighttime, where nighttime is defined in the program as extending from one hour before sunset to one hour after sunrise, and the cloud cover exceeded five-tenths.

The inputs to the mesoscale wind-field model for the 0900L request for transport/diffusion calculations were still based on the 0500L rawinsonde measurement at El Paso, but the rawinsonde observation was modified because the observation was more than three-hours old at 0900L. The modifications made by the mixing-layer analysis routine are shown in Figure 5-5. The routine has inserted the 0900L surface temperature and winds from El Paso and the GWC predicted 700 millibar temperature and winds into the rawinsonde observation and has removed the 0500L temperature and winds observed at the surface and 812, 832, 877 and 700 millibar levels. As a result, the analysis routine calculates a mixing depth of 2099 meters MSL (893 meters AGL) based on the increase in virtual temperature which occurs at 792 millibars. The mean wind components calculated for the mixing layer were  $u$  equal  $-4.87 \text{ m sec}^{-1}$  and  $v$  equal  $1.89 \text{ m sec}^{-1}$ , or a wind direction of 111 degrees at  $5.2 \text{ m sec}^{-1}$ .

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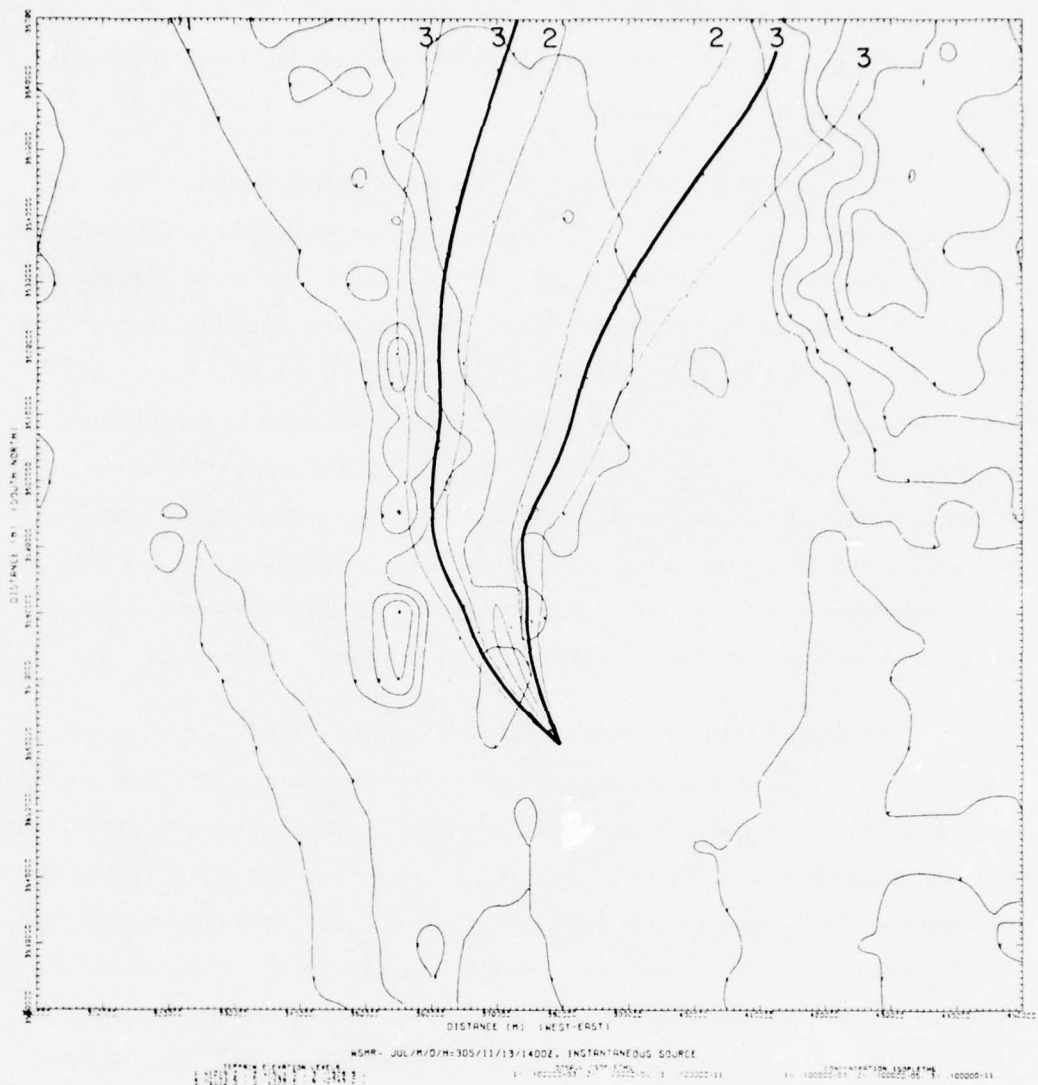


Figure 5-4. Concentration isopleth (heavy line) and dosage isopleths for 0700L, 14 November 1974. Codes for isopleth levels are identified just below the computer plot.



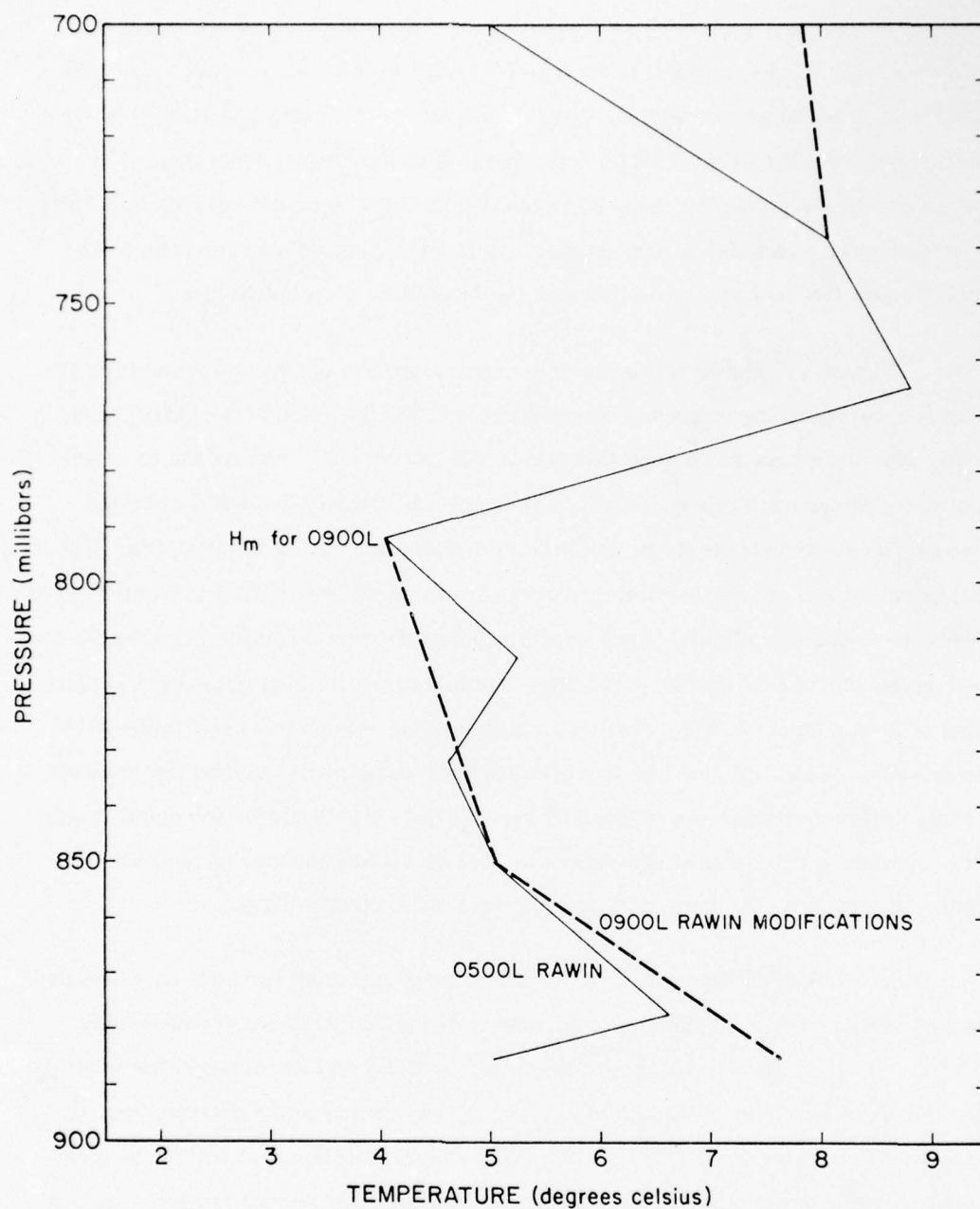


Figure 5-5. El Paso rawinsonde observation at 0500L, 14 November 1974 (solid line) and modifications made by the mixing-layer analysis routine for the 0900L request for a transport/diffusion calculation (broken line).

The mesoscale wind-field model solution for 0900L is shown in Figure 5-6. Since the wind components input to the model at 0900L are nearly identical to those used as inputs for 0700L, the solution shown in Figure 5-6 resembles the solution obtained for 0700L except in the vicinity of the Organ Mountains. The deeper mixing-layer depths obtained in the 0900L solution do not restrict the flow over the Organ Mountains nearly as much as in the 0700L solution and the down-slope flow on the east and south sides of the mountains does not occur.

Figure 5-7 shows isopleths of concentration and dosage calculated for the point source assuming a release occurred at 0900L. The cloud trajectory is no longer affected by the downslope flow that occurred at 0700L and begins to travel westward, is diverted slightly southward around the Organ Mountains and then proceeds west-northwesterly in the Jornada Del Muerto valley flow pattern. The concentration and dosage isopleths, drawn for the same levels used in Figure 5-4 for 0700L, have become slightly more broad in the crosswind direction because the standard deviations of the azimuth wind angle are significantly larger for a net radiation index of 2 used in the 0900L calculations than for the index of -1 used in the 0700L calculations. However, had the calculations been carried-out beyond the confines of the solution matrix shown in Figures 5-4 and 5-7 the isopleths for 0900L would have terminated or closed at shorter downwind distances because of the deeper mixing depths along the trajectory and the increased cloud widths.

The latest rawinsonde data available for performing concentration and dosage calculations for a release at 1300L was still the 0500L El Paso rawinsonde. Since the rawinsonde data was more than six hours old and the criteria for modifying the rawinsonde and GWC data was not met, the mixing-layer analysis routine selected a default value of 1997 m MSL (192 AGL) from Table 3-1 for the mixing depth and the surface wind of 141 degrees at 3 meters per second from the surface observations at El Paso for 1300L. The wind-flow pattern for 1300L produced by the mesoscale model, shown in Figure 5-8, indicates southeasterly flow over the



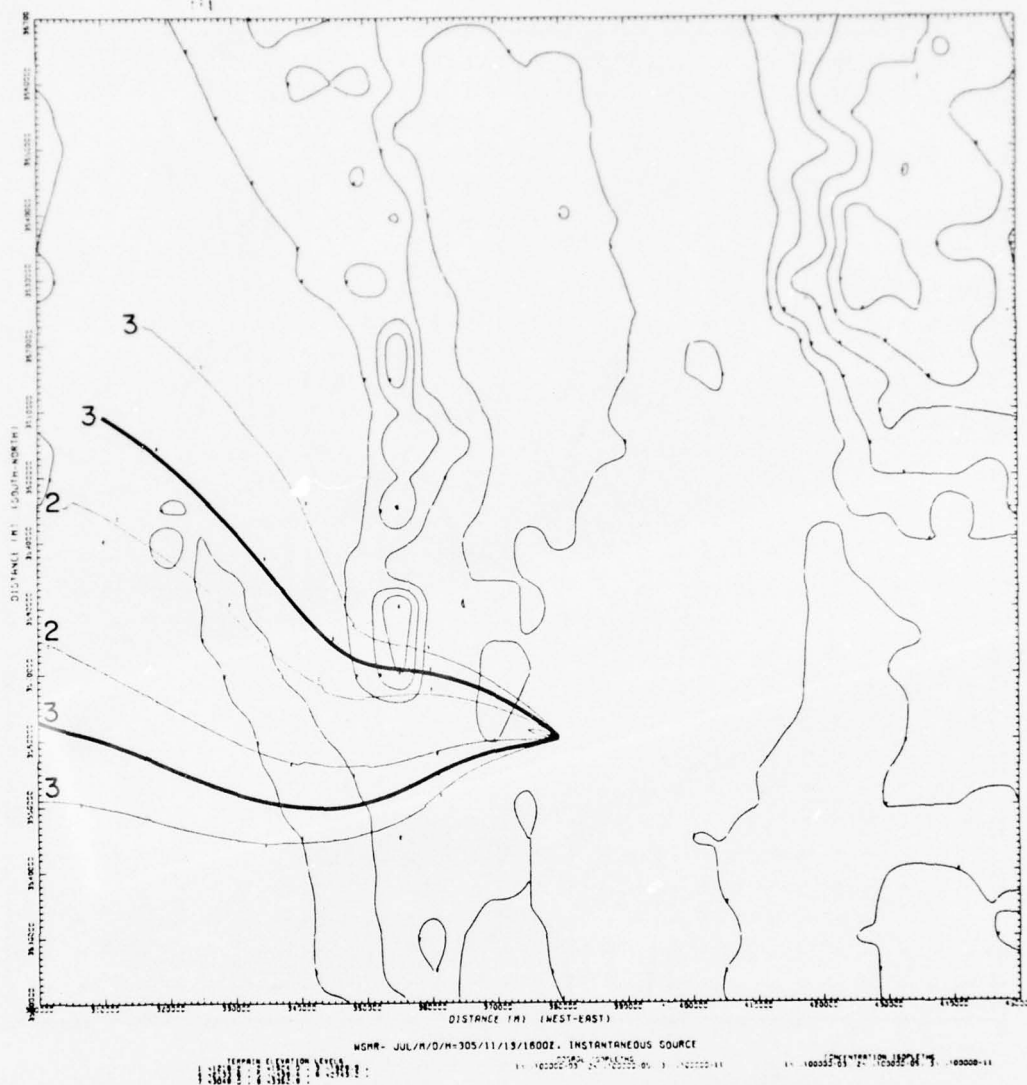


Figure 5-7. Concentration isopleth (heavy line) and dosage isopleths for 0900L, 14 November 1974. Codes for isopleth levels are identified just below the computer plot.

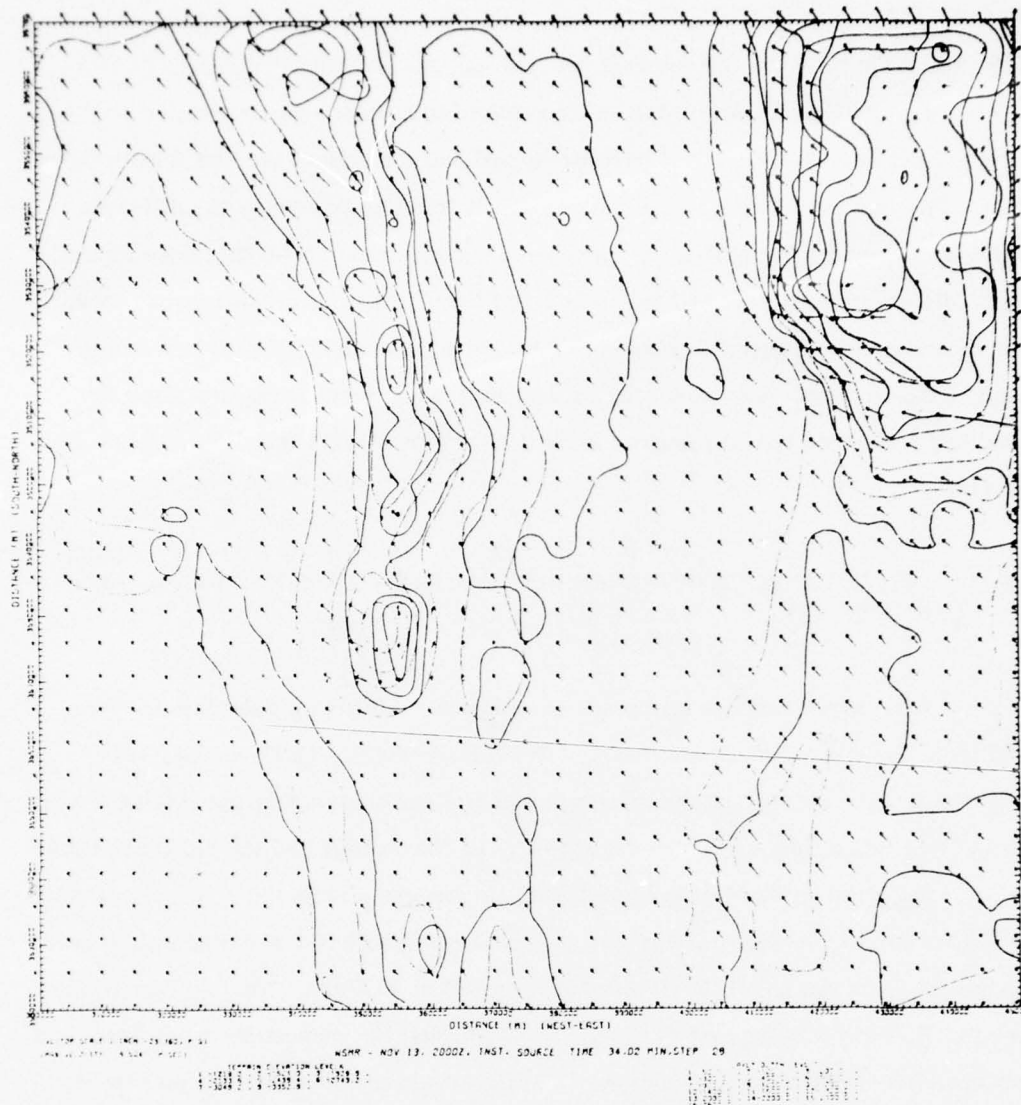


Figure 5- 8. Mesoscale wind-field model solution for 1300L, 14 November 1974.



solution grid except immediately upwind of the San Andres and Organ Mountains and in the vicinity of the Sacramento Mountains. As indicated in Figure 5-9 showing the concentration and dosage isopleths for a point source release at 1300L, the cloud trajectory is directed northwestward and intersects the San Andres Mountains. The isopleths begin to expand rapidly at this point because the diffusion model compensates for attempted increases in concentration (in this case caused by rapidly decreasing mixing layer depth and insufficient increase in wind speed to compensate for reduced mixing depth) by increasing cloud dimensions in the plane of the horizon. The isopleths expand in a more regular fashion after the cloud has traversed the San Andres Mountains and reached the valley Jornada De Muerto.

#### 5.2 INSTANTANEOUS POINT SOURCE CALCULATIONS FOR 0300L, 15 NOVEMBER 1974

A program request was made for transport/diffusion calculations downwind from the point-source southeast of WSMR for 0300L, 15 November 1974. Since the latest rawinsonde observation available for analysis by the mixing-layer routine was more than six hours old (1700L, 14 November) and the GWC prediction data was rejected on temperature criteria, the program selected a default value of 30 meters for the surface mixing-layer depth from Table 3-1 and a default wind component from the 0300L surface wind reported at El Paso. The surface wind speed at El Paso was reported as calm at 0300L and the mesoscale wind field model was initialized with zero momentum. The flow-field produced by the mesoscale model is shown in Figure 5-10. As indicated in the figure, downslope flow is occurring everywhere, but is greater west of the Sacramento Mountains and in the region just east of San Augustine Pass separating the Organ and San Andres Mountains. The cloud, as indicated in Figure 5-11 by the isopleth patterns, begins to move southwestward for a few kilometers, then moves toward the low elevations in the Tularosa

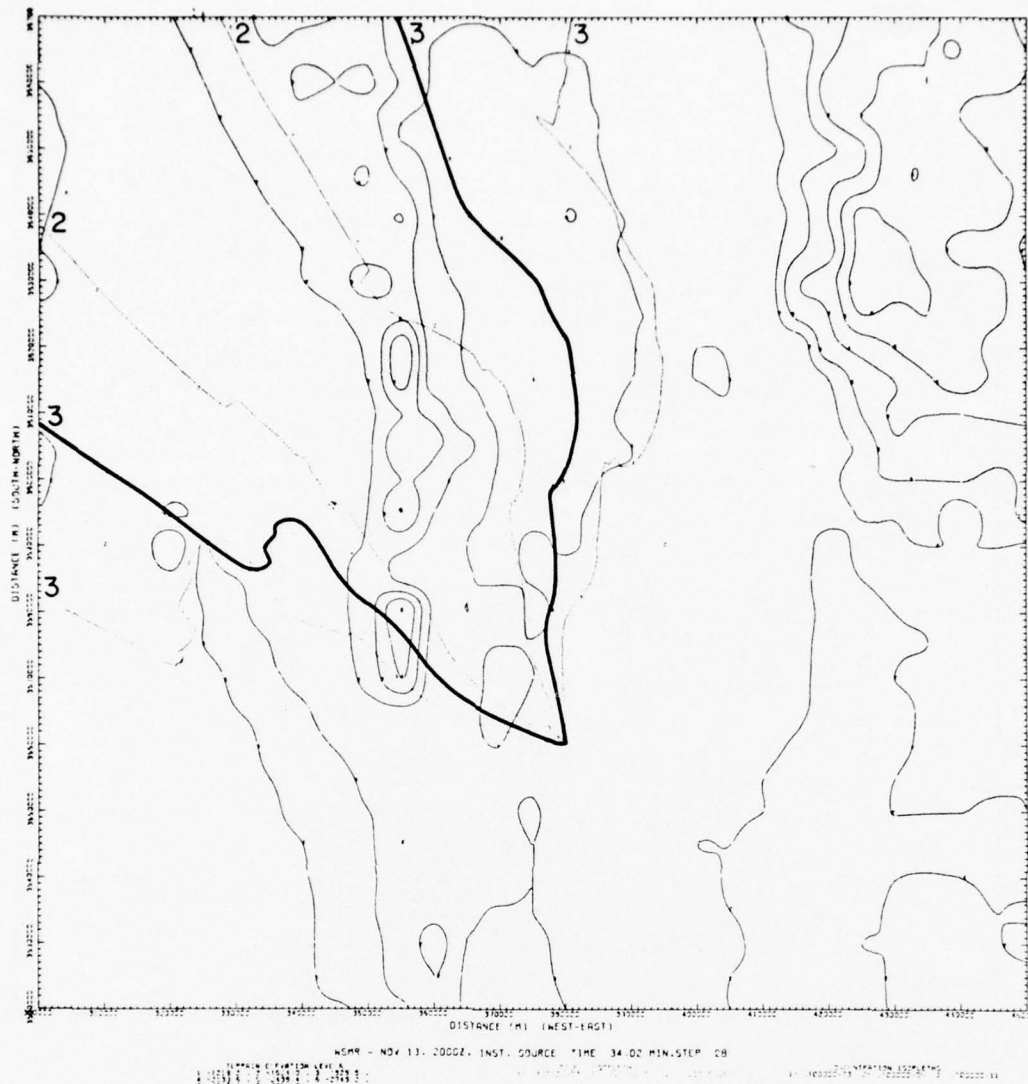


Figure 5-9. Concentration isopleth (heavy line) and dosage isopleths for 1300L, 14 November 1974. Codes for isopleth levels are identified just below the computer plot.

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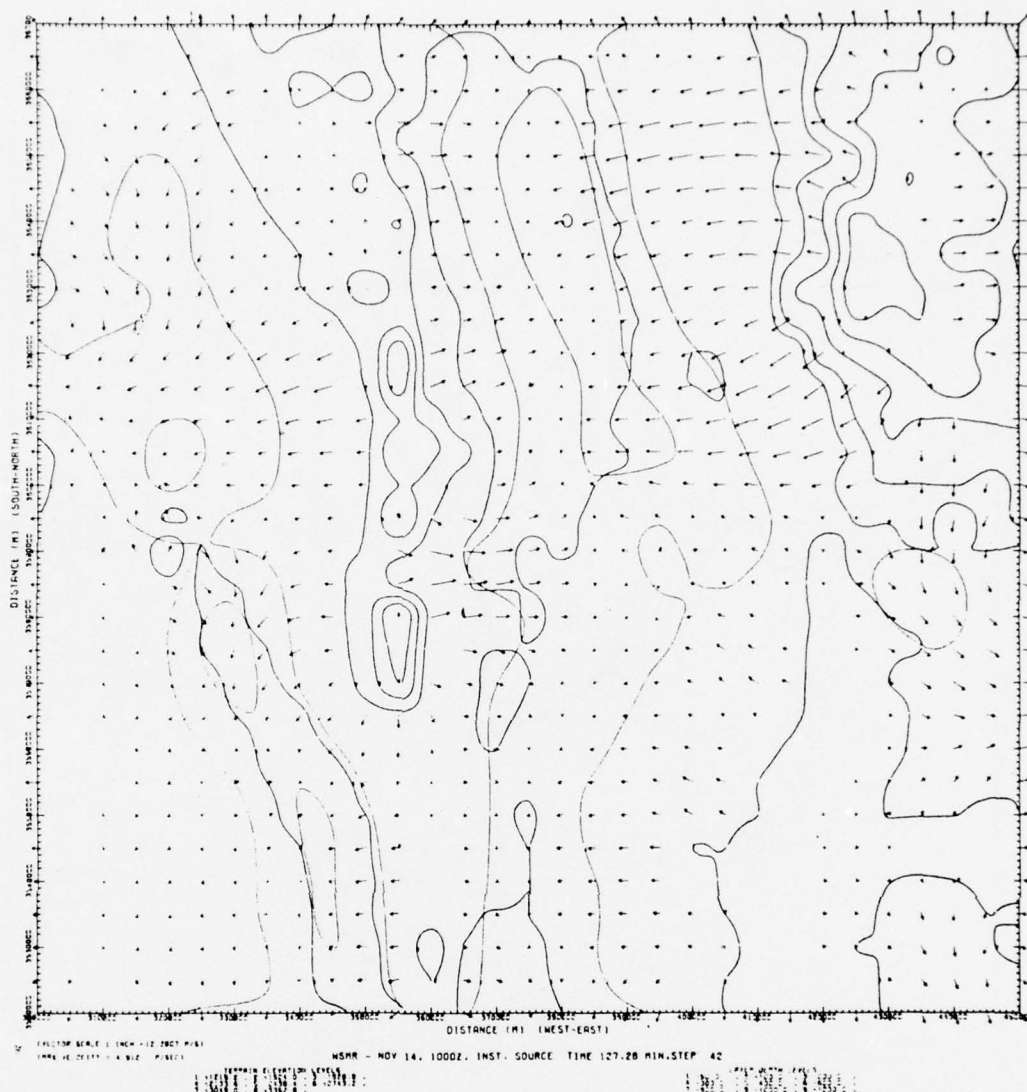


Figure 5-10. Mesoscale wind-field model solution for 0300L, 15 November 1974.

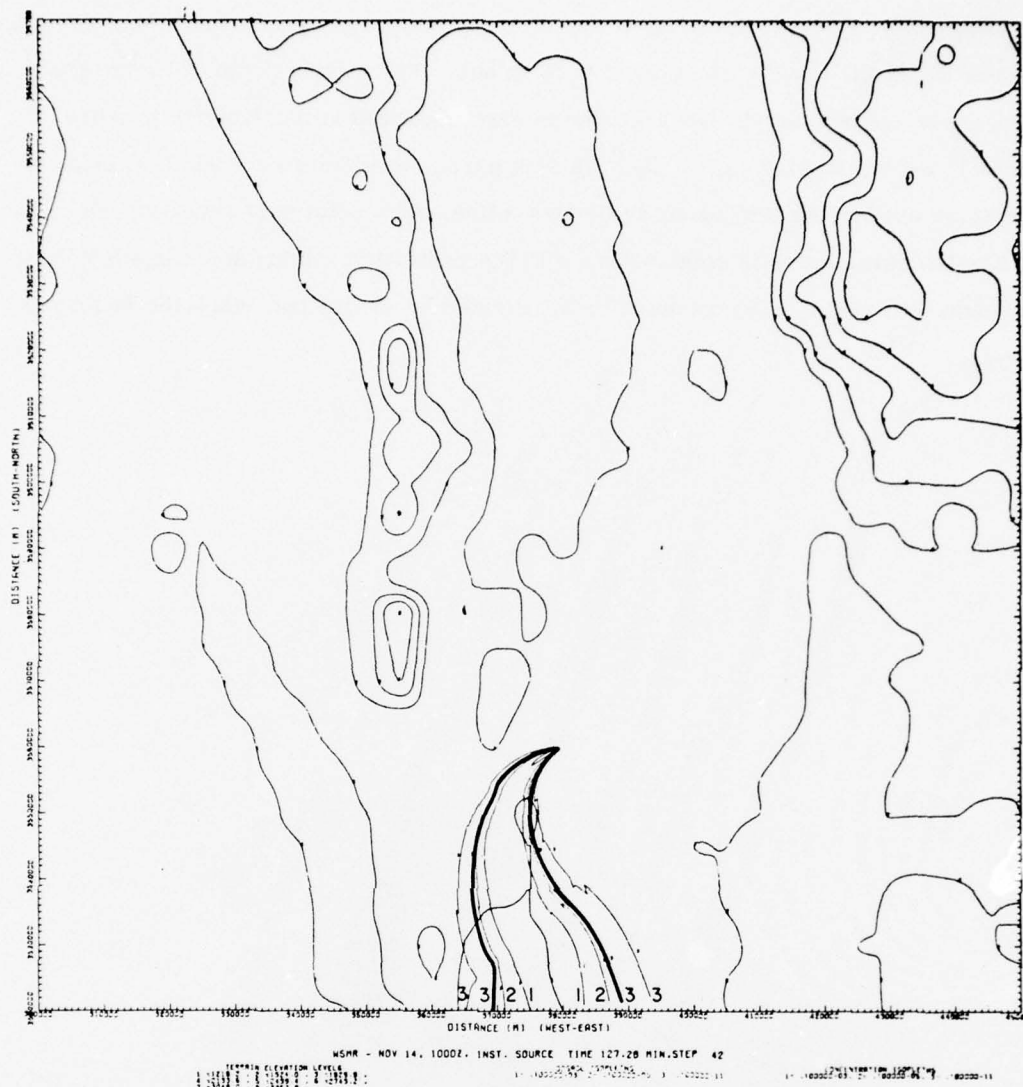


Figure 5-11. Concentration isopleth (heavy line) and dosage isopleths for 0300L, 15 November 1974. Codes for isopleth levels are identified just below the computer plot.



Valley at the southern boundary of the solution matrix grid. The highest wind speed along the cloud trajectory of  $0.86 \text{ m sec}^{-1}$  and mixing depth of 79 meters occurs at the boundary. Because the release occurred at nighttime with more than five-tenths cloud cover, the diffusion parameters for a net radiation index of -1 were used in the transport/diffusion routine. The relatively small values of the diffusion parameters in combination with the restricted mixing depth and low wind speeds lead to the high concentrations indicated by the narrow isopleths in Figure 5-11.



## REFERENCES

- Briggs, G. A., 1971: Some recent analyses of plume rise observations. In Proceedings of the Second International Clean Air Congress, Academic Press, New York.
- Briggs, G. A., 1972: Chimney plumes in neutral and stable surroundings. Atm. Env., 6(7), 507-510.
- Carnahan, Luther, and Wilkes, 1969: Applied Numerical Methods. Wiley and Sons, Inc., New York, New York.
- Cramer, H. E., et al., 1972: Development of dosage models and concepts. Technical Report, Contract No. DAAD09-67-6-6-0020(R), Desert Test Center, Fort Douglas, Utah.
- Dumbauld, R. K., et al., 1970: Handbook for estimating toxic fuel hazards. Final Report under Contract No. NAS8-21453, NASA Report No. CR-61326.
- Dumbauld, R. K., J. R. Bjorklund and J. F. Bowers, 1973: NASA/MSFC multi-layer diffusion models and computer program for operational prediction of toxic fuel hazards. NASA Contractor Report NASA CR-129006. H. E. Cramer Company Technical Report prepared for National Aeronautics and Space Administration, George C. Marshall Space Flight Center, Alabama 35812.
- Holzworth, G. C., 1967: Estimates of mean maximum mixing depths in the contiguous United States, Mon. Wea. Rev., 92, 235-242.
- Lavoie, R. L., 1972: A mesoscale numerical model of lake-effect storms. J. Atm. Sci., 29(6), 1025-1040.
- Norton, C. and G. Hoidale, 1975: The diurnal variation of mixing depth by month over White Sands Missile Range, N. M. Research and Development Technical Report ECOM-5579, Atmospheric Sciences Laboratory, U. S. Army Electronics Command, White Sands Missile Range, New Mexico 88002.
- Pasquill, F., 1962: Atmospheric Diffusion. D. Van Nostrand Co., Ltd., London, 297.
- Shapiro, R., 1970: Smoothing, filtering and boundary effects. Reviews of Geophysics and Space Physics, 8(2), 359-387.

- Swanson, R. N. and M. M. Hoidale, 1962: Low-level wind profile prediction techniques. Progress Report 4, SMSA, White Sands Missile Range, New Mexico.
- Swanson, R. N. and H. E. Cramer, 1965: A study of lateral and longitudinal intensities of turbulence. J. Appl. Met., 4, 409-417.
- Tingle, A. G. and J. R. Bjorklund, 1973: Study and investigation of computer algorithms for the solution of the shallow-fluid equations as a means of computing terrain influences on wind fields. H. E. Cramer Company Technical Report TR-73-302-01 prepared under Contract No. DAAD07-73-C-0309 with ASL, ECOM, White Sands Missile Range, New Mexico.
- Turner, D. B., 1964: A diffusion model for an urban area. J. Appl. Meteor., 3(1), 83-91
- Woolf, H. M., 1968: On the computation of solar elevation angles and the determination of sunrise and sunset times. NASA TMX-1646. National Meteorological Center, ESSA, Hillcrest Heights, Maryland.

APPENDIX A  
USERS' INSTRUCTIONS FOR THE ANALYSIS,  
APPLICATION AND GRAPHICS  
PHASES OF EPAMS

This appendix gives users' instructions for the three main phases of EPAMS. The computer programs that comprise the many phases of EPAMS are written in FORTRAN V and are designed for use on a Univac 1108 computer. A complete listing of the EPAMS computer program is given in Appendix B. Also, a block diagram of the main components of each phase of EPAMS, as well as, temporary executive routines is given in Section 4 of the main body of this report. The program has been delivered to WSMR with three dummy executive routines, these routines are shown as XECAMS, ANALIZ and APPLY in Figure 4-1, Section 4. The final design of these routines is not the responsibility of the H. E. Cramer Company and as such they are only presented here for completeness and to provide temporary drivers for the Analysis, Application and Graphics Phases. See Section A.7 below for data file numbers assigned by the temporary executive XECAMS.

The input variables required in the temporary executive XECAMS are described in Section A.1 below. Also, optional input variables for the Analysis, Application and Graphics Phases are given in Sections A.2, A.3, and A.4, respectively. An example execution card deck is given in Section A.5 and the input data method used in the Analysis, Application and Graphics Phases is given in Section A.6

A.1 EPAMS EXECUTIVE INPUTS

The temporary executive XECAMS requires data input via the EPAMS input message file to direct the executive to execute one of the three phases of EPAMS. The set of variables given below are read by XECAMS prior to the execution of any of the EPAMS phases. One data card is read for each phase and only those variables

required by the particular phase need be input. A summary table of the input variables and their respective units and default values is given in Table A-1.

<u>FORTTRAN VARIABLE</u>	<u>FORMAT</u>	<u>CARD COLUMNS</u>	<u>DEFINITION</u>
TYPE 1	I3	1-3	This integer variable is used to direct the executive to execute one of the EPAMS Phases. If set equal to 2, the Analysis Phase is executed and XECAMS calls the Analysis Supervisor ANALIZ. If set equal to 1, the Application Phase is executed and XECAMS calls the Application Supervisor APPLY. If set equal to 4 the Graphics Phase is executed and XECAMS calls the Graphics Supervisor PLTPRG. (This variable is referenced only in the executive XECAMS.)
TYPE 2	I3	4-6	This integer variable is used to execute alternate sections of the Analysis and Application Phases. If set equal to 1 or 2 and TYPE1 equals 2, the mixing layer and mesoscale wind field programs of the Analysis Phase are executed by a call to the mixing layer and mesoscale wind field programs. If set equal to 1 and TYPE 1 equals 1, the transport/diffusion programs of the

TABLE A-1  
SUMMARY TABLE OF INPUT VARIABLES  
FOR THE EPAMS TEMPORARY  
EXECUTIVE XECAMS

FORTRAN VARIABLE	UNITS	FORMAT	CARD COLUMNS	LIMITS	DEFAULT VALUE
TYPE 1	N/A	I3	1-3	= 1, 2 or 4	N/A
TYPE 2	N/A	I3	4-6	= 1 or 2	N/A
TYPE 3	N/A	I3	7-9	$\geq -9$ and $\leq 9$	0
JULIAN	Julian Day	I3	10-12	= end of last month	N/A
MONTH	Month	I3	13-15	$\geq 1$ and $\leq 12$	N/A
DAY	Day	I3	16-18	$\geq 1$ and $\leq 31$	N/A
HOUR	Hour (GMT)	I3	19-21	$\geq 00$ and $\leq 23$	N/A
MINUTE	Minute	I3	22-24	$\geq 00$ and $\leq 60$	N/A
XPLACE	Meters	F10.2	25-34	$\geq 300000$ and $\leq 450000$	360000
YPLACE	Meters	F10.2	35-44	$\geq 3520000$ and $\leq 3670000$	3585000
ZPLACE	Meters	F10.2	45-54	$\geq 1310$	1310



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CRAMER (H E) CO INC SALT LAKE CITY UTAH  
MIXING-LAYER ANALYSIS ROUTINE AND TRANSPORT/DIFFUSION APPLICATI--ETC(U)  
MAR 77 R K DUMBAULD, J R BJORKLUND

F/G 4/2

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<u>FORTRAN VARIABLE</u>	<u>FORMAT</u>	<u>CARD COLUMNS</u>	<u>DEFINITION</u>
TYPE 2 (Continued)			Application Phase are executed by a call to program TRYDIF. TYPE 2 is not referenced in the Graphics Phase.
TYPE 3	I3	7-9	<p>This integer variable is used to control input data to parts of the Analysis, Application and Graphics Phases. If TYPE 3 is set less than or equal to zero, no input data is read by the particular phase being executed. The programs will default or calculate all potential input data variables.</p> <p>Specifically if TYPE 3 is positive (greater than zero) and the mixing layer/mesoscale section of the Analysis Phase is being executed, the data variables given in Section A. 2 are input via EPAMS file XINFIL (data card input). If the absolute value of TYPE 3 is equal to 9, the program only executes the mixing layer solution. This option is used only to display meteorological data and no solution files are generated or altered.</p> <p>If TYPE 3 is positive (greater than zero), and the transport/diffusion</p>

<u>FORTRAN</u> <u>VARIABLE</u>	<u>FORMAT</u>	<u>CARD</u> <u>COLUMNS</u>	<u>DEFINITION</u>
TYPE3 (Continued)			<p>section of the Application Phase is being executed, the data variables given in Section A.3 are input via EPAMS file XINFIL (data card). If TYPE3 is zero, the program defaults to an instantaneous source with no input data. If equal to -1 the program defaults to a continuous SO<sub>2</sub> source given by the ASARCO copper stack in El Paso, Texas. If equal to -2, the program defaults to a continuous SO<sub>2</sub> source given by the ASARCO lead stack in El Paso, Texas.</p> <p>If TYPE3 is positive (greater than zero) and the Graphics Phase is being executed, the variables given in Section A.4 are input via EPAMS file XINFIL (data card).</p> <p>If any of the three phases of EPAMS cannot complete its task, the particular phase will set TYPE3 equal to a negative number and return control to the executive routines. If the phase solution was completed TYPE3 is greater than or equal to zero upon return.</p>

<u>FORTTRAN VARIABLE</u>	<u>FORMAT</u>	<u>CARD COLUMNS</u>	<u>DEFINITION</u>
JULIAN	I3	10-12	The Julian day of the last day of the month prior to the month of the desired solution date and time. (Referenced only in Analysis Phase.)
MONTH	I3	13-15	Month of the desired solution. (Referenced only in Analysis Phase.)
DAY	I3	16-18	Day of the desired solution. (Referenced only in Analysis Phase.)
HOUR	I3	19-21	Hour of the desired solution (past, present or future) in Greenwich mean time (00 to 23). (Referenced only in Analysis Phase.)
MINUTE	I3	22-24	Minute of the desired solution (00 to 60). (Referenced only in the Analysis Phase.)
XPLACE	F10.2	25-34	The UTM (Universal Transvers Mercator) easterly (x) coordinate of the source location in meters. If equal to blank or zero, the program uses 360000 meters.
YPLACE	F10.2	35-44	The UTM northerly (y) coordinate of the source location in meters. If equal to blank or zero, the program uses 3585000 meters.



<u>FORTRAN VARIABLE</u>	<u>FORMAT</u>	<u>CARD COLUMNS</u>	<u>DEFINITION</u>
ZPLACE	F10.2	45-54	The elevation (MSL) of the source location in meters. If equal to blank or zero, the program uses 1310 meters.

## A.2 ANALYSIS PHASE INPUTS

This section describes the variables input to the mixing layer part of the Analysis Phase. The variables given below are read only if the variable TYPE3 from the executive is positive (greater than zero). These variables are read in the FORTRAN namelist format through namelist QLST1 via EPAMS file XINFIL (data card). The namelist format is explained in Section A.6 below. A summary table of the input variables is given with their respective units and default values in Table A-2. Possible input variables are:

<u>FORTRAN VARIABLE</u>	<u>DEFINITION</u>
UN	Vector component $u$ of the mean layer wind for use in the mesoscale wind field calculation in units of meters/second. The component $u$ is positive toward the east and negative toward the west. (Default = calculated from the meteorological data base.)

$$UN = V \cdot \sin(\theta \pm 180.0)$$

where  $V$  = mean layer wind speed  
 $\theta$  = mean layer wind direction  
measured from 0 degrees  
north clockwise (direction  
from which wind is blowing)



TABLE A-2  
SUMMARY TABLE OF THE INPUT VARIABLES  
FOR THE ANALYSIS PHASE INPUT  
THROUGH NAMELIST QLST1

FORTTRAN VARIABLE	UNITS	LIMITS	DEFAULT VALUE <sup>①</sup>	INITIAL VALUE
UN	Meters/ Second	>-99.0	②	-99
VN	Meters/ Second	>-99.0	②	-99
PN	Meters (MSL)	≥1340	②	-99
GN	Meters/ Second <sup>2</sup>	>-99.0	②	-99
ABLKN	Meters	≥30	30 Meters	30.0
SURFTN	OK	>-99.0	②	-99
PØTMPN	OK	>-99.0	②	-99
ZELEVN	Meters (MSL)	>-99.0	②	-99
DTLMDN	Fraction	>0 and <1	0.4	0.4
ISMTHN	Integer	≥0 and ≤25	7	7
NCNTN	Integer	≥0	2	2

(Table A-2 continued on following page.)

① If the variable is equal to or less than the initial value the variable is set equal to the default value.

② These variables are normally calculated from the EPAMS data base. They are given as input variables to provide the capability to override calculated quantities.

TABLE A-2 (Continued)

FORTTRAN VARIABLE	UNITS	LIMITS	DEFAULT VALUE <sup>①</sup>	INITIAL VALUE
NETRDN	Index	$\geq -2$ and $\leq 4$	2	-9
KFLG1	Switch	0 or 1	0	0
KFLG2	Switch	0 or 1	0 or if TYPE 3=9 then 1	0

<sup>①</sup> See previous page for footnote.

FORTTRAN  
VARIABLE

DEFINITION

VN	Vector component $v$ of the mean layer wind for use in the mesoscale wind field calculations in meters/second. The component $v$ is positive toward the north and negative toward the south. (Default = calculated from the meteorological data base.)  $VN = V \cdot \cos (\theta \pm 180.0)$
PN	Elevation (MSL) of the surface mixing layer above the meteorological station (if available) or source location in meters. (Default = calculated from the meteorological data base.)
GN	Reduced gravity parameter for use in the meso-scale wind field calculations in units of meters/second <sup>2</sup> . See Page 6, Section 2 of the main body of this report. (Default = calculated from the meteorological data base.)
ABLKN	Minimum surface mixing layer depth constraint in meters. This parameter must be greater than zero. (Default = 30 meters.)
SURFTN	Surface temperature in degrees kelvin. (Default = determined from the meteorological data base.)
PØTMPN	Array containing the potential temperature at a maximum of 25 levels in degrees kelvin. (Default = determined from the meteorological data base.)
ZELEVN	Array containing the elevation (MSL) in meters of each of the values input into PØTMPN. (Default = determined from the meteorological data base.)
DTLMDN	Mesoscale model solution stability parameter shown in Equation 2-4 in the main body of this report. (Default = 0.4.)

<u>FORTTRAN VARIABLE</u>	<u>DEFINITION</u>
ISMTHN	Number of mesoscale model time iterations between applications of a nine-point low-pass filter. (Default = 7, filtered every 7th step.)
NCNTN	Number of mesoscale model time iterations between recalculations of the model time increment constant. (Default = 2, recalculated every 2nd step.)
NETRDN	Net radiation index as defined in Section 3.2 in the main body of this report. (Default = calculated from the meteorological data base.)
KFLG1	Switch to control the initialization of the mesoscale model. If set equal to zero, the program will initialize the mesoscale model with a cold or hot start according to the rules given in Section 4.1 of the main body of this report. If KFLG1 is set equal to 1, the program forces a cold start, i.e., the model is initialized with the constant momentum field calculated from UN, VN and PN above. (Default = 0.)
KFLG2	Switch to control the print output from the Analysis Phase. If set equal to 0, only completion messages are output to the EPAMS output file XOTFIL (printer). If set non-zero, the Analysis Phase prints detailed tables of the meteorological data used and solution characteristics of the mesoscale model. If the absolute value of TYPE3 defined in Section A.1 is equal to 9, KFLG2 is automatically set non-zero. However, no mesoscale output is produced. (Default = 0.)

### A.3 APPLICATION PHASE INPUTS

This section describes the variables that are input to the transport/diffusion section of the Application Phase. The variables given below are read only if TYPE3



from the executive is positive (greater than zero). These variables are read in the FORTRAN namelist format through namelist QLST2 via EPAMS input file XINFIL. A summary table of the input variables is given with their respective default values in Table A-3. Possible input variables are:

<u>FORTTRAN VARIABLE</u>	<u>DEFINITION</u>
XSØUR	UTM easterly (x) coordinate of the source location in meters. (Default = value used in Analysis Phase or if continuous source 1 or 2 is specified = 356000 meters (ASARCO).)
YSØUR	UTM northerly (y) coordinate of the source location in meters. (Default = value used in Analysis Phase or if continuous source 1 or 2 is specified = 3520100 meters (ASARCO).)
ZSØUR	Elevation (MSL) of the surface at the source location in meters. (Default = value used in Analysis Phase or if continuous source 1 or 2 is specified = 1150.6 meters (ASARCO).)
Q	Source strength of source. Input in units of total material released if an instantaneous source or total material per second if a continuous source. (Default = 1 if an instantaneous source, = 2520 g/second SO <sub>2</sub> if continuous source 1 (ASARCO Copper), = 1764 g/second SO <sub>2</sub> if continuous source 2 (ASARCO lead).)
SIGXØ	Standard deviation of the alongwind source distribution after cloud stabilization for instantaneous sources only. Input in units of meters. (Default = 0.)
SIGYØ	Standard deviation of the crosswind source distribution after cloud stabilization for instantaneous sources only. Input in units of meters. (Default = 0.)



TABLE A-3  
SUMMARY TABLE OF THE INPUT VARIABLES  
FOR THE APPLICATION PHASE INPUT  
THROUGH NAMELIST QLST2

FORTTRAN VARIABLE	UNITS	LIMITS	DEFAULT VALUE <sup>②</sup>
XSØUR	Meters	$\geq 300000$ and $\leq 450000$	XPLACE
YSØUR	Meters	$\geq 3520000$ and $\leq 3670000$	YPLACE
ZSØUR	Meters	$\geq 1340$	ZPLACE
Q	①	$> 0$	=1 if KINDSØ = 0 =2520 g/sec. if KINDSØ = 1 =1764 g/sec. if KINDSØ = 2
SIGXØ	Meters	$\geq 0$	0
SIGYØ	Meters	$\geq 0$	0
SIGZØ	Meters	$\geq 0$	0
H	Meters	$\geq 0$	=0 if KINDSØ = 0 =252.4 if KINDSØ = 1 =186.5 if KINDSØ = 2

(Table A-3 continued on following page.)

① The source strength input unit is total material released for instantaneous sources (KINDSØ = 0) or total material released per second for continuous sources (KINDSØ > 0). If the source strength is input as grams for instantaneous sources or grams per second for continuous sources, the output concentration units are grams per cubic meter and dosage units are gram seconds per cubic meter. Dosage is calculated only for instantaneous sources.

② If the value of the variable is less than or equal to zero, the variable is set equal to the default value.

TABLE A-3 (Continued)

FORTTRAN VARIABLE	UNITS	LIMITS	DEFAULT VALUE <sup>②</sup>
Z	Meters	$\geq 0$	0
TUA	Seconds	$\geq 0$	2.5
ALPHA	Fraction	$> 0$	1
BETA	Fraction	$> 0$	1
KINDSØ	Integer	$\geq 0$	=0 if TYPE 3 $\geq 0$ =1 if TYPE 3 = -1 =2 if TYPE 3 = -2
DECAY	Fraction	$\geq 0$	0
BLAMDA	Fraction	$\geq 0$	0
GAMMA	Fraction	$\geq 0$	1
STTEMP	°K	$\geq$ Ambient Air	=366.3 if KINDSØ = 1 =352.4 if KINDSØ = 2
RADIUS	Meters	$> 0$	=4.877 if KINDSØ = 1 =3.658 if KINDSØ = 2
EXTVEL	Meters/ Second	$\geq 0$	=2.1476 if KINDSØ = 1 =2.7512 if KINDSØ = 2
VS	Meters/ Second	$\geq 0$	0
CØNISS	Concentration Output Units	$\geq 0$	$1 \times 10^{-4}$ , $1 \times 10^{-6}$ and $1 \times 10^{-12}$
DØSISS	Dosage Output Units	$\geq 0$	$1 \times 10^{-4}$ , $1 \times 10^{-6}$ and $1 \times 10^{-12}$

(Table A-3 continued on following page.)

<sup>②</sup>See previous page for footnote.

TABLE A-3 (Continued)

FORTTRAN VARIABLE	UNITS	LIMITS	DEFAULT VALUE <sup>②</sup>
TEMPSF	<sup>o</sup> K	<u>&gt;</u> 0	Historical Data
RTLAPS	<sup>o</sup> K/Meter	<u>&gt;</u> 0	Historical Data
KFLG1	Integer	= 0 or 1	0
KFLG2	Integer	= 0 or 1	0

<sup>②</sup>See previous page for footnote.

FORTRAN  
VARIABLE

DEFINITION

SIGZØ	Standard deviation of the vertical source distribution after cloud stabilization for instantaneous sources only. Input in units of meters. (Default = 0.)
H	Source emission release height above ground if a continuous source or effective height above ground after cloud stabilization for instantaneous sources. Input in meters. (Default = 0 if instantaneous, = 252.4 meters if continuous source 1 (ASARCO Copper), = 186.5 meters if continuous source 2 (ASARCO Lead).)
Z	Height in meters above ground at which concentration and/or dosage is to be calculated. (Default = 0.)
TAU	Source emission time in seconds for instantaneous sources only. (Default = 2.5 seconds.)
ALPHA	Crosswind diffusion coefficient. (Default = 1.)
BETA	Vertical diffusion coefficient. (Default = 1.)
KINDSØ	Source type switch, where if KINDSØ = 0, the program assumes an instantaneous source. If KINDSØ is greater than zero, the program assumes a continuous source. If set equal to 1, the program assumes a continuous source 1 which is the copper smelter stack at ASARCO, El Paso, Texas. If set equal to 2, the program assumes a continuous source which is the lead smelter stack at ASARCO El Paso, Texas. (Default = 0.)
DECAY	Coefficient of time dependent decay input as a fraction. (Default = 0.)
BLAMDA	Coefficient of precipitation scavenging input as a fraction. (Default = 0.)



FORTRAN VARIABLE	DEFINITION
GAMMA	Coefficient of vertical reflection input as the fraction of material reflected at the surface. (Default = 1.)
STTEMP	Stack effluent exit temperature in degrees Kelvin for continuous sources only. (Default = 366.3 °K if continuous source 1, = 352.4 if continuous source 2, no default is provided for KINDSØ > 2.)
RADIUS	Internal stack radius in meters for continuous sources only. (Default = 4.877 meters for continuous source 1, = 3.658 meters for continuous source 2. No default is provided for KINDSØ > 2.)
VS	Particle or droplet settling velocity in meters/second for concentration and/or dosage with depletion due to gravitational deposition. (Default = 0.)
CØNISS	Array of a maximum of 3 concentration values for which concentration isopleth half widths are to be calculated. (Default = $1 \times 10^{-4}$ , $1 \times 10^{-6}$ and $1 \times 10^{-12}$ .)
DØSISS	Array of a maximum of 3 dosage values for which dosage isopleth half widths are calculated for instantaneous sources only. (Default = $1 \times 10^{-4}$ , $1 \times 10^{-6}$ and $1 \times 10^{-12}$ .)
TEMPSF	Surface temperature in degrees Kelvin for continuous source only. (Default = calculated in Analysis Phase or from historical data.)
RTLAPS	Lapse rate of potential temperature in degrees Kelvin/meter for continuous sources only. (Default = calculated from elevation and potential temperature provided by the Analysis Phase or from historical data.)
KFLG1	Mesoscale model solution switch. If set equal to 0, the program will calculate the source cloud trajectory from the present or most current mesoscale



<u>FORTRAN VARIABLE</u>	<u>DEFINITION</u>
KFLG1 (Continued)	wind field solution. If non-zero, the program will use the past mesoscale solution. (Default = 0.)
KFLG2	Detail print output switch. If equal to zero, the program writes to the EPAMS output file the calculated concentration, dosage, standard deviation of the lateral concentration distribution and the isopleth half widths at each trajectory point. If non-zero, the program also outputs the trajectory points with the wind speed, surface layer depth, time and total distance. (Default = 0.)

#### A.4 GRAPHICS PHASE INPUTS

This section describes the variables that are input to the Graphics Phase. The variables given below are read only if TYPE3 from the executive is positive (greater than zero). These variables are read using the FORTRAN namelist format through namelist QLST3 via EPAMS file XINFIL. A summary table of the input variables is given with their respective default values in Table A-4. The plot routines assume all plot output is to be written to FORTRAN logical unit 1 on magnetic tape. Also, the plot routines assume the plotter is a drum plotter with at least 24 inch paper and with three different pen turrets to hold optional plot colors. The best color combination is for pen 1 to be black, pen 2 to be red and pen 3 to be blue.

<u>FORTRAN VARIABLE</u>	<u>DEFINITION</u>
ISW	Array of print and/or plot options
ISW(1)	If equal to zero, mesoscale wind field solutions are not printed. If equal to 1, mesoscale wind field solutions are printed in wind speed vector

TABLE A-4  
SUMMARY TABLE OF THE INPUT VARIABLES  
FOR THE GRAPHICS PHASE INPUT  
THROUGH NAMELIST QLST3

FORTTRAN VARIABLE	UNITS	LIMITS	DEFAULT VALUE <sup>③</sup>
ISW(1)	N/A	$\geq -2$ and $\leq 2$	0
ISW(2)	N/A	0 or 1	1
ISW(3)	N/A	0 or 1	0
ISW(5)	N/A	0 or 1	0
ISW(7)	N/A	0 or 1	0
ISW(8)	N/A	0 or 1	0
ISW(9)	N/A	$\geq -2$ and $\leq 2$	0
ISW(10)	N/A	0, 1, 2 or -2	0
ISW(11)	N/A	0 or 1	0
XST	Meters	$\geq 300000$ and $\leq 450000$	XPLACE

(Table A-4 continued on following page.)

① Terrain contour intervals are defaulted to 1219.2, 1524, 1828.8, 2133.6, 2438.4, 2743.2, 3048, 3352.8 meters.

② Mixing layer depth contour intervals are defaulted to 50, 100, 200, 300, 400, 600, 800, 1000, 1200, 1400, 1600, 1800, 2000, 2200, 2400, 2600 meters.

③ If the value of the variable is less than or equal to zero the variable is set equal to its default value.

TABLE A-4 (Continued)

FORTRAN VARIABLE	UNITS	LIMITS	DEFAULT VALUE <sup>③</sup>
YST	Meters	$\geq 3520000$ and $\leq 3670000$	YPLACE
NCØNT	Integer	$\geq 0$ and $\leq 8$	8
CØNT	Meters	$\geq 0$	①
NCØNTS	Integer	$\geq 0$ and $\leq 16$	16
CØNTS	Meters	$\geq 0$	②
SCL	Inches/Meter	$> 0$	$1 \times 10^{-4}$
CNISS	Concentration Units	$\geq 0$	N/A
DSISS	Dosage Units	$\geq 0$	N/A

① Terrain contour intervals are defaulted to 1219.2, 1524, 1828.8, 2133.6, 2438.4, 2743.2, 3048, 3352.8 meters.

② Mixing layer depth contour intervals are defaulted to 50, 100, 200, 300, 400, 600, 800, 1000, 1200, 1400, 1600, 1800, 2000, 2200, 2400, 2600 meters.

③ If the value of the variable is less than or equal to zero the variable is set equal to its default value.

FORTTRAN  
VARIABLE

DEFINITION

ISW(1) (Continued)	components for each elapsed 30 minutes of meso-scale model time plus the final solution. If equal to 2, the wind speed and direction are printed rather than vector components. If negative, only the final wind field solution is printed. (Allow for 31 pages of output for each mesoscale wind field solution printed. The maximum is 155 pages.) (Default = 0.)
ISW(2)	If non-zero, isopleths of concentration and/or dosage are plotted on a terrain contour map. The data is taken from the transport/diffusion solution file. Also, isopleths can be recalculated and plotted by the use of CNISS and/or DSISS below. (Default = 1.)
ISW(3)	If non-zero, the relative variance of the change in momentum and the relative variance of the change in layer depth are plotted as a function of mesoscale model solution time. For an explanation of the purposes of this plot see Sections 4.2 and 4.3 of the main body of this report. (Default = 0.)
ISW(4)	Not used at present.
ISW(5)	If non-zero, the total momentum and total volume from the mesoscale solution are plotted as a function of mesoscale model solution time. For an explanation of the purpose of this plot, see Section 4.3 of the main body of this document. (Default = 0.)
ISW(6)	Not used at present.
ISW(7)	If non-zero, the program uses elevation (MSL) rather than depth in plotting contours of the mixing layer under ISW(10) below. (Default = 0.)
ISW(8)	If non-zero, a contour plot of the terrain elevation (MSL) is generated. (Default = 0.)



FORTTRAN  
VARIABLE

DEFINITION

ISW(9)	If equal to 1, wind speed and direction vectors are plotted on a terrain contour map. If equal to 2, the wind speed and direction vectors are plotted without the terrain contours. If ISW(9) is positive, each intermediate mesoscale solution is plotted at 30 minute intervals including the final solution. A maximum of 5 plots could be generated under this option. However, if ISW(9) is negative, only the final solution is plotted. If this option is selected, specify 3 different pen colors for the three different pen turrets (black, red and blue). (Default = 0.)
ISW(10)	If equal to 1, contours of layer depth or elevation depending on ISW(7) are plotted on plots generated by ISW(9) above. If equal to 2, contours of layer depth or elevation are plotted on contours of terrain elevation for each of the intermediate mesoscale solutions. If equal to -2, only the final solution is plotted. (Default = 0.)
ISW(11)	If non-zero, trajectories generated from optional start locations given by XST and YST below are calculated and plotted on plots generated under ISW(9) above. If ISW(11) is positive, trajectories are plotted only. If negative, trajectories are both printed and plotted. (Default = 0.)
ISW(12) through ISW(19)	Not used at present.
XST	Array of a maximum of 5 UTM easterly (x) coordinates of the start location of optional trajectories in meters.
YST	Array of a maximum of 5 UTM northerly (y) coordinates of the start location of optional trajectories in meters.



<u>FORTRAN VARIABLE</u>	<u>DEFINITION</u>
NCØNT	Number of terrain elevation contours to generate. (Default = 8.)
CØNT	Array of a maximum of 8 contour elevation levels in meters. (Default = 1219.2 to 3352.8 in increments of 304.8 meters or 1000 feet.)
NCØNTS	Number of mixing-layer depth (elevation) contours to generate. (Default = 16.)
CØNTS	Array of a maximum of 16 layer depth (elevation) contour levels in meters. (Default = 50, 100, 200, 300, 400 to 2600 in increments of 200 meters.)
SCL	Plot scale factor for ISW(2), ISW(8), ISW(9), ISW(10) and ISW(11) in inches per meter. (Default = $1.0 \times 10^{-4}$ .)
CNISS	Array of a maximum of 3 concentration isopleth values to use in place of those in the diffusion solution file under ISW(2) above. (No defaults provided.)
DSISS	Array of a maximum of 3 dosage isopleth values to use in place of those in the diffusion solution file under ISW(2) above. (No defaults provided.)

#### A.5 EXAMPLE EPAMS EXECUTION CARD DECK

Figure A-5 gives an example job card deck that executes the EPAMS program. The first three cards shown in Figure A-5 initialize the job and define the EPAMS program file. The next two cards are used to assign a plot output tape to be generated by the Graphics Phase of EPAMS. The sixth card shown assigns all of the catalogued data and solution files required by EPAMS and is an element residing in the EPAMS program file. The seventh card executes the data case

```

@FIN
▽$QLST3▽ISW=0, 2*1, 0, 1, 3*0, -1, 2*1, ▽$END
▽▽4▽▽▽▽▽1
▽$QLST2▽KFLG2=1, Q=100, ▽$END
▽▽1▽▽1▽▽1
▽$QLST1▽KFLG2=1, ▽$END
▽▽2▽▽1▽▽1304▽▽11▽13▽14▽00▽▽380000. ▽▽3560000. 0▽▽1310. 0
@XQT▽B. ABSEPAMS
@ADD▽B. FILEPAMS
@MSG, WVC010U, PAN=####, RUN=EPAMS, NAME=users name
@ASG, TV1., T, C0101U
@USE▽B., NEWHEC*EPAMS.
@ASG, AX▽NEWHEC*EPAMS.
@RUN▽EPAMS, PAN, name, time, pages

```

FIGURE A-5. Example UNIVAC 1108 EPAMS deck set up to calculate concentration and dosage from an instantaneous source on November 13, 1974 at 1400Z. The symbol ▽ means a blank punch.

cards. The first two data cards direct the Analysis Phase to analyse the meteorological data on November 13, 1974 at 1400Z. Also, the source location and elevation is given on data card one to specify the release point and enable the program to select the closest meteorological data. Optional input was selected for the Analysis Phase in order to set KFLG2 to 1 to obtain detailed output from this phase. The next two data cards direct EPAMS to execute, with detailed output, the Application Phase for the concentration and dosage from an instantaneous source. The data cards give a source strength of 100 and allow the program to default all other possible inputs. The last two data cards execute the Graphics Phase and specify plots of concentration and dosage isopleths are to be produced, as well as plots of the final mesoscale wind field solution, relative variance of momentum and depth and total momentum and volume.

The order of the data cards in the example gives an EPAMS solution from start to end. However, the user could execute any one or group of the EPAMS phases depending on the solution desired. An example would be to place a set of Application and Graphics data cards after those shown in Figure 5-1 to produce concentration and dosage for an alternate source location. The user in this case would duplicate the last 4 data cards and would then include the alternate source location in the \$QLST2 card of the second set.

#### A.6 DATA INPUT METHOD

The three phases of EPAMS use the FORTRAN namelist data input method. The namelist input data must be in a specific form in order to be read using a NAMELIST list. The first character in each card to be read must be blank. The first card in the namelist list contains the namelist name preceded by the character \$ (\$QLST1). The last card in each namelist list contains \$END to terminate the list. The form of the remaining data items in the list may be:

- a. *Variable Name = Constant* - The *variable name* may be a subscripted array name or a single variable name. Subscripts must be integer constants. The *constant* may be integer or real.
- b. *Array Name = Set of Constants (Separated by Commas)* - The *array name* is not subscripted. The *set of constants* consists of constants of the type real or integer. The number of constants must be less than or equal to the array size. Successive occurrences of the same constant can be represent in the form  $k * constant$ .

The sequence of the input data parameters within the list is not significant. A more detailed explanation of the FORTRAN NAMELIST can be found in any Fortran Language Manual. The input parameters within the namelist that have default values are initialized to zero or other values in the Analysis Phase (Table A-2) prior to input of the first case. Parameters that are not used or have default constant or calculated values need not appear in the namelist list. When multiple cases are executed, all parameters retain their values from the previous case except in the Analysis Phase and are changed only by input. Also, the computer program assumes that core storage has been zeroed prior to execution.

#### A.7 EPAMS TEMPORARY EXECUTIVE AND DATA FILES

The H. E. Cramer Company has provided a temporary executive routine XECAMS to drive the programs that comprise the Analysis, Application and Graphics Phases of EPAMS. Program XECAMS is the main executive driver of EPAMS. This program assigns logical file numbers to each of the 12 EPAMS data and solution files. The internal file names are held in common block FILES defined on page B-8 of Appendix B and are assumed defined prior to the execution of any EPAMS phase. The internal file name, logical number and contents are



<u>FILE NAME</u>	<u>LOGICAL UNIT NUMBER</u>	<u>CONTENTS</u>
XINFIL	5	Card reader.
XØTFIL	6	Printer.
ØBFILE	0	Upper-air data master file directory. This file contains the station number, station location and hours for which upper air data has been recorded.
UAFIL	1	Upper-air data inventory file containing the observations for the stations and hours identified in ØBFILE.
SFCØBF	20	Surface data master file directory containing the station number, station location and hours for which surface data has been recorded.
SBFILE	21	Surface data inventory file containing the observation for the stations and hours identified in SFCØBF.
GWCPFL	10	GWC (Global Weather Central) data master file directory containing the location and rawinsonde (upper-air) hours for which GWC prediction data has been calculated.
GWCFIL	11	GWC data inventory file containing the prediction data for the 18 hours following each rawinsonde hour and for each location given in GWCPFL.
WSTRRN	12	White Sands Missile Range terrain elevation (MSL meters) data. This file contains the 41 x 41 (1681) point matrix of elevation data where the internal 31 x 31 points are real terrain data and the 5 outermost rows and columns are artificially filled with the minimum WSMR elevation. The data

<u>FILE NAME</u>	<u>LOGICAL UNIT NUMBER</u>	<u>CONTENTS</u>
		are stored starting with the most south-west corner and proceeding eastward, then moving one point north and repeating so the last point is the most north-east elevation. The real terrain data of the internal 31 x 31 points has a south-west UTM coordinate of 300000, 3520000 meters. The last of the real terrain to the east is at x = 450000 and to the north is y = 3670000 covering 150 kilometers in both directions. This file is treated as a read-only file by the EPAMS phases.
MXLYRF	13	This file contains the present and past solutions of the mesoscale wind-field model. The file contains two data blocks, both 5111 words long. Block 1 is the past solution and block 2 is the present or most current solution. Each block consists of the variables given in common block MXBUFR defined in the FORTRAN procedure listing in Appendix B, page B-9.
TRDFFL	14	This file contains the diffusion model solutions from the Application Phase. The file contains one block of 4090 words. The block contains the variables NCALC, IULIAN, IMONTH, IDAY, IHOURL, NINUTE, XSOURC, YSOURC, ZSOURC, KINDS, CONI (3), DCSI (3), DUMMY(664), XX (310), YY(310), SIGMY(310), CHIT (310), DOST(310), YCHIT(310,3) and YDOST(310,3). The variable NCALC is the total number of points in the cloud trajectory, IULIAN is the Julian day of the solution, IMONTH is the month, IDAY is the day, IHOURL is the hour, NINUTE is the minute and XSOURC, YSOURC and ZSOURC is the source location. Also,

<u>FILE NAME</u>	<u>LOGICAL UNIT NUMBER</u>	<u>CONTENTS</u>
		<p>KINDS is the source type number, CØNI concentration isopleth levels, DØSI dosage isopleth levels and DUMMY is extra space for future use. XX and YY define the trajectory location, SIGMY is the standard deviation of the crosswind concentration (dosage) distribution at XX, YY, CHIT and DØST are the concentration and dosage and YCHIT and YDØST are the concentration and dosage isopleth halfwidths, respectively.</p>
SPARE	9	<p>This file is used to store intermediate output from the mesoscale wind-field model for subsequent printing and/or plotting by the Graphics Phase. The file can contain from 2 to 6 blocks of data. The last block is indicated by the first word in the block being negative. This block contains the relative variance of the change in momentum and depth for each model time step, as well as the total volume and momentum for each time step. Each block contains 5111 words where the first blocks are the variables in common MXBUFR defined on page B-9 of Appendix B. The last block is also the same as common MXBUFR except the common block SWELL defined in subroutine MYPRG (page B88, Appendix B) has replaced the arrays M, N and P in MXBUFR and the first word of the block is set to the negative of the total number of mesoscale model time steps. Also, the first blocks are written at approximately 30 minutes model time intervals until model convergence. The final solution is then written before the last data block of this file.</p>

Included in the common block of internal file names are three variables that define the number of data blocks in the master directory files. These variables are MXBLKU, MXBLKG and MXBLKS for files ØBFILE, GWCPFL and SFCØBF, respectively. The Analysis Phase programs use these variables to start reading the master file directories with the most current data, where the most current data is assumed to be at the end of the files. In a real time environment, these variables would probably be set to 1 with the most current observations being the only data in the files. These variables are also initialized in the executive EXAMS on page B-22 of Appendix B.



## APPENDIX B

Appendix B contains the complete FORTRAN listing of the EPAMS computer programs. Page B-2 shows the UNIVAC 1108 element (FILEPAMS) used to assign the necessary data files. Page B-3 and B-4 show the UNIVAC 1108 element (EPAMS-MAP/WSMR) used to collect the EPAMS programs into a segmented absolute program named ABSEPAMS. Pages B-5 through B-21 show the UNIVAC 1108 FORTRAN procedure used to define the common blocks used by the EPAMS programs. Also, the procedure defines all important variables used in the program. The remainder of the Appendix contains a FORTRAN listing of each program used in the EPAMS system. Also, the subroutines UADATA, XTRCUA, SATVP, SFCDTA, TESTFD, GWCDTA, BLKIN, BLKOUT and DRMRD are routines written and supplied by personnel at WSMR. However, some of these routines have been modified and are not interchangeable with previous copies of the routines.

Card images used to assign the EPAMIS data files.

000001	000	W50,AX	0100*SW005.
000002	000	W50,AX	0100*SW000.
000003	000	W50,AX	0100*SW001.
000004	000	W50,AX	0100*SW002.
000005	000	W50,AX	0100*SW003.
000006	000	W50,AX	0100*SW004.
000007	000	W50,AX	0100*SW005.
000008	000	W50,AX	0100*SW006.
000009	000	W50,AX	0100*SW007.
000010	000	W50,AX	0100*SW008.
000011	000	W50,AX	0100*SW009.
000012	000	W50,AX	0100*SW010.
000013	000	W50,AX	0100*SW011.
000014	000	W50,AX	0100*SW012.
000015	000	W50,AX	0100*SW013.
000016	000	W50,AX	0100*SW014.
000017	000	W50,AX	0100*SW015.
000018	000	W50,AX	0100*SW016.
000019	000	W50,AX	0100*SW017.
000020	000	W50,AX	0100*SW018.

Card images used to collect the EPAMS programs into a segmented absolute program named ASBSEPAMS.

```

000001 014  MAP,ISK,B,MAXWDTS
000002 014  DEF AXUAGT
000003 014  REF BLKIN,IDIFTN,CLSSTN,NEKR25,INWDU4,NI025,NEKR35,STN,CUS,ALOG,APRK
000004 014  REF XSTOP$,ALOG10,ATAN2,SQRT
000005 014  IN B,MAXWDTS,UAUTAR,XTRCUA,SAIVP
000006 014  END
000007 014  MAP,ISK,B,MAXWDTS
000008 014  DEF MAGOUT
000009 014  REF BLKIN,CLSSTN,IDIFTN,INWDU3,NI025,NI015,NEKR35,ALOG10,APRK
000010 014  IN B,MAXWDTS,OMOUTR,SAIVP
000011 014  END
000012 014  MAP,ISK,B,MAXWDTS
000013 014  DEF MXSTRT
000014 017  REF BLKIN,BLKOUT,INWDU3,NI025,NEKR25,SQRT,NEKR35,ATAN2
000015 014  IN B,MAXSTRT,REC035
000016 014  END
000017 017  MAP,ISK,B,ASBSEPAMS
000018 017  NOT NR-A*RBLIB,PL0T/CAL035,NR-A*RBLIB,FACTOR/MSMR01
000019 017  NOT NR-A*RBLIB,NUMBER/CAL835,NR-A*RBLIB,SYMBOL/CAL835
000020 017  NOT NR-A*RBLIB,SCALE/CAL035,NR-A*RBLIB,AXIS/CAL835
000021 017  NOT NR-A*RBLIB,LINE/CAL035,NR-A*RBLIB,GRID
000022 017  LIB ASLINES*PLOT.
000023 014  SEG A
000024 014  IN B,XECAMS,BLKIN,BLKOUT,DRMRD
000025 014  IN MESSAGE,TIMES,FILES
000026 014  SEG B*(A)
000027 014  IN B,ANALIZ
000028 014  SEG C*(B)
000029 014  IN B,MALYR,NEWPRM
000030 014  SEG J*(C)
000031 014  IN B,MAXWDTS
000032 014  SEG L*(D)
000033 014  IN B,MAXWDTS
000034 014  SEG E1*(E)
000035 014  IN B,MAXWDTS
000036 014  SEG E2*(E)
000037 014  IN B,LYKAMH,LYNCHK
000038 014  SEG L4*(E)

```

000039	014	IN U.MXSF01,SUPER
000040	014	SEG F2*(E4)
000041	014	IN U.SFC01A,.TESTFD
000042	014	SEG F4*(F2
000043	014	IN U.DAT01T
000044	014	SEG F0*(F2
000045	014	IN U.LONGAT
000046	014	SEG U1*(L
000047	014	IN U.SOLVMA,MAXDPR,WINDFLD,WINDCOM
000048	014	SEG E5*(U1
000049	014	IN U.MX3INTs
000050	014	SEG E6*(E5
000051	014	IN U.MX3CLV
000052	014	SEG E7*(E5
000053	014	IN U.MX3OUT
000054	014	SEG F7*(E0)
000055	014	IN U.MYPRG,SHELL
000056	014	SEG E3*(E5
000057	016	IN U.PLIFRG,.HEC014/WSMR,.HEC015/WSMR,.HEC015/WSMR,.HEC003,ES,M1,DTA1,M1
000058	016	IN U.FRAX,COCDM
000059	014	SEG U*(B3)
000060	016	IN U.HEC007,.HEC013/.SMK
000061	014	SEG U1*(G
000062	014	IN U.HEC005,.HEC009
000063	014	SEG U3*(G
000064	014	IN U.HEC006,.HEC008
000065	014	SEG U4*(G
000066	014	IN U.HEC007
000067	014	SEG U2*(E
000068	015	IN U.APPLY
000069	014	SEG U1*(E2)
000070	016	IN U.IRYLIF,DIF022,SOURCE,COMMAND
000071	014	SEG U2*(C1
000072	014	IN U.IR0PRT
000073	014	SEG U3*(U2
000074	014	IN U.DIFFU2
000075	014	END
000076	017	PACK B.
000077	017	PRK B.
000078	017	PRK T B.



Card images for the UNIVAC 1108 Procedure Definition Processor (PDP) containing program common blocks.

```

1*      COMMENT PROC
2*      C*U*C*U*C*U C XECAMS ANALYSIS, APPLICATION AND GRAPHICS PHASES C*U*C*U*C*U C
3*
4*      C
5*      C THIS PROGRAM ASSUMES THE PROC MESSAGE, TIMES AND FILES GIVEN BELOW
6*      C HAVE BEEN DEFINED IN THE CONTROL PROGRAMS THAT EXECUTE THESE
7*      C ROUTINES. THE DEFINITIONS OF THE VARIABLES IN THESE PROCs ARE
8*      C GIVEN BELOW. THE PROGRAM CONSISTS OF THREE PHASES ANALYSIS,
9*      C APPLICATION AND GRAPHICS.
10*
11*      C (NOTE - IF YOU ARE USING THE DUMMY COPY OF XECAMS THE INPUT DATA )
12*      C ( VARIABLES TYPE1,TYPE2,TYPE3,JULIAN,MONTH,DAY,HOUR,MINUTE, )
13*      C ( XPLACE,YPLACE,ZPLACE ARE INPUT FIRST ON EXECUTION AND )
14*      C ( THEN AFTER THE COMPLETION OF EACH PHASE OF PROCESSING. ALL )
15*      C ( ARE INTEGERS EXCEPT THE LAST THREE. THEY ARE READ USING )
16*      C ( AN (813,3F10.2) FORMAT. THE VARIABLES ARE DEFINED IN PROC )
17*      C ( MESSAGE AND TIMES BELOW. THIS PROG IS INITIALLY PROVIDED )
18*      C ( WITH THE DUMMY ROUTINES XECAMS, ANALIZ, APPLY ALL OTHER )
19*      C ( ROUTINES ARE OPERATIONAL PROGRAMS. )
20*
21*      C THE ANALYSIS PHASE IS EXECUTED BY A CALL TO SUBROUTINE MIXLYR.
22*      C THIS PHASE ANALYZES THE METEOROLOGICAL DATA BASE AND CALCULATES
23*      C PARAMETERS NECESSARY FOR THE EXECUTION OF THE MESO-SCALE MODEL
24*      C AND OTHER PARAMETERS FOR USE IN THE APPLICATION PHASE. THIS PHASE
25*      C HAS OPTIONAL INPUT DATA IN NAMELIST FORMAT VIA NAMELIST GLST1.
26*      C THIS IS DETERMINED BY THE VARIABLE TYPE3 DEFINED IN PROC MESSAGE
27*      C BELOW. THIS PHASE STORES ALL RESULTS IN THE DATA BASE AND AT
28*      C COMPLETION RETURNS CONTROL TO THE CALLING PROGRAM. IF THE PROG
29*      C CANNOT COMPLETE THE MIXING LAYER SOLUTION OR THE MESOSCALE
30*      C SOLUTION TYPE3 IS RETURNED AS A NEGATIVE NUMBER.
31*      C ONLY THE MIXING LAYER CALCULATIONS PART OF THE ANALYSIS SECTION
32*      C IS EXECUTED IF TYPE3 IS SET EQUAL TO 9. SEE PROC MESSAGE BELOW.
33*
34*      C THE APPLICATION PHASE IS EXECUTED BY A CALL TO SUBROUTINE TRYU1F.
35*      C THIS PHASE OBTAINS THE RESULTS OF THE ANALYSIS PHASE FROM THE DATA
36*      C BASE AND EXECUTES THE TRANSPORT (TRAJECTORY) AND DIFFUSION MODELS.
37*      C THIS PHASE HAS OPTIONAL INPUT DATA IN NAMELIST FORMAT VIA
38*      C NAMELIST GLST2. THIS IS DETERMINED BY THE VARIABLE TYPE3 DEFINED
39*      C IN PROC MESSAGE BELOW. THIS PHASE PRINTS THE DIFFUSION MODEL

```

```

39* C
40* C
41* C
42* C
43* C
44* C
45* C
46* C
47* C
48* C
49* C
50* C
51* C
52* C
53* C
54* C
55* C
56* C
57* C
58* C
59* C
60* C
61* C
62* C
63* C
64* C
65* C
66* C
67* C
68* C
69* C
70* C
71* C
72* C
73* C
74* C
75* C
76* C

CALCULATIONS AND STORES ALL RESULTS IN THE DATA BASE AND RETURNS
CONTROL TO THE CALLING PROGRAM. IF THE APPLICATION PHASE DOES NOT
HAVE ENOUGH INFORMATION OR IF THERE IS A MODEL FAILURE TYPE3 IS
RETURNED AS A NEGATIVE NUMBER. ALSO, TYPE3 CAN BE USED TO
DEFAULT A SOURCE TYPE.

THE GRAPHICS PHASE IS EXECUTED BY A CALL TO SUBROUTINE PLIPRG.
THIS PHASE OBTAINS THE RESULTS OF THE ANALYSIS OR THE APPLICATION
PHASE OR BOTH AND PRINTS AND/OR PLOTS THE RESULTS. THIS PHASE
HAS OPTIONAL INPUT DATA IN NAMELIST FORMAT VIA NAMELIST GLST3.
THIS IS DETERMINED BY THE VARIABLE TYPE3 DEFINED IN PROC MESSAGE
BELOW. AT THE COMPLETION OF THIS PHASE CONTROL IS RETURNED TO THE
CALLING PROGRAM. IF THE APPLICATION PHASE CANNOT COMPLETE AN
ASSIGNED TASK TYPE3 IS RETURNED AS A NEGATIVE NUMBER.

FILE INFORMATION - FILES USED IN DIFFERENT PHASES
NOTE - FILE LOGICAL NUMBER ASSIGNMENTS ARE MADE IN XECAMS
APPLICATION PROG USES FILES MXLYRF,WSTRN, TRDFFL, XINFIL, XOIFIL
-FILE MXLYRF CONTAINS 2 BLOCKS 511 WORDS PER BLOCK, MESOSCALE
SOLUTION FILE CONTAINING PAST (BLOCK 1) AND PRESENT (BLOCK 2)
SOLUTIONS. EACH BLOCK IS CONSTRUCTED AS IN COMMON MXBUFR
-FILE WSTRN CONTAINS THE TERRAIN DATA (41X41 GRID) (1 BLOCK)
-FILE TRDFFL CONTAINS THE DIFFUSION MODEL SOLUTION (1 BLOCK OF
4090 WORDS, THIS BLOCK CONTAINS NCALC,IULIAN,IMONTH,IDAY,THOUR,
MINUTE,XSOURC,YSOURC,ZSOURC,KINDS,
CON(I(3),DOSI(3),DUMMY(664),XX(310),YY(310),SIGMY(310),CHIT(310),
DUST(310),YCHIT(310,3),YDUST(310,3) NCALC IS THE NO. OF TRAJECT
POINTS - IULIAN TO MINUTE COME FROM PROC TINES -
XSOURC,YSOURC,ZSOURC IS THE SOURCE LOCATION - KINDS IS THE
SOURCE TYPE (KINDSO BELOW) - CONI,DOSI INPUT ISOPLETH VALUES
(CONISS,DOSISS) - XX,YY TRAJECTORY COORDINATES - SIGMY, CHIT,
DUST ARE SIGMA-Y, CON AND DOS AT XX,YY - YCHIT AND DOST ARE THE
LATERAL DISTANCE FROM CENTERLINE TO ISOPLETH VALUE FOR THE 3 INPUT
ISOPLETH LEVELS.

ANALYSIS - PROG USES FILES MXLYRF, WSTRN, OBFILE, UAFIL
GWCFL,GWCPFL,SUFILE,SFCOBF, SPARE, XINFIL, XOIFIL
-FILE SPARE CONTAINS UP TO 5 BLOCKS OF INTERMEDIATE MESOSCALE
SOLUTIONS FROM COMMON MXBUFR. THE LAST BLOCK CONTAINS 1000 WORDS

```

```

77* C CONTAINING INFO TO PLOT MOMENTUM, VOLUME, REL CHANGE MOM AND REL
78* C CHANGE VOLUME (SPARE IS WRITTEN IN SUB MYPRG)
79* C
80* C GRAPHICS - PROG USES FILES MXLYKF, WSTRRN, TRUFFL, SPARE, XINFIL,
81* C XOTFIL
82* C
83* C
84* C
85* C
86* C
87* C
88* C
89* C
90* C
91* C
92* C
93* C
94* C
95* C
96* C
97* C
98* C
99* C
100* C
101* C
102* C
103* C
104* C
105* C
106* C
107* C
108* C
109* C
110* C
111* C
112* C
113* C
114* C

```

END  
 MESSAGE PROC  
 COMMON /MESSAGE/ TYPE1,TYPE2,TYPE3,XPLACE,YPLACE,ZPLACE  
 INTEGER TYPE1,TYPE2,TYPE3  
 \*\* THESE VARIABLES ARE PASSED TO THE PROCESSING PHASES. VIA THIS  
 COMMON BLOCK. THE PHASES ASSUME -  
 TYPE1 - NOT REFERENCED  
 TYPE2 - NOT REFERENCED  
 TYPE3 - INPUT DATA CONTROL VARIABLE REFERENCED IN ALL THREE PHASES  
 ANALYSIS PHASE - IF TYPE3 IS ZERO NO INPUT DATA IS ASSUMED.  
 IF TYPE3 IS NON-ZERO INPUT DATA IS READ FROM  
 UNIT XINFIL VIA NAMELIST GLST1. THE VARIABLES  
 THAT CAN BE INPUT ARE DEFINED IN PROC NEWPRM  
 BELOW. TYPE3 IS RETURNED AS A LOG NO. IF  
 THERE IS A FAILURE IN THE ANALYSIS PHASE.  
 IF THE ABSOLUTE VALUE OF TYPE3 = 9 THE MESO-  
 SCALE SOLUTION IS NOT PRODUCED, ONLY THE  
 MIXING LAYER SOLUTION IS PRODUCED. THIS  
 OPTION IS USED ONLY TO DISPLAY THE NET DATA  
 USED AND MIXING LAYER CALCULATIONS. IF TYPE3  
 IS NEG. NO INPUT DATA IS ASSUMED. IF POS.  
 INPUT DATA IS READ AS ABOVE. HOWEVER, KFLG2  
 IN NAMELIST GLST1 (PROC NEWPRM) IS NOW SET  
 NON-ZERO AUTOMATICALLY.  
 APPLICATION PHASE - IF TYPE3 IS ZERO OR NEGATIVE NO INPUT DATA  
 IS ASSUMED AND ALL INPUT PARAMETERS ARE  
 DEFAULTED. HOWEVER, IF TYPE3 = -1 THE PROG  
 DEFAULTS TO CONTINUOUS SOURCE 1 (ASARCO  
 COPPER), OR IF TYPE3 = -2 THE PROGRAM  
 DEFAULTS TO CONTINUOUS SOURCE 2 (ASARCO  
 LEAD).  
 IF TYPE3 IS > ZERO INPUT DATA IS READ



```

113* FROM UNIT XINFIL VIA NAMELIST QLST2. THE
116* VARIABLES THAT CAN BE INPUT ARE DEFINED
117* IN PROC SOURCE BELOW. TYPE3 IS RETURNED AS
118* A NEG IF THERE IS A FAILURE IN THE
119* APPLICATION PHASE.
120*
121* GRAPHICS PHASE - IF TYPE3 IS A ZERO NO INPUT DATA IS ASSUMED.
122* IF TYPE3 IS NON-ZERO INPUT DATA IS READ
123* FROM UNIT XINFIL VIA NAMELIST QLST3. THE
124* VARIABLES THAT CAN BE INPUT ARE DEFINED
125* IN PROC N1 BELOW. TYPE3 IS RETURNED AS A NEG
126* IF THERE IS A FAILURE IN THE GRAPHICS PHASE.
127*
128* XPLACE - X (EASTERLY) UTM COORDINATE OF THE SOURCE (EMISSION)
129* LOCATION IN METERS (IF = 0.0 THE PROG USES 360000.0
130* FROM PROC DEFINP BELOW.) (REFERENCED ONLY IN THE ANALYSIS
131* PHASE)
132*
133* YPLACE - Y (NORTHERLY) UTM COORDINATE OF THE SOURCE (EMISSION)
134* LOCATION IN METERS (IF = 0.0 THE PROG USES 3585000.0
135* FROM PROC DEFINP BELOW.) (REFERENCED ONLY IN THE ANALYSIS
136* PHASE)
137*
138* ZPLACE - Z ELEVATION OF SOURCE (EMISSION) BASE LOCATION IN METERS
139* (IF = 0.0 THE PROGRAM USES 1310.0 FROM PROC DEFINP BELOW)
140* (REFERENCED ONLY IN THE ANALYSIS PHASE)
141*
142* END
143*
144* FILES
145*
146* COMMON /FILES/ XINFIL,XOTFIL,SPARE,WSTRN,ODFILE,MXLYRF,TRDFFL
147* 1,UAFIL,GWCFIL,GWCPFL,SBFILE,SFCOBF,MXBLKU,MXBLKG,MXBLKS
148* INTEGER XINFIL,XOTFIL,SPARE,WSTRN,ODFILE,MXLYRF,TRDFFL
149* INTEGER UAFIL,GWCFIL,GWCPFL,SBFILE,SFCOBF
150* THESE VARIABLES ARE PASSED TO THE 3 PHASES VIA THIS COMMON BLOCK
151* XINFIL - INPUT DATA (CARD) FILE
152* XOTFIL - OUTPUT (PRINT) FILE
153* SPARE - FILE USED TO STORE TEMPORARY OUTPUT FROM ANALYSIS PHASE FOR
154* PRINTING AND/OR PLOTTING BY GRAPHIC PHASE
155*
156* WSTRN - TERRAIN DATA FILE
157* ODFILE - UPPER AIR DATA MASTER DIRECTORY FILE
158* MXLYRF - MESO-SCALE SOLUTION FILE
159* TRDFFL - DIFFUSION MODEL SOLUTION FILE
160* UAFIL - UPPER AIR DATA INVENTORY FILE

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153* C GWCFILE - GWC DATA INVENTORY FILE
154* C GWCPLF - GWC DATA MASTER DIRECTORY FILE
155* C SFILE - SURFACE DATA INVENTORY FILE
156* C SFCDF - SURFACE DATA MASTER DIRECTORY FILE
157* C MXBLKU - MAXIMUM NO. OF DATA BLOCKS IN FILE OBFILE
158* C MXBLKG - MAXIMUM NO. OF DATA LOCKS IN FILE GWCPLF
159* C MXBLKS - MAXIMUM NO. OF DATA BLOCKS IN FILE SFCDF
160* C
161* C
162* C
163* C
164* C
165* C
166* C
167* C
168* C
169* C
170* C
171* C
172* C
173* C
174* C
175* C
176* C
177* C
178* C
179* C
180* C
181* C
182* C
183* C
184* C
185* C
186* C
187* C
188* C
189* C
190* C

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END  
 SUBROUTINE PROC  
 COMMON /MXBUFR/ NETRAD,IULIAN,IMONTH,IDAY,IHOUR,NINUTE,XSOURC,  
 1YSOURC,ZSOURC,SURFTA,POTMPR(25),ZELEVR(25),UO,VO,PO,ABLKO,DILNDO,  
 200,ISMTHO,NCNIO,M(41,41),N(41,41),P(41,41)  
 REAL M,N  
 MXBUFR CONTAINS THE WINDFIELD SOLUTION MATRICES M,N,P AND THE  
 INITIALIZATION AND CONTROL PARAMETERS USED IN THE SOLUTION  
 NETRAD - NET RADIATION INDEX  
 XSOURC - UTM EASTERLY COORDINATE (METERS) OF SOURCE  
 YSOURC - UTM NORTHERLY COORDINATE (METERS) OF SOURCE  
 ZSOURC - ELEVATION OF SOURCE (METERS)  
 SURFTA - CONTAINS THE SURFACE TEMP  
 POTMPR - CONTAINS THE POTENTIAL TEMP AT THE FIRST 25 LEVELS  
 ZELEVR - CONTAINS THE ELEVATION OF THE FIRST 25 LEVELS  
 UO - U COMPONENT OF WIND SPEED (MPS)  
 VO - V COMPONENT OF WIND SPEED (MPS)  
 PO - LAYER ELEVATION (METERS)  
 ABLKO - MINIMUM LAYER DEPTH (METERS) CONSTRAINT  
 DILNDO - STABILITY PARAMETER FOR CALCULATING TIME STEP BETWEEN  
 MODEL ITERATIONS  
 GO - REDUCED GRAVITY FACTOR  
 ISMTHO - NO. OF TIME STEPS (ITERATIONS) BETWEEN FILTER APPLICATION  
 ICNIO - NO. OF TIME STEPS (ITERATIONS) BETWEEN RECALCULATION  
 OF THE TIME STEP INCREMENT  
 END  
 SUBROUTINE PROC  
 THIS COMMON BLOCK IS THE SAME AS MXBUFR ABOVE IT IS RENAMED FOR  
 USE IN SUBROUTINE PLTHRG FOR EASE OF SEGMENTED COLLECTION  
 COMMON /BUFRMX/ NETRAD,IULIAN,IMONTH,IDAY,IHOUR,NINUTE,XSOURC,  
 1YSOURC,ZSOURC,SURFTA,POTMPR(25),ZELEVR(25),UO,VO,PO,ABLKO,DILNDO,  
 200,ISMTHO,NCNIO,M(41,41),N(41,41),P(41,41)

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191*      250,ISMTHO,ICNTIO,M(41,41),N(41,41),P(41,41)
192*      REAL M,N
193*
194*      END
195*      WINDFLD  PROC
196*      COMMON /WINDFLD/ IUM,JUM,G2,DTL,NH,ISM,TIN,ICNT,UVMIN,UVEGU,UVMAX,
197*      DUPMAX,GP(39),B3P(39),C3P(39),DELXI(6),DELYJ(6),DXPI(6),DYPJ(6),
198*      2TIMMAX,IFLG,SIPN,H(41,41)
199*
200*      C
201*      C
202*      C ** NOTE - ALL VARIABLES WITH ** DEPEND ON THE TERRAIN GRID MATRIX
203*      C ** OR TERRAIN GRID AXES. IF EITHER ARE MODIFIED REVIEW ALL
204*      C ** ** CARUS FOR NECESSARY MODIFICATIONS. ALSO, REVIEW COMMENTS
205*      C ** IN SUBROUTINE TRNPRT.
206*      C
207*      C
208*      C IUM,JUM,G2,DTL,NH,ISM,TIN,ICNT - INTERNAL CONSTANTS AND COUNTERS
209*      C UVMIN - MIN. VALUE > 0 FOR U OR V TO PREVENT UNDERFLOWS
210*      C UVMAX - MAX. VALUE FOR U OR V TO PREVENT MODEL INSTABILITY
211*      C UVEGU - USED IN CALCULATING M AND N AND P TO PREVENT UNDERFLOWS
212*      C DUPMAX - MAX. DEPTH OF LAYER TO PREVENT MODEL INSTABILITY
213*      C GP,B3P,C3P - ARRAYS USED TO STORE FORWARD DIFFERENCES IN MODEL
214*      C CALCULATION TO AVOID CALCULATING BACKWARD DIFFERENCES
215*      C DELXI - ARRAY CONTAINING THE INVERSE OF THE POS. DISTANCE BETWEEN
216*      C POINTS 1-3,2-4,3-5,4-6,5-7,6-8 OF THE EXPANDED GRID OF THE
217*      C X AXIS. THE ARRAY DELXI IS SET THROUGH DATA IN PROC WINDTA
218*      C , (1/(6*XINC)), (1/(3*XINC)), (1/(2*XINC))
219*      C DELYJ - ARRAY CONTAINING THE INVERSE OF THE POS. DISTANCE BETWEEN
220*      C POINTS 1-3,2-4,3-5,4-6,5-7,6-8 OF THE EXPANDED GRID OF THE
221*      C Y AXIS. THE ARRAY DELYJ IS SET THROUGH DATA IN PROC WINDTA
222*      C BELOW IN THE SAME MANNER AS DELXI EXCEPT YINC IS USED.
223*      C DXPI - ARRAY CONTAINING THE INVERSE OF THE POS. DISTANCE BETWEEN
224*      C EACH POINT 1-2,2-3,3-4,4-5,5-6,6-7 OF THE EXPANDED GRID OF
225*      C THE X AXIS. THE ARRAY DXPI IS SET THROUGH DATA IN PROC
226*      C WINDTA BELOW AND EQUALS (1/(32*XINC)), (1/(16*XINC)),
227*      C (1/(8*XINC)), (1/(4*XINC)), (1/(2*XINC)), (1/XINC)
228*      C DYPJ - SAME AS DXPI EXCEPT FOR Y AXIS AND USES YINC.
229*      C

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229* C TIMMAX - MAX MODEL TIME FOR ANY RUN.
230* C IFLG,STPN - CONTROL PARAMETERS
231* C H - ELEVATION OF TERRAIN - THIS ARRAY IS INPUT AS 1 BLOCK FROM
232* C FILE WSTRN AND CONSISTS OF THE REGULAR EVENLY SPACED GRID
233* C PLUS THE EXPANDED GRID REGION. THE EXPANDED GRID REGION
234* C (1ST AND LAST 5 ROWS AND COLUMNS) IS SET EQUAL TO THE MINIMUM
235* C TERRAIN ELEVATION (HMIN IN PROC WNDCOM) UNLESS SEVERE TERRAIN
236* C GRADIENTS ARE CAUSING STABILITY PROBLEMS. IN PLACES OF SEVERE
237* C TERRAIN GRADIENTS THE FIFTH ROW (COLUMN) IN SHOULD BE SET TO
238* C ITS REAL TERRAIN VALUE IN THESE ISOLATED AREAS.
239* C PROG CURRENTLY READS 1681 (41,41) POINTS INTO H
240* C
241* C
242* C COMMON /WINDCOM/ IUP,JUP,XSTRT,YSTRT,XINC,YINC,XMIN,HMIN
243* C ** IUP - THE NUMBER OF TOTAL PNTS. IN THE X AXIS OR THE NO. OF PNTS.
244* C OF REAL TERRAIN PLUS 10 FOR THE EXPANDED REGION AT BOTH ENDS
245* C OF THE AXIS. (CURRENTLY SET TO 41)
246* C ** JUP - THE NUMBER OF TOTAL PNTS. IN THE Y AXIS OR THE NO. OF PNTS.
247* C OF REAL TERRAIN PLUS 10 FOR THE EXPANDED REGION AT BOTH ENDS
248* C OF THE AXIS. (CURRENTLY SET TO 41)
249* C ** XSTRT - STARTING COORDINATE OF THE X AXIS OF THE REAL TERRAIN GRID
250* C (NOT INCLUDING EXPANDED REGION) (METERS)
251* C ** YSTRT - STARTING COORDINATE OF THE Y AXIS OF THE REAL TERRAIN GRID
252* C (NOT INCLUDING EXPANDED REGION) (METERS)
253* C ** XINC,YINC - INCREMENT IN METERS BETWEEN GRID POINTS IN THE REAL
254* C TERRAIN GRID AREA FOR THE X,Y AXES (METERS)
255* C ** XMIN - MINIMUM VALUE OF XINC AND YINC (METERS)
256* C ** HMIN - MINIMUM TERRAIN ELEVATION HEIGHT (METERS)
257* C
258* C
259* C COMWIND PROC
260* C THIS COMMON BLOCK IS THE SAME AS WNDCOM ABOVE IT IS RENAMED FOR
261* C USE IN SUBROUTINE TRYU1F FOR EASE OF SEGMENTED COLLECTION
262* C COMMON /COMWIND/ IUP,JUP,XSTRT,YSTRT,XINC,YINC,XMIN,HMIN
263* C
264* C
265* C CONWIND PROC
266* C THIS COMMON BLOCK IS THE SAME AS WNDCOM ABOVE IT IS RENAMED FOR
267* C USE IN SUBROUTINE PLTPRG FOR EASE OF SEGMENTED COLLECTION
268* C COMMON /CONWIND/ IUP,JUP,XSTRT,YSTRT,XINC,YINC,XMIN,HMIN

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267*      END
268*      MODULE PROC
269*      C ** VALUES OF GRID PARAMETERS THAT ARE CONSTANT OVER THE GRID REGION
270*      DATA DELX1/4,1666666E-6,8.3333333E-6,1.6666666E-5,3.3333333E-5,
271*      16.6666666E-5,1.0E-4/
272*      DATA DELY1/4,1666666E-6,8.3333333E-6,1.6666666E-5,3.3333333E-5,
273*      16.6666666E-5,1.0E-4/
274*      DATA DXPI/6,25E-6,1.25E-5,2.5E-5,5.0E-5,1.0E-4,2.0E-4/
275*      DATA DYPJ/6,25E-6,1.25E-5,2.5E-5,5.0E-5,1.0E-4,2.0E-4/
276*      DATA TIMMAX/7200./,IFLG/0/
277*
278*      END
279*      MODULE PROC
280*      C ** VALUES OF PROGRAM CONSTANTS THAT ARE FIXED BY THE TERRAIN GRID
281*      C      USED
282*      DATA ICP,ICP,XSTRT,YSTRT,XINC,YINC,XMIN,HMIN/41,41,300000.,
283*      13520000.,3*5000.,1140./
284*
285*      END
286*      TIMES
287*      C ** THESE VARIABLES ARE PASTED TO THE ANALYSIS PHASE VIA THIS COMMON
288*      C      BLOCK. THESE VARIABLES GIVE THE TIME AND DATE FOR THE DESIRED
289*      C      SOLUTION. THE TIME AND DATE CAN BE PAST, PRESENT OR FUTURE
290*      C      JULIAN - JULIAN DAY OF LAST DAY OF PREVIOUS MONTH
291*      C      MONTH - MONTH (1-12)
292*      C      DAY - DAY (1-31)
293*      C      HOUR - HOUR IN GREENWICH TIME (00-23)
294*      C      MINUTE - MINUTE (00-60)
295*      C      COMMON /TIMES/ JULIAN,MONTH,DAY,HOUR,MINUTE
296*      C      INTEGER DAY,HOUR
297*
298*      END
299*      N1
300*      C ** THIS PROC DEFINES DATA INPUT TO THE GRAPHICS PHASE. DATA IS READ
301*      C      FROM UNIT XINFIL VIA NAMELIST GLST3 ONLY IF TYPE3 IN PROC MESSAGE
302*      C      IS NON-ZERO. IF NO INPUT IS DESIRED THE PROGRAM DEFAULTS THE
303*      C      VARIABLES AS GIVEN BELOW.
304*      C      ISW - ARRAY OF PRINT/PLOT OUTPUT OPTIONS
305*      C      ISW(1) - IF = 0 MESO-SCALE WIND FIELD SOLUTIONS ARE NOT PRINTED,
306*      C      IF = 1 PRINT IN VECTOR COMPONENTS. IF = 2 PRINT IN SPEED
307*      C      AND DIRECTION. IF POSITIVE ALL INTERMEDIATE SOLUTIONS

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305* ARE PRINTED (30,60,90,120, FINAL MINUTES). IF NEGATIVE
306* ONLY THE FINAL SOLUTION IS PRINTED. ( DEFAULT = 0)
307* IF # 0 PLOT THE DIFFUSION ISOPLETHS OR RECALCULATE
308* ISOPLETHS AND PLOT ON TERRAIN MAP (DEFAULT = 1)
309* IF # 0 PLOT THE RELATIVE VARIANCE OF THE CHANGE IN
310* MOMENTUM AND VOLUME FROM THE MESO-SCALE SOLUTION TO
311* ANALYZE BEHAVIOR OF SOLUTION. (DEFAULT = 0)
312* ISW(4) - N/A
313* ISW(5) - IF # 0 PLOT TOTAL MOMENTUM AND VOLUME VERSUS TIME FROM
314* THE MESO-SCALE SOLUTION TO ANALYZE THE BEHAVIOR OF THE
315* SOLUTION (DEFAULT = 0)
316* ISW(6) - N/A
317* ISW(7) - IF # 0 THE PROGRAM USES ELEVATION RATHER THAN DEPTH IN
318* ISW(10) BELOW. IF # 0 YOU MUST INPUT NCONTS AND CONTS
319* BELOW (DEFAULT = 0)
320* ISW(8) - IF # 0 PLOT TERRAIN ELEVATION MAP FROM FILE "STRRN
321* (USES ONLY INTERNAL 31X31 GRID) (DEFAULT = 0)
322* ISW(9) - IF # 1 PLOT VECTOR MESO-SCALE SOLUTIONS ON TERRAIN MAP,
323* IF # 2 PLOT VECTOR MESO-SCALE SOLUTIONS ALONE,
324* IF POSITIVE ALL INTERMEDIATE SOLUTIONS ARE PLOTTED (30,60,
325* 90,120, FINAL MINUTES) IF NEGATIVE ONLY THE FINAL
326* SOLUTION IS PLOTTED. (DEFAULT = 0)
327* ISW(10) - IF # 1 PLOT THE LAYER DEPTH ON PLOTS GENERATED BY ISW(9)
328* IF # 2 PLOT THE LAYER DEPTH ON TERRAIN ONLY. IF EQUAL TO
329* 2 AND POSITIVE ALL INTERMEDIATE SOLUTIONS ARE PLOTTED,
330* IF # 2 AND NEGATIVE ONLY THE FINAL SOLUTION IS PLOTTED.
331* (DEFAULT = 0)
332* ISW(11) - IF # 0 CALCULATE TRAJECTORIES FROM START POINTS XST,YST
333* AND PLOT ON PLOTS GENERATED BY ISW(9) ABOVE. IF POSITIVE
334* PLOT TRAJECTORIES ONLY. IF NEGATIVE PRINT AND PLOT
335* TRAJECTORIES (DEFAULT = 0)
336* ISW(12)-ISW(19) - N/A
337* ISW(20) - DO NOT USE, INTERNAL PROG SWITCH
338* XST,YST - ARRAYS OF START POINTS OF TRAJECTORIES GENERATED UNDER
339* ISW(11) ABOVE. (MAX OF 5 VALUES EACH). IF XST AND YST
340* ARE BOTH ZERO THE PROG DEFAULTS TO THE SOURCE LOCATION
341* USED IN THE ANALYSIS PHASE.
342* NCONT - NO. OR TERRAIN CONTOUR LEVELS (DEFAULT = 3)

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361*	C	AFTER CLOUD STABILIZATION (METERS)
362*	C	INSTANTANEOUS SOURCE ONLY (DEFAULT = 0.0)
363*	C	STANDARD DEVIATION OF THE CROSSWIND SOURCE DISTRIBUTION
364*	C	AFTER CLOUD STABILIZATION (METERS)
365*	C	INSTANTANEOUS SOURCE ONLY (DEFAULT = 0.0)
366*	C	STANDARD DEVIATION OF THE VERTICAL SOURCE DISTRIBUTION
367*	C	AFTER CLOUD STABILIZATION (METERS)
368*	C	INSTANTANEOUS SOURCE ONLY (DEFAULT = 0.0)
369*	C	H - HEIGHT ABOVE GROUND (ZSOUR) OF CLOUD AFTER STABILIZATION
390*	C	FOR INSTANTANEOUS SOURCES, OR HEIGHT ABOVE GROUND OF
391*	C	EMISSION FOR CONTINUOUS SOURCES (METERS)
392*	C	(DEFAULT = 0 FOR INST. SOURCE, = 252.4 M IF CONT. SOURCE 1,
393*	C	= 180.5 M IF CONT. SOURCE 2)
394*	C	Z - HEIGHT ABOVE GROUND FOR CONCENTRATION AND DOSAGE CALCULATIONS
395*	C	(METERS) (DEFAULT = 0)
396*	C	TAU - SOURCE EMISSION TIME FOR INSTANTANEOUS SOURCES (SECONDS)
397*	C	(DEFAULT = 2.5 SEC)
398*	C	ALPHA - CROSSWIND DIFFUSION COEFFICIENT (DEFAULT = 1)
399*	C	BETA - VERTICAL DIFFUSION COEFFICIENT (DEFAULT = 1)
400*	C	KINDSO - IF = 0 INSTANTANEOUS SOURCE, IF ≠ 0 CONTINUOUS SOURCE.
401*	C	IF = 1 CONTINUOUS SOURCE 1 (ASARCO COPPER)
402*	C	IF = 2 CONTINUOUS SOURCE 2 (ASARCO LEAD)
403*	C	(IF TYPE3 ≥ 0 DEFAULT = 0) (IF TYPE3 = -1 OR -2 DEFAULT
404*	C	= 1 OR 2)
405*	C	DECAY - COEFFICIENT OF TIME DEPENDENT DECAY (DEFAULT = 0)
406*	C	BLAMDA - COEFFICIENT OF PRECIPITATION SCAVENGING (DEFAULT = 0)
407*	C	GAMMA - REFLECTION COEFFICIENT - FRACTION OF MATERIAL REFLECTED
408*	C	AT THE SURFACE (DEFAULT = 1.0)
409*	C	STTEMP - STACK EFFLUENT EXIT TEMPERATURE (DEG K) CONTINUOUS SOURCE
410*	C	ONLY
411*	C	(DEFAULT = 366.3 DEG K CONT. SOURCE 1, OR = 352.4 DEG K
412*	C	CONT. SOURCE 2)
413*	C	RADIUS - INTERNAL STACK RADIUS (METERS) CONTINUOUS SOURCES ONLY
414*	C	(DEFAULT = 4.877 M CONT. SOURCE 1, OR = 3.658 M CONT.
415*	C	SOURCE 2)
416*	C	EXTVEL - STACK EFFLUENT EXIT VELOCITY (METERS/SECOND) CONTINUOUS
417*	C	SOURCES ONLY
418*	C	(DEFAULT = 2.1476 M/SEC CONT. SOURCE 1, OR 2.7512 M/SEC

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419*      C      CONT. SOURCE 2)
420*      C      VS - PARTICLE SETTLING VELOCITY FOR GRAVITATIONAL DEPOSITION
421*      C      OR DEPLETION OF CONCENTRATION AND DOSAGE DUE TO GRAVITATIONAL
422*      C      DEPOSITION (METERS/SEC)
423*      C      (DEFAULT = 0)
424*      C      CONISS - ARRAY OF 3 VALUES CONTAINING THE CONCENTRATION ISOPLETH
425*      C      LEVELS IN UNITS OF UNITS PER CUBIC METER (DEFAULT =
426*      C      1.0E-4, 1.0E-6, 1.0E-12)
427*      C      DOSISS - ARRAY OF 3 VALUES CONTAINING THE DOSAGE ISOPLETH
428*      C      LEVELS IN UNITS OF UNITS SECONDS PER CUBIC METER (DEFAULT
429*      C      = 1.0E-4, 1.0E-6, 1.0E-12)
430*      C      TEMPSF - SURFACE TEMP (DEG K) IF NOT PROVIDED BY ANALYSIS PHASE
431*      C      (CONTINUOUS SOURCES ONLY)
432*      C      RTLAPS - LAPSE RATE OF POTENTIAL TEMPERATURE (DEG K/METER) IF NOT
433*      C      PROVIDED BY THE ANALYSIS PHASE (CONTINUOUS SOURCES ONLY)
434*      C      KFLG1 - IF = 0 THE PROGRAM WILL USE THE PRESENT SOLUTION OF THE
435*      C      MESO-SCALE MODEL IN THE APPLICATION PHASE. IF # 0 THE
436*      C      PROGRAM WILL USE THE PAST MESO-SCALE SOLUTION.
437*      C      KFLG2 - IF = 0 ONLY CONCENTRATION, DOSAGE AND ISOPLETHS ARE
438*      C      PRINTED. IF # 0 THE TRAJECTORY AND RELATED PARAMETERS ARE
439*      C      ALSO PRINTED.
440*      C
441*      C      COMMON /SOURCE/ XSOUR,YSOUR,ZSOUR,Q,SIGXO,SIGYO,SIGZO,H,Z,TAU
442*      C      1,ALPHA,BETA,KINDSO,DECAY,BLAMDA,GAMMA,STTEMP,RADIUS,EXTVEL,VS,
443*      C      2CONISS(3),DOSISS(3),TEMPSF,RTLAPS,KFLG1,KFLG2
444*      C
445*      C      END
446*      C      DIFUZZ  PROC
447*      C      PARAMETERS PAST TO DIFFUSION MODEL ROUTINE
448*      C      NETRAD IS THE CALCULATED NET RADIATION INDEX FROM ANALYSIS ROUTINE
449*      C      XSOURC IS THE RELEASE (SOURCE) LOCATION USED BY ANALYSIS ROUTINES
450*      C      YSOURC IS THE RELEASE (SOURCE) LOCATION USED BY ANALYSIS ROUTINE
451*      C      ZSOURC IS THE ELEVATION OF THE RELEASE (SOURCE) USED BY ANALYSIS
452*      C      ROUTINES (ELEVATION OF GROUND)
453*      C      XX - ARRAY OF UTM X COORDINATES IN METERS DEFINING THE TRAJECTORY
454*      C      OF THE CLOUD CENTROID
455*      C      YY - ARRAY OF UTM Y COORDINATES IN METERS DEFINING THE TRAJECTORY
456*      C      OF THE CLOUD CENTROID
457*      C      UBAR - ARRAY GIVING THE LAYER WIND SPEED IN MPS AT EACH XX,YY PNT.

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457* C
458* C
459* C
460* C
461* C
462* C
463* C
464* C
465* C
466* C
467* C
468* C
469* C
470* C
471* C
472* C
473* C
474* C
475* C
476* C
477* C
478* C
479* C
480* C
481* C
482* C
483* C
484* C
485* C
486* C
487* C
488* C
489* C
490* C
491* C
492* C
493* C
494* C

HM - ARRAY GIVING THE MIXING LAYER DEPTH IN METERS AT EACH XX,YY
      POINT
R - SCRATCH SPACE USED IN CONCENTRATION, ETC CALCULATIONS
SURFTA - SURFACE TEMP FROM ANALYSIS PHASE (DEG K)
POTMPK - POTENTIAL TEMP AT EACH LEVEL ZELEV (DEG K)
ZELVEVR - ELEVATION (METERS)

COMMON /DIFUZZ/ NETRAU,IULIAN,IMONTH,IDAY,THOUR,MINUTE,XSOURC,
1YSOURC,ZSOURC,SURFTA,POTMPR(25),ZELEV(25),XX(310),YY(310),
2UBAR(310),HM(310),R(3611)

C ** THE COMMON AREA DIFUZZ MUST BE GREATER THAN OR EQUAL IN SIZE TO
COMMON MXBUFR ABOVE. ALSO, WITH A GRID SPACING OF 5 KM THE PROG
USES 1/10 OR 500 M AS THE TRAJECTORY INCREMENT GIVING A MAXIMUM
OF 310 POINTS FROM ONE GRID SIDE TO THE OTHER. IF THE GRID SPACE
IS REDUCED FROM 5 KM TO A SMALLER VALUE THE ARRAY IN DIFUZZ
MAY HAVE TO BE INCREASED. IF SO SEE ALSO, REQUIRED CHANGES IN
SUBROUTINE TRNPRT
      END
NEWPRM PROC

C ** THIS PROC DEFINES DATA INPUT TO THE ANALYSIS PHASE. DATA IS
READ FROM UNIT XINFIL VIA NAMELIST GLST1 ONLY IF TYPE3 IN PROC
MESSAGE ABOVE IS NON-ZERO. IF NO INPUT IS DESIRED OR VARIABLES ARE
NOT IN INPUT LIST THEY DEFAULT TO VALUES GIVEN BELOW.

UN - U COMPONENT OF THE LAYER WIND SPEED (MPS) (UN IS CALCULATED
      IF NOT INPUT)
VN - V COMPONENT OF THE LAYER WIND SPEED (MPS) (VN IS CALCULATED
      IF NOT INPUT)
PN - ELEVATION OF THE MIXING LAYER ABOVE THE STATION OR SOURCE
      (METERS) (PN IS CALCULATED IF NOT INPUT)
GN - REDUCED GRAVITY PARAMETER FOR MESO-SCALE MODEL (DEFAULT =
      CALCULATED)
ABLKN - MINIMUM MIXING LAYER DEPTH CONSTRAINT (DEFAULT = 30 M)
SURFTN - SURFACE TEMPERATURE (DEGREES K) (DEFAULT = MET DATA BASE)
POTMPN - ARRAY CONTAINING THE POTENTIAL TEMP (DEG K) AT THE FIRST
      25 LEVELS (DEFAULT = MET DATA BASE)

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495* ZELEV - ARRAY CONTAINING THE ELEVATION (M) OF THE FIRST 25 LEVELS
496* (DEFAULT = MET DATA BASE)
497* DTLMON - MESO-SCALE MODEL STABILITY PARAMETER (DEFAULT = 0.4)
498* ISMTHN - NO. OF MESO-SCALE MODEL ITERATIONS BETWEEN APPLICATION
499* OF THE 9 POINT FILTER (DEFAULT = 7)
500* NCNTN - NO. OF MESO-SCALE MODEL ITERATIONS BETWEEN RECALCULATIONS
501* OF THE ITERATION TIME INTERVAL (DEFAULT = 2)
502* NETRDN - NET RADIATION INDEX (DEFAULT = MET DATA BASE)
503* KFLG1 - IF = 0 THE PROGRAM WILL USE A COLD OR A HOT START IN
504* THE MESO-SCALE MODEL DEPENDING ON WHETHER UN,VN, FN ARE
505* WITHIN 25% OF VALUES USED IN PREVIOUS SOLUTION.
506* IF # 0 THE PROGRAM WILL FORCE A COLD START OF MESO-SCALE
507* MODEL.
508* KFLG2 - IF = 0 THE PROGRAM WILL PRINT ONLY COMPLETION MESSAGES
509* IF # 0 THE PROGRAM WILL PRINT DETAILED DATA MESSAGES
510* COMMON /NEWPRM/ UN,VN,PN,GN,ABLKN,DTLMON,ISMTHN,NCNTN,NETRDN,
511* 1XSOURN,YSOURN,ZSOURN,SURFTN,POTMPN(25),ZELEVN(25),IFLG1,KFLG1,
512* 2KFLG2
513*
514* END
515* OBUFER PROC
516* UPPER AIR DATA INVENTORY
517* UASTNS - STATION NUMBER
518* UASTNA - STATION UTM X COORD IN KM
519* UASTNY - STATION UTM Y COORD IN KM
520* UASTNZ - STATION ELEVATION IN METERS
521* TLVLMX - NO. OF LEVELS OF TEMP. DATA FOR STATION,RUN
522* TADRES - DRUM ADDRESS OF TEMP DATA FOR STATION,RUN
523* WLVLMX - NO. OF LEVELS OF WIND DATA FOR STATION ,RUN
524* WADRES - DRUM ADDRESS OF WIND DATA FOR STATION ,RUN
525* LATEST - RUN INDEX FOR LATEST RUN
526* RUNMAX - MAX. NO. OF RUNS
527* STNMAX - MAX. NO. OF STATIONS
528* COMMON /OBUFER/ UASTNS(25),UASTNA(25),UASTNX(25),UASTNY(25),
529* 1UASTNZ(25),TLVLMX(25,3),TADRES(25,3),WLVLMX(25,3),WADRES(25,3)
530* 2,UATIME(3),LATEST,RUNMAX,STNMAX
531* INTEGER TLVLMX,WLVLMX,TADRES,WADRES,LATEST,RUNMAX,STNMAX,UATIME,
532* 1UASTNS

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533*      REAL UASTNX,UASTNY,UASTNZ,UASTNA
534*
535*      END
536*      TDATA
537*      C      PROC
538*      C      UPPER AIR DATA FOR PARTICULAR STATION, RUN
539*      C      PS - PRESSURE IN PASCALS (PASCALS*.01 = MB)
540*      C      QS -
541*      C      TS - TEMP DEG K
542*      C      ZS - ELEVATION METERS
543*      C      TV - VIRTUAL TEMP DEG K
544*      C      TA - POTENTIAL TEMP, DEG. K
545*      C      US,VS - WIND COMPONENTS MPS
546*      C      DELTA - HYDROSTATIC EQUATION EXPONENT
547*      C      PU - U-VALUE FOR PRESSURE LEVEL
548*      C      IMAX - NO. OF LEVELS
549*      C      COMMON /TDATA/ PS(40),QS(40),TS(40),ZS(40),TV(40),TA(40),US(40),
550*      C      REAL PS,PU,QS,TS,ZS,TV,TA,US,VS,DELTA
551*      C      INTEGER IMAX
552*
553*      END
554*      WDATA
555*      C      PROC
556*      C      UPPER AIR DATA -CONT-
557*      C      UW,VW - WIND COMPONENTS MPS
558*      C      ZW - ELEVATION METERS
559*      C      KMAX - NO. OF LEVELS
560*      C      COMMON /WDATA/ UW(40),VW(40),ZW(40),KMAX
561*
562*      END
563*      ABUFER
564*      C      PROC
565*      C      SCRATCH AREA
566*      C      COMMON /ABUFER/ A(5700)
567*
568*      END
569*      GWDATA
570*      C      GWC PREDICTION DATA
571*      C      GTIME - TIME
572*      C      P - PRESSURE (PASCALS)
573*      C      T - TEMP, DEG. K
574*      C      O - SPECIFIC HUMIDITY
575*      C      U,V - WIND COMPONENTS (MPS)
576*      C      Z - ELEVATION METERS

```

```

571* COMMON /GWDATA/ GTIME,P(4),Q(4),T(4),U(4),V(4),Z(4)
572* INTEGER GTIME
573*
574* ENU
575* SFDATA PROC
576* C SURFACE DATA
577* C STIME - TIME
578* C WD - WIND DIRECTION (DEG)
579* C WS - SPEED (MPS)
580* C WG - WIND GUSTS (MPS)
581* C SLP - SEA LEVEL PRESS (MB) (CONVERTED TO STATION PRESS. IN MB)
582* C BT - BAROMETRIC TENDENCY
583* C TSS - SURFACE TEMP (DEG K)
584* C TD - DEW POINT DEPRESSION (DEG K)
585* C AS - ALTIMETER SETTING (INCHES HG)
586* C PA - 6 HOURLY PRECIP. (MILLIMETERS)
587* C TSC - TOTAL SKY COVER
588* C PW - PAST WEATHER (WMO 4500)
589* C VV - VISIBILITY (M)
590* C WW1,WW2,WW3,WW4 - PRESENT WEATHER
591* C NH - FRACTION OF CELESTIAL DOME COVERED BY LOW CLOUDS (8 THS)
592* C CL - TYPE OF LOW CLOUD (WMO 0513)
593* C H - HEIGHT ABOVE GROUND OF LOWEST CLOUD (WMO 1600)
594* C CM - TYPE OF MIDDLE CLOUD (WMO 0515)
595* C CH - TYPE OF HIGH CLOUD (WMO 0509)
596* C NS - AMOUNT OF CLOUDS (8 THS)
597* C K - CLASSIFICATION OF CLOUDS ACCORDING TO HEIGHT
598* C CT - TYPE OF CLOUD WITHIN HEIGHT CLASSIFICATION
599* C HSHS - HEIGHT ABOVE GROUND OF BASE OF CLOUD LAYER (WMO 1677)
600* C COMMON /SFDATA/ STIME,WD,WS,WG,SLP,BT,TSS,TD,AS,PA,TSC,PW,VV,WW1,
601* C WW2,WW3,WW4,NH,CL,H,CM,CH,NS,K,CT,HSHS
602* C INTEGER STIME,TSC,PW,VV,WW1,WW2,WW3,WW4,CL,H,CM,CH,CT,HSHS,BT
603* C
604* C ENU
605* METPRM PROC
606* C COMMON /METPRM/ IFLAG1,IFLAG2,IFLAG3,IFLAG4,I1,J1,K1,IPASS,NUMHRS,
607* C INSTA1N,IDXSTA(25),STADST(25),STATNZ,STATNX,STATNY,TIME,NLVL,T,TS50,
608* C 2SF52,SAVSPD,SAVDIR,OBUFNR,UABLK,GWCBK,SFCBLK,MXU6LK,MXGBLK,MXSBLK
609* C 3,JUTIME,N850,N700
610* C
611* C ENU

```



```

609*      DEFIMP  PROC
610*      C      DEFAULT VALUES FOR INPUTS IN COMMON NEWPRM
611*      DATA UN,VN,PN,GN,ABLK,DTLMDN,ISMTHN,IUCNTN,NETRDN,XSOURN,YSOURN,
612*      1ZSOURN,SURFTN,POTMPN,ZELEVN,IFLG1,KFLG1,KFLG2/4*-99.0,30.0,
613*      20.4,7.2,-9,360000.0,3585000.0,1310.0,51*-99.0,3*0/
614*      END
615*      GBUFER  PROC
616*      COMMON /GBUFER/ GRIDX(25),GRIDY(25),GRDBLK(80),ANLTIM(80),RUNMAX,
617*      1GRDUMAX
618*      INTEGER GRDBLK,ANLTIM,RUNMAX,GRDUMAX
619*      END
620*      SBUFER  PROC
621*      COMMON /SBUFER/ SFCSTN(76),SFSTNA(76),SFSTNX(76),SFSTNY(76),
622*      1SFSTNZ(76),SAURES(76,6),RUNTIM(6),LATEST,RUNMAX,STNMAX
623*      INTEGER SFCSTN,SAURES,RUNTIM,LATEST,RUNMAX,STNMAX
624*      END
625*      TRPUTA  PROC
626*      COMMON /TRPUTA/ PT(3),GT(3),TI(3),ZT(3),TB(3),TI(3),UT(3),VT(3),
627*      1TD(3),NMAX
628*      END

```

1*	C	MAIN PROGRAM XECAMS	XEC00100
2*	C		XEC00200
3*		INCLUDE MESSAGE	XEC00300
4*		INCLUDE TIMES	XEC00400
5*	C	INCLUDE FILES	XEC00500
6*		SET UP FILES AND INITIALIZE ALL APPROPRIATE CONSTANTS	XEC00600
7*		XINFIL = 5	XEC00700
8*		XUTFIL = 6	XEC00800
9*		OLFILE = 0	XEC00900
10*		UAFIL = 1	XEC01000
11*		SFCOBF = 20	XEC01100
12*		SBFILE = 21	XEC01200
13*		GWCPFL = 10	XEC01300
14*		GWCFIL = 11	XEC01400
15*		WSTRN = 12	XEC01500
16*		MXLYRF = 13	XEC01600
17*		TROFFL = 14	XEC01700
18*		SPARE = 9	XEC01800
19*		MXBLKU = 18	XEC01900
20*		MXBLKG = 1	XEC02000
21*		MXBLKS = 120	XEC02100
22*		5 READ (XINFIL,1000,END=90) TYPE1,TYPE2,TYPE3,JULIAN,MONTH,DAY,HOUR,	XEC02200
23*		1 MINUTE,XPLACE,YPLACE,ZPLACE	XEC02300
24*		1000 FORMAT (813,3F10.2)	XEC02400
25*		10 GO TO (20,60,40,80),TYPE1	XEC02500
26*	C	20 CALL APPLICATION SUPERVISOR	XEC02600
27*		IF (TYPE3 .LT. 0) GO TO 90	XEC02700
28*		GO TO 5	XEC02800
29*	C	CALL ALTERNATE PROGS	XEC02900
30*		40 CONTINUE	XEC03000
31*	C	CALL OPYQC	XEC03100
32*		GO TO 5	XEC03200
33*	C	CALL ANALYSIS SUPERVISOR	XEC03300
34*		60 CALL ANALIZ	XEC03400
35*		IF (TYPE3 .LT. 0) GO TO 90	XEC03500
36*		GO TO 5	XEC03600
37*	C	WHAT NEXT	
38*			

XEC03700  
XEC03800  
XEC03900  
XEC04000  
XEC04100  
XEC04200

80 CONTINUE  
CALL PLTPRG  
IF (TYPE3 .LT. 0) GO TO 90  
GO TO 5  
90 STOP  
END

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ANA00100  
ANA00200  
ANA00300  
ANA00400  
ANA00500  
ANA00600  
ANA00700  
ANA00800  
ANA00900  
ANA01000  
ANA01100

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11*

SUBROUTINE ANALIZ
C ANALYSIS SUPERVISOR
INCLUDE MESSAGE
GO TO (20,20,30),TYPE2
C CALL MIXING LAYER ANALYSIS FOREMAN
20 CALL MIXLYR
GO TO 40
C OTHER ANALYSIS ROUTINES
30 CONTINUE
40 RETURN
END

```



1*		SUBROUTINE APPLY	APY000100
2*	C	THIS SUBROUTINE SUPERVISES THE APPLICATIONS ROUTINES	APY000200
3*		INCLUDE MESSAGE,LIST	APY000300
4*	C	SET UP APPROPRIATE CONSTANTS, ETC	APY000400
5*		GO TO (20,40,40),TYPE2	APY000500
6*	C	CALL THE TRANSPORT/DIFFUSION APPLICATION FOREMAN	APY000600
7*		20 CALL TRYDIF	APY000700
8*		GO TO 60	APY000800
9*	C	OTHER APPLICATIONS FOREMAN	APY000900
10*		40 CONTINUE	APY01000
11*		60 RETURN	APY01100
12*		END	APY01200



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B-27

SUBROUTINE MXUBAN  
INCLUDE TIMES,LIST  
INCLUDE ABUFFER,LIST  
INCLUDE FILES,LIST  
INCLUDE NEWPRM,LIST  
INCLUDE OBUFER,LIST  
INCLUDE TDATA,LIST  
INCLUDE WDATA,LIST  
INCLUDE SFDATA,LIST  
INCLUDE METPRM,LIST  
INCLUDE DEFINP,LIST  
INCLUDE MESSAGE,LIST  
DIMENSION KULIAN(12)  
INTEGER TIME,UABLK,GWCBK,SFCBLK,OBUFN  
DATA MXUBLK,MXGBLK,MXSBLK/30,1,120/  
DATA KULIAN/0,31,59,90,120,151,181,212,243,273,304,334/  
  
NAMELIST /GLST1/ UN,VN,PN,GN,ABLK, SURFTN,POTMPN,ZELEVN,DTLMDN,  
1ISMTHN,NCNTN,NETRUN,KFLG1,KFLG2  
  
IF (UN,LE,-99.0) GO TO 6  
UN = -99.0  
VN = -99.0  
PN = -99.0  
GN = -99.0  
ABLK = 30.0  
DTLMDN = 0.4  
ISMTHN = 7  
NCNTN = 2  
NETRUN = -9  
XSOURN = 360000.0  
YSOURN = 3585000.0  
ZSOURN = 1310.0  
SURFTN = -99.0  
IFLG1 = 0  
KFLG1 = 0  
KFLG2 = 0

C  
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C

MX000100  
MX000200  
MX000300  
MX000400  
MX000500  
MX000600  
MX000700  
MX000800  
MX000900  
MX001000  
MX001100  
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MX001900  
MX002000  
MX002100  
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MX002300  
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MX003600  
MX003700  
MX003800

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```

DO 5 I=1,25
  POTPIN(I) = -99.0
  5 ZELEV(I) = -99.0
  6 CONTINUE
  IF (TYPE3 .LE. 0) GO TO 10
  READ (XINFIL,QLST1,END=10)
  10 TYPE3 = IABS(TYPE3)
  IPASS = 74
  TIME = 0
  IF (MONTH .GT. 0 .AND. DAY .GT. 0) GO TO 30
  CALL ERTRAN(9,UATIME(1),UATIME(2))
  DECODE(12,9007,UATIME,L) MONTH,DAY,IPASS,HOUR,MINUTE,TIME
  JULIAN = KULIAN(MONTH)
  IF (MONTH.GT.2 .AND. MOD(IPASS,4).EQ.0) JULIAN = JULIAN+1
  30 UATIME(1) = JULIAN+DAY
  UATIME(2) = HOUR*100+MINUTE
  WRITE (XOIFIL,9006) IPASS,UATIME(1),MONTH,DAY,UATIME(2)
  IF (TYPE3 .EQ. 9) KFLG2 = 1
  IF (KFLG2 .GT. 0) WRITE (XOTFIL,QLST1)
  IF (MXBLKU .GT. 0) MXUBLK = MXBLKU
  IF (MXBLKG .GT. 0) MXGBLK = MXBLKG
  IF (MXBLKS .GT. 0) MXSBLK = MXBLKS
  IF (XPLACE .LE. 0.0) XPLACE = XSOURN
  IF (YPLACE .LE. 0.0) YPLACE = YSOURN
  IF (ZPLACE .LE. 0.0) ZPLACE = ZSOURN
  XSOURN = XPLACE
  YSOURN = YPLACE
  ZSOURN = ZPLACE
  SFSZ = ZSOURN
  SAVSPD = -99.0
  SAVDIR = -99.0
  UBRLYR = -99.0
  VERLYR = -99.0

```

C  
C  
C  
C  
C  
C

THIS SUBROUTINE CONTROLS THE CALCULATION OF THE MIXING LAYER DEPT.,  
THE LAYER WIND SPEED COMPONENTS AND THE NET RADIATION INDEX.

MX003900  
MX004000  
MX004100  
MX004200  
MX004300  
MX004400  
MX004500  
MX004600  
MX004700  
MX004800  
MX004900  
MX005000  
MX005100  
MX005200  
MX005300  
MX005400  
MX005500  
MX005600  
MX005700  
MX005800  
MX005900  
MX006000  
MX006100  
MX006200  
MX006300  
MX006400  
MX006500  
MX006600  
MX006700  
MX006800  
MX006900  
MX007000  
MX007100  
MX007200  
MX007300  
MX007400  
MX007500  
MX007600



```

77* C      CALC TIME OF SOLUTION DESIRED
78*      TIME = (DAY+JULIAN)*100+HOUR
79* C      DETERMINE STATION AND DATA FOR RAWINSONDE DATA
80*      OBUFRN = 431
81* C      LOOK FOR DATA FOR PAST 3 HOURS
82*      IPASS = 1
83*      CALL MXUADT
84*      IF (IFLAG1 .GT. 0) GO TO 100
85* C      3 HOUR NOT FOUND TRY FOR 12 HOURS
86*      IPASS = 2
87*      CALL MXUADT
88* C      IFLAG1 = 1 IS UPPER AIR DATA <= 3 HOURS OLD
89* C      IFLAG1 = 2 IS UPPER AIR DATA <= 12 HOURS OLD
90* C      IFLAG1 = 0 MEANS NO UPPER AIR DATA (DEFAULT HMLYR - LAYER DEPTH)
91*      IF (IFLAG1 .EQ. 0) SF52 = ZSOURN
92*      100 CONTINUE
93*      IFLAG2 = 0
94*      IF (IFLAG1 .EQ. 1.OR.IFLAG1 .EQ. 0) GO TO 200
95* C      DETERMINE IF THERE IS GWC DATA
96*      OBUFRN = 212
97* C      IFLAG2 = 0 NO GWC DATA
98* C      IFLAG2 = 1 GWC DATA PRESENT NO MOD OF RAWIN AT 700 MB, ETC.
99* C      IFLAG2 = 2 OR 3 GWC DATA PRESENT MOD RAWIN AT 700 MB AND REPLACE
100*      RAWIN WINDS AT 850 AND 700 MB
101*      IF = 3 THEN ALSO, AT 700 MB > 0
102*      CALL MXGWD(PS,TS)
103*      200 CONTINUE
104* C      DETERMINE SURFACE DATA
105*      OBUFRN = 845
106*      CALL MXSFD
107* C      IFLAG3 = 0 NO SURFACE DATA, DEFAULT NET RADIATION INDEX
108* C      IFLAG3 = 1 SURFACE DATA
109* C      IFLAG3 = 2 RAWIN MODIFIED WITH SURFACE DATA
110* C      IFLAG3 = 3 SAME AS 2 BUT ALSO, MODIFIED WITH GWC AT 850 MB
111* C      IFLAG3 = 4 SAME AS 3 BUT ALSO, AT AT 850 MB > 0
112*      IF (SURFTN .LE. 0.0.AND.TS(1) .GT. 0.0) SURFTN = TS(1)
113*      IF (IFLAG1 .EQ. 0) GO TO 500
114*      IF (IDIFTM(TIME,JUTIME) .LE. 6) GO TO 480

```

```

MX007700
MX007800
MX007900
MX008000
MX008100
MX008200
MX008300
MX008400
MX008500
MX008600
MX008700
MX008800
MX008900
MX009000
MX009100
MX009200
MX009300
MX009400
MX009500
MX009600
MX009700
MX009800
MX009900
MX010000
MX010100
MX010200
MX010300
MX010400
MX010500
MX010600
MX010700
MX010800
MX010900
MX011000
MX011100
MX011200
MX011300
MX011400

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```

115*      IF (IFLAG3 .LT. 3) IFLAG1 = 0
116*      +80 CONTINUE
117*      C      CALCULATE MIXING LAYER DEPTH
118*      CALL LYRAHM(UBRLYR,VBRLYR,HMLYR)
119*      IF (HMLYR .LE. 0.0.OR.HMLYR .GE. 9999.0) GO TO 500
120*      IF (PN .LE. -99.0) PN = HMLYR
121*      GO TO 530
122*      C      DEFAULT MIXING LAYER HEIGHT - HMLYR
123*      500 CALL LYRDHM(HMLYR,SFSZ)
124*      IF (PN .LE. -99.0) PN = HMLYR
125*      IFLAG4 = 1
126*      GO TO 600
127*      530 CONTINUE
128*      C      CALC GN
129*      IF (GN .GT. -0.1) GO TO 600
130*      SUM1 = 0.0
131*      SUM2 = 0.0
132*      L = 0
133*      540 L = L+1
134*      IF (L .GT. NLVLT) GO TO 590
135*      TLAST = TS(L)
136*      ZLAST = ZS(L)
137*      IF (TLAST .LE. 0.0.OR.ZLAST .LE. 0.0) GO TO 540
138*      550 L = L+1
139*      IF (L .GT. NLVLT) GO TO 590
140*      IF (ZS(L) .LE. 0.0.OR.TS(L) .LE. 0.0) GO TO 550
141*      IF (ZS(L) .GT. HMLYR) GO TO 560
142*      SUM1 = SUM1+(ZS(L)-ZLAST)*0.5*(TS(L)+TLAST)
143*      SUM2 = SUM2+(ZS(L)-ZLAST)
144*      ZLAST = ZS(L)
145*      TLAST = TS(L)
146*      GO TO 550
147*      560 IF (SUM2 .LE. 0.0) GO TO 590
148*      SUM1 = SUM1/SUM2
149*      SUM2 = 0.0
150*      L = L-1
151*      570 L = L+1
152*      IF (L .GT. NLVLT) GO TO 580

```

```

MX011500
MX011600
MX011700
MX011800
MX011900
MX012000
MX012100
MX012200
MX012300
MX012400
MX012500
MX012600
MX012700
MX012800
MX012900
MX013000
MX013100
MX013200
MX013300
MX013400
MX013500
MX013600
MX013700
MX013800
MX013900
MX014000
MX014100
MX014200
MX014300
MX014400
MX014500
MX014600
MX014700
MX014800
MX014900
MX015000
MX015100
MX015200

```







```

1* SUBROUTINE MXUOUT
2* THIS SUBROUTINE RETRIEVES THE UPPER AIR DATA
3* INCLUDE TIMES,LIST
4* INCLUDE NEWPRM,LIST
5* INCLUDE OBUFER,LIST
6* INCLUDE TDATA,LIST
7* INCLUDE WDATA,LIST
8* INCLUDE FILES,LIST
9* INCLUDE METPRM,LIST
10* EQUIVALENCE (I1,I),(J1,J),(K1,K)
11* INTEGER TIME,UABLK,OBUFN
12* DATA SAVSPD,SAVUIR/9999.,9999./
13* IPASS =1 IS LOOK FOR LESS THAN 3 HOURS
14* IPASS =2 IS LOOK FOR LESS THAN 12 HOURS
15* IPASS =3 IS NO HM FOUND COME BACK AND LOOK FOR OTHER DATA
16* IF (IPASS .LT. 3) UABLK = MXUUBLK+1
17* GO TO (90,100,110),IPASS
18* SET HOUR INTERVAL MAXIMUM TO 3 HOURS
19* NUMHRS = 3
20* IFLAG1 = 1
21* GO TO 120
22* SET HOUR INTERKVAL MAXIMUM TO 12 HOURS
23* NUMHRS = 12
24* IFLAG1 = 2
25* GO TO 120
26* CONTINUE
27* IPASS = 3 GOES HERE
28* CONTINUE
29* UABLK = UABLK-1
30* IF (UABLK .LE. 0) GO TO 400
31* LOAD BUFFER WITH UPPER AIR DATA INVENTORY
32* CALL BLKIN(OBUFN,UASINS,UABLK,OBFILE,ISTS)
33* CALC TIME DIFF
34* J = RUNMAX
35* J = J-1
36* IF (J .LE. 0) GO TO 120
37* IF (UATIME(J) .LE. 0) GO TO 130
38* L = IUIFTM(TIME,UATIME(J))

```

```

MXU00100
MXU00200
MXU00300
MXU00400
MXU00500
MXU00600
MXU00700
MXU00800
MXU00900
MXU01000
MXU01100
MXU01200
MXU01300
MXU01400
MXU01500
MXU01600
MXU01700
MXU01800
MXU01900
MXU02000
MXU02100
MXU02200
MXU02300
MXU02400
MXU02500
MXU02600
MXU02700
MXU02800
MXU02900
MXU03000
MXU03100
MXU03200
MXU03300
MXU03400
MXU03500
MXU03600
MXU03700
MXU03800

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39*      IF (L .LT. 0) GO TO 130
40*      IF (L .GT. NUMHRS) GO TO 400
41*      DETERMINE INDICES OF ALL STATIONS WITHIN 100 KM
42*      CALL GLSSIN(NSTATN,UASTNX,UASTNY,IDXSTA,STADST,STIMAX,100.)
43*      K = 0
44*      170 K = K+1
45*      IF (K .GT. NSTATN) GO TO 130
46*      I = IDXSTA(K)
47*      IF (TLVLMX(I,J) .LE. 0.OR.WLVLMX(I,J) .LE. 0) GO TO 170
48*      320 IMAX = TLVLMX(I,J)
49*      KMAX = WLVLMMX(I,J)
50*      CALL UADATA(I,J,IFLAG)
51*      M = FLD(35,1,IFLAG)
52*      L = FLD(34,1,IFLAG)
53*      IF (M.EQ. 0.AND.L .EQ. 0) GO TO 170
54*      PROVIDE DEFAULT SPD AND DIR IF NO OTHER DATA FOUND
55*      IF (ZS(1) .GT. 0.0) GO TO 350
56*      IF (ABS(US(1))+ABS(VS(1))) 355,355,350
57*      350 SAVSPU = US(1)
58*      SAVDIR = VS(1)
59*      GO TO 365
60*      355 IF (Z*(2) .GT. 0.0) GO TO 360
61*      IF (ABS(UW(2))+ABS(VW(2))) 365,365,360
62*      360 SAVSPU = UW(2)
63*      SAVDIR = VW(2)
64*      365 CONTINUE
65*      FOUND DATA - EXAMINE FOR ENOUGH DATA TO CALC HM
66*      IF (IMAX .LT. 3) GO TO 170
67*      M = 0
68*      N850 = 0
69*      N700 = 0
70*      DO 380 L=1,IMAX
71*      IF (ABS(PS(L)-85000.0) .GT. 100.0) GO TO 373
72*      N850 = L
73*      373 IF (ABS(PS(L)-70000.0) .GT. 100.0) GO TO 374
74*      N700 = L
75*      374 CONTINUE
76*      IF (TV(L) .LE. 0.0.OR.ZS(L) .LE. 0.0) GO TO 380

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77*      IF (PS(L) .GT. 0.0.AND.PS(L) .LT. 70000.0) GO TO 381
78*      M = M+1
79*      380 CONTINUE
80*      381 IF (M .LT. 3) GO TO 170
81*      JUTIME = UATIME(J)
82*      NLVLT = IMAX
83*      STATNZ = UASTNZ(I)
84*      STATNX = UASTNX(I)
85*      STATNY = UASTNY(I)
86*      DO 390 L=1,25
87*      IF (L .GT. NLVLT) GO TO 390
88*      IF (POTMPN(L) .LE. 0.0) POTMPN(L) = TA(L)
89*      IF (ZELEVN(L) .LE. 0.0) ZELEVN(L) = ZS(L)
90*      390 CONTINUE
91*      GO TO 500
92*      400 NSTATN = 0
93*      410 IFLAG1 = 0
94*      N850 = 0
95*      N700 = 0
96*      500 CONTINUE
97*      C* C
98*      IF (KFLG2 .EQ. 0) GO TO 630
99*      WRITE (XOTFIL,9000)
100*      IF (IFLAG1 .EQ. 0) GO TO 620
101*      WRITE (XOTFIL,9001) UABLK,J1,K1,UASTNS(I),STATNX,STATNY,STATNZ,
102*      JTIME,JUTIME
103*      *RITE (XOTFIL,9002)
104*      DO 600 M=1,NLVLT
105*      600 WRITE (XOTFIL,9003) M,PS(M),QS(M),TS(M),ZS(M),TV(M),TA(M),US(M),
106*      1VS(M),DELTA(M),PD(M)
107*      WRITE (XOTFIL,9004)
108*      DO 610 M=1,KMAX
109*      610 WRITE (XOTFIL,9005) M,UW(M),VW(M),ZW(M)
110*      GO TO 630
111*      620 WRITE (XOTFIL,9006) NUMHRS
112*      630 CONTINUE
113*      9000 FORMAT ('1 *** UPPER AIR DATA PROCESSED ***')
114*      9001 FORMAT ('0BLOCK=',I3,' RUN INDEX=',I2,' STA INDEX=',I3,' STATION=',MXU11400
MXU07700
MXU07800
MXU07900
MXU08000
MXU08100
MXU08200
MXU08300
MXU08400
MXU08500
MXU08600
MXU08700
MXU08800
MXU08900
MXU09000
MXU09100
MXU09200
MXU09300
MXU09400
MXU09500
MXU09600
MXU09700
MXU09800
MXU09900
MXU10000
MXU10100
MXU10200
MXU10300
MXU10400
MXU10500
MXU10600
MXU10700
MXU10800
MXU10900
MXU11000
MXU11100
MXU11200
MXU11300
MXU11400

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115*      1,16,' UTM X=',F8.3,' UTM Y=',F9.3,' UTM Z=',F9.3,' CALC FOR TIME=',MXU11500
116*      2,16,' OBS TIME=',I0)
117*      9002 FORMAT ('0 UPPER AIR OBS. PRESS. DATA', ' LEVEL PRESS. MIXING MXU11600
118*      1 TEMP ELEV VIRT-TEMP POT-TEMP U-SPD COMP V-SPD COMP HYDRO EQU MXU11700
119*      2 EXPO DEW PNT DEP',/6X,'(PASCALS) RATIO (DEG K) (M) (DEG K) MXU11800
120*      3 (DEG K) (M/S) (M/S)',/21X,'(DEG K)',)
121*      9003 FORMAT (2X,12,F10.1,E11.6,F7.2,F9.2,F8.2,F10.2,F11.2,E15.6,F1MXU11900
122*      11.2)
123*      9004 FORMAT ('0 UPPER AIR OBS. WIND DATA', ' LEVEL U-SPD COMP V-SPD COMP MXU12000
124*      1 ELEV',/10X,'(M/S)',/6X,'(M/S)',/4X,'(M)',)
125*      9005 FORMAT (2X,12,F11.2,F10.2)
126*      9006 FORMAT ('0 NO UPPER AIR DATA FOUND WITHIN ',I4,' HOURS, PROG CONTIMXU12100
127*      INUES')
128*      C*C
129*      RETURN
130*      END

```



```

1* SUBROUTINE MXGWD(T,PU,TU)
2* INCLUDE TIMES,LIST
3* INCLUDE NEWPRM,LIST
4* INCLUDE FILES,LIST
5* INCLUDE GWDATA,LIST
6* INCLUDE METPRM,LIST
7* INCLUDE ABUFER,LIST
8* INCLUDE GBUFER,LIST
9* INCLUDE TDATA,LIST
10* DIMENSION PU(1),TU(1)
11* INTEGER FLAG,TIME
12* INTEGER OBUFRN,GWCBLK
13* IFLAG2 = 0
14* GWCBLK = MXGBLK+1
15* GWCBLK = GWCBLK-1
16* IF (GWCBLK .LE. 0) GO TO 700
17* C OBTAIN GWC PREDICTION DATA INVENTORY
18* CALL BLKIN(OBUFRN,GRIDX(1),GWCBLK,GWCPFL,ISTS)
19* C FIND CLOSEST GWC STATION
20* CALL CLSSTN(NSSTATN,GRIDX,GRIDY,IDXSTA,STADST,GRDMAX,100.0)
21* IF (NSTATN .NE. 0) GO TO 200
22* GO TO 90
23* L = 0
24* L = L+1
25* IF (L .GT. NSTATN) GO TO 90
26* I = IDXSTA(L)
27* K = RUNMAX+1
28* K = K-1
29* IF (K .LT. 1) GO TO 205
30* IF (ANLTIM(K) .LE. 0) GO TO 210
31* IF (ANLTIM(K) .GT. JUTIME) GO TO 210
32* M = JUTIM(TIME,ANLTIM(K))
33* IF (M .GT. 18) GO TO 205
34* GTIME = TIME
35* IFLAG2 = 0
36* CALL GWCUTA(I,GRDBLK(K),FLAG)
37* IF (FLAG .EQ. 0) GO TO 205
38* IFLAG2 = 1

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```

39* IF (N850 .EQ. 0.0R,N700 .EQ. 0) GO TO 700
40* IF (T(3) .LE. 0.0OR,TS(N700) .LE. 0.0) GO TO 700
41* T850 = T(3)-TS(N700)
42* IF (ABS(T850) .GT. 5.0OR,Q(3) .LE. 0.0) GO TO 700
43* TS(N700) = T(3)
44* TV(N700) = (1.0+0.61*(Q(3)/(1.0-Q(3))))*T(3)
45* US(N850) = U(2)
46* VS(N850) = V(2)
47* US(N700) = U(3)
48* VS(N700) = V(3)
49* IFLAG2 = 2
50* IF (T850 .GT. 0.0) IFLAG2 = 3
51* GO TO 800
52* 700 CONTINUE
53* IFLAG2 = 0 NO DATA
54* 800 CONTINUE
55* IF (KFLG2 .EQ. 0) GO TO 820
56* WRITE (XOTFIL,9000)
57* IF (IFLAG2 .GT. 0) GO TO 810
58* WRITE (XOTFIL,9001)
59* GO TO 820
60* 610 WRITE (XOTFIL,9002) GWCBLK,K,I,GRIDX(I),GRIDY(I),TIME,ANLTIME(K),
61* 1GTIME
62* IF (IFLAG2 .GT. 1) WRITE (XOTFIL,9003) T850,T(3)
63* WRITE (XOTFIL,9004)
64* DO 815 I=1,4
65* 615 WRITE (XOTFIL,9005) I,P(I),Q(I),T(I),U(I),V(I),Z(I)
66* 820 CONTINUE
67* 9000 FORMAT ('1 *** GWC PREDICTION DATA PROCESSED ***')
68* 9001 FORMAT ('0 NO GWC DATA FOUND OR DATA DID NOT MEET RAOB MODIFICATION
69* 1N SPECS')
70* 9002 FORMAT ('0 BLOCK=,I3,' RUN INDEX=,I2,' STA INDEX=,I3,' UTM X=,
71* 1F8.3,' UTM Y=,F9.3,' CALC FOR TIME=,I6,' UPPER AIR OBS TIME=,I6,
72* 2,' GWC PRE TIME=,I6)
73* 9003 FORMAT (' DELTA T=,F8.3,' T AT 700=,F8.3,' RAWIN MODIFICATIONS
74* 1ADE')
75* 9004 FORMAT ('0 GWC PREDICTION DATA',/,' LEVEL PRESS. SPECIFIC TEMP.
76* 1U-SPD COMP V-SPD COMP ELEV.,/6X,'(PASCALS) HUM. (DEG K)

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MXG03900
MXG04000
MXG04100
MXG04200
MXG04300
MXG04400
MXG04500
MXG04600
MXG04700
MXG04800
MXG04900
MXG05000
MXG05100
MXG05200
MXG05300
MXG05400
MXG05500
MXG05600
MXG05700
MXG05800
MXG05900
MXG06000
MXG06100
MXG06200
MXG06300
MXG06400
MXG06500
MXG06600
MXG06700
MXG06800
MXG06900
MXG07000
MXG07100
MXG07200
MXG07300
MXG07400
MXG07500
MXG07600

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MXG07700  
MXG07800  
MXG07900  
MXG08000

2M/S) (M/S) (M)')  
9005 FORMAT (2X,I2,F10.1,E10.4,F8.2,F9.2,2F11.2)  
RETURN  
END

77\*  
78\*  
79\*  
80\*

MXS00100  
MXS00200  
MXS00300  
MXS00400  
MXS00500  
MXS00600  
MXS00700  
MXS00800  
MXS00900  
MXS01000  
MXS01100  
MXS01200  
MXS01300  
MXS01400  
MXS01500  
MXS01600  
MXS01700  
MXS01800  
MXS01900  
MXS02000  
MXS02100  
MXS02200  
MXS02300  
MXS02400  
MXS02500  
MXS02600  
MXS02700  
MXS02800  
MXS02900  
MXS03000  
MXS03100  
MXS03200  
MXS03300  
MXS03400  
MXS03500  
MXS03600  
MXS03700  
MXS03800

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1* SUBROUTINE MXSFDT
2* INCLUDE FILES,LIST
3* INCLUDE TIMES,LIST
4* INCLUDE TDATA,LIST
5* INCLUDE WDATA,LIST
6* INCLUDE NEWPRM,LIST
7* INCLUDE SFDATA,LIST
8* INCLUDE METPRM,LIST
9* INCLUDE SBUFER,LIST
10* INCLUDE ABUFER,LIST
11* INCLUDE GWDATA,LIST
12* DIMENSION JDXSTA(25),STBDST(25),SOLAR(3)
13* DIMENSION PTUS(40,8)
14* EQUIVALENCE (PTUS,PS)
15* REAL LAT,LON
16* LOGICAL CEILING
17* INTEGER FLAG,TIME
18* INTEGER OBUFRN,SFCBLK
19* DATA SOLAR/60.,35.,15./
20* THIS SUBROUTINE EXAMINES THE SURFACE DATA TO DETERMINE IF A
21* MODIFICATION OF THE RAWINSONDE DATA IS DESIRED AND ALSO TO
22* C CALCULATE THE NET RADIATION INDEX
23* ISW1 = 0
24* IFLAG3 = 0
25* NUMHRS = 3
26* NSTATN = 0
27* IF NO STATIONS WITHIN 3 HRS OLD DEFAULT NET RADIATION
28* SFCBLK = MXSBLK+1
29* 150 SFCBLK = SFCBLK-1
30* IF (SFCBLK .LE. 0) GO TO 350
31* GET SURFACE DATA INVENTORY
32* CALL BLKIN(OBUFRN,SFCSTN,SFCBLK,SFCOBF,ISTIS)
33* DETERMINE CLOSEST STATION WITHIN 50 KM
34* CALL CLSSTN(NSTATN,SFSTNX,SFSTNY,JDXSTA,STBDST,STNMAX,50.0)
35* C IF NO STATIONS TRY FOR NEXT BLOCK
36* L = 0
160 L = L+1
IF (L .GT. NSTATN) GO TO 150

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39* J = RUNMAX
40* J = J-1
41* IFLAG3 = 0
42* IF (J .LE. 0) GO TO 100
43* IF (RUNTIM(J) .LE. 0) GO TO 250
44* N = IDUFTIME(TIME,RUNTIM(J)/100)
45* IF (N .LT. 0) GO TO 250
46* IF (J .EQ. RUNJMAX.AND.N .GT. NUMHRS) GO TO 350
47* IF (N .GT. NUMHRS) GO TO 160
48* I = JDXSTA(L)
49* STIME = RUNTIM(J)
50* CALL ULKIN(5500,A(1),SFCBLK,SBFILE,ISTS)
51* CALL SFCDTA(1,J,FLAG)
52* IF (FLAG .EQ. 0) GO TO 250
53* PROVIDE FOR DEFAULT SPD AND DIR IF NO THERE
54* IF (WD .GT. 360.0) WD = -1.0
55* IF (WD .GE. 0.0) WD = WD+SFSINA(I)
56* IF (WD .LT. 0.0.OR.WS .LT. 0.0) GO TO 330
57* SAVDIR = (WD+180.0)*.01745329
58* SAVSPD = WS*SIN(SAVDIR)
59* SAVDIR = WS*COS(SAVDIR)
330 IF (ISW1 .EQ. 2) GO TO 700
60* SET LOCATION OF STATION
61* XST1 = SFSINX(1)*1.0E3
62* YST1 = SFSINY(1)*1.0E3
63* SFSZ = SFSINZ(1)
64* IF (SURFTN .LE. 0.0.AND.TSS .GT. 0.0) SURFTN = 1SS
65* SET STATION FOUND FLAG ON
66* ISW2 = 1
67* GO TO 400
68*
69* C DEFAULT LOCATION FOR NET RADIATION CALCULATION
70* 350 IF (ISW1 .GT. 0) GO TO 700
71* XST1 = XSOURN
72* YST1 = YSOURN
73* IF (IFLAG3 .EQ. 0) SFSZ = ZSOURN
74* TURN STATION FOUND FLAG OFF
75* ISW2 = 0
76* C CALCULATE THE NET RADIATION

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```

77* 400 CONTINUE
78*   C CALCULATE THE NET RADIATION INDEX - NETRON
79*   C FIRST CALC THE LONGITUDE AND LATITUDE
80*   C CALL LONLAT(XST1,YST1,LON,LAT)
81*   C USE DEFAULT IF ISW2 = 0
82*   C IF (ISW2.EQ. 0) GO TO 600
83*   C NOBS = FLAG/16
84*   C K = FLD(32,4,FLAG)
85*   C FLAG = K+1
86*   C DETERMINE CLOUD COVER AND CEILING- CLDCVR IN TENTHS, CEILING IF <2KM
87*   C THEN TRUE, ELSE FALSE
88*   C FLAG GIVES TYPE OF SURFACE DATA
89*   C FLAG = 1 SYNOPTIC
90*   C FLAG = 2 AIRWAYS
91*   C FLAG = 3 METAR
92*   C FLAG = 4 SYNOPTIC-AIRWAYS MERGED
93*   C FLAG = 5 SYNOPTIC-METAR MERGED
94*   C FLAG = 6 RESERVED
95*   C GO TO (500,540,560,500,560,560),FLAG
96*   C SYNOPTIC OR MERGED SYNOPTIC
97*   C 500 IF (TSC.LT. 0 .OR. TSC.GT. 9) GO TO 520
98*   C CLSDVR = TSC
99*   C 510 CLDCVR = CLDCVR*0.125
100*   C GO TO 550
101*   C 520 IF (NH.LT. 0 .OR. NH.GT. 9) GO TO 530
102*   C CLDCVR = NH
103*   C GO TO 510
104*   C 530 IF (NS.LT. 0 .OR. NS.GT. 9) GO TO 560
105*   C CLDCVR = NS
106*   C GO TO 510
107*   C AIRWAYS
108*   C 540 IF (IABS(TSC).GT. 10.OR.TSC.EQ. -1) GO TO 530
109*   C CLDCVR = IABS(TSC)*0.1
110*   C IF CEILING < 2 KM SET TRUE, ELSE SET FALSE
111*   C 550 IF (HSHS.LT. 0 .OR. HSHS.GT. 99) GO TO 560
112*   C IF (HSHS.LT. 56 .AND. HSHS.GT. 50) GO TO 560
113*   C CEILING = .TRUE.
114*   C IF (HSHS.GE. 57.AND.HSHS.LT. 90) CEILING = .FALSE.

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MXS07700
MXS07800
MXS07900
MXS08000
MXS08100
MXS08200
MXS08300
MXS08400
MXS08500
MXS08600
MXS08700
MXS08800
MXS08900
MXS09000
MXS09100
MXS09200
MXS09300
MXS09400
MXS09500
MXS09600
MXS09700
MXS09800
MXS09900
MXS10000
MXS10100
MXS10200
MXS10300
MXS10400
MXS10500
MXS10600
MXS10700
MXS10800
MXS10900
MXS11000
MXS11100
MXS11200
MXS11300
MXS11400

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115*      IF (HSHS .GT. 97) CEILING = .FALSE.
116*      GO TO 600
117*      ISW2 = 0
118*      C      CALCULATE 1 HOUR PAST SUNRISE TO 1 HOUR BEFORE SUNSET
119*      600 CALL DAYNIT(LON,LAT,SNRISE,SUNSET,ALPHA)
120*      C      DETERMINE THE PRESENT HOUR
121*      TIMES = HOUR+FLOAT(MINUTE)*1.6666666E-2
122*      NETRON = -1
123*      C      DETERMINE IF DAY OR NIGHT
124*      IF (SNRISE .GT. SUNSET) GO TO 604
125*      IF (TIMES .GE. SNRISE.AND.TIMES .LE. SUNSET) GO TO 630
126*      GO TO 605
127*      604 IF (TIMES .GE. SNRISE.OR.TIMES .LE. SUNSET) GO TO 630
128*      605 CONTINUE
129*      C      NIGHT TIME
130*      IF (ISW2 .EQ. 0) GO TO 610
131*      IF (CLDCVR .LE. 0.4) GO TO 620
132*      610 NETRON = -1
133*      GO TO 670
134*      620 NETRON = -2
135*      GO TO 670
136*      C      DAY TIME
137*      CONTINUE
138*      IF (ALPHA .GT. 90.0) ALPHA = ABS(ALPHA-180.0)
139*      DO 640 NETRON=1,3
140*      IF (ALPHA .GT. SOLAR(NETRON)) GO TO 650
141*      640 CONTINUE
142*      NETRON = 4
143*      650 NETRON = 5-NETRON
144*      NETRON = NETRON-1
145*      IF (ISW2 .EQ. 1) GO TO 660
146*      NETRON = NETRON-1
147*      GO TO 670
148*      660 IF (CLDCVR .LE. 0.5) GO TO 670
149*      NETRON = NETRON-1
150*      IF (CEILING) NETRON = NETRON-1
151*      IF (NETRON .LT. 1) NETRON = 1
152*      670 CONTINUE

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MXS11500
MXS11600
MXS11700
MXS11800
MXS11900
MXS12000
MXS12100
MXS12200
MXS12300
MXS12400
MXS12500
MXS12600
MXS12700
MXS12800
MXS12900
MXS13000
MXS13100
MXS13200
MXS13300
MXS13400
MXS13500
MXS13600
MXS13700
MXS13800
MXS13900
MXS14000
MXS14100
MXS14200
MXS14300
MXS14400
MXS14500
MXS14600
MXS14700
MXS14800
MXS14900
MXS15000
MXS15100
MXS15200

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```

153*      ISW1 = 1
154*      IF (ISW2 .EQ. 1) ISW1 = 2
155*      700 IF (N .GT. NUMHRS) GO TO 600
156*      C      CALCULATE THE SURFACE PRESSURE AT THE STATION
157*      IF (A5 .LE. 0.0) GO TO 710
158*      SLP = AS*(1.0-.0065*SFSTNZ(I)/288.0)*5.2658*1013.25/29.92
159*      GO TO 720
160*      710 IF (SLP .GT. 0.0.AND.ISS .GT. 0.0) GO TO 715
161*      C      MISSING DATA GO BACK IF NEEDED
162*      IF (ISW2 .EQ. 0.0K,IFLAG1 .GT. 1) GO TO 250
163*      GO TO 800
164*      715 CONTINUE
165*      SLP = EXP(ALOG(SLP)-SFSTNZ(I)/(29.29*ISS))
166*      720 CONTINUE
167*      IFLAG3 = 1
168*      IF (IFLAG1 .LE. 1) GO TO 800
169*      IF (ABS(SLP-PS(1)*.01) .GT. 10.0) GO TO 250
170*      IF (T0 .LE. 0.0) GO TO 250
171*      TS(1) = TSS
172*      T850 = 1.0-373.16/(TSS-TD)
173*      T850 = 1013.25*EXP(T850*(13.3185+T850*(-1.976+T850*(-.6445-.1299*
174*      1T850))))
175*      T850 = .622*T850/(PS(1)*.01-T850)
176*      TV(1) = (1.0+0.61*T850)*TSS
177*      IF (WD .LT. 0.0.OR.WS .LT. 0.0) GO TO 725
178*      VS(1) = (WD+180.0)*.0174532925
179*      US(1) = WS*SIN(VS(1))
180*      VS(1) = WS*COS(VS(1))
181*      725 CONTINUE
182*      IFLAG3 = 2
183*      IF (IFLAG2 .LT. 2) GO TO 730
184*      C      GWC MODS MADE
185*      IF (T(2) .LE. 0.0) GO TO 800
186*      T850 = T(2)-TSS
187*      IF (ABS(T850) .GT. 5.0) GO TO 730
188*      IF (Q(2) .LE. 0.0) GO TO 800
189*      IFLAG3 = 3
190*      IF (T050 .GT. 0.0) IFLAG3 = 4

```

```

MXS15300
MXS15400
MXS15500
MXS15600
MXS15700
MXS15800
MXS15900
MXS16000
MXS16100
MXS16200
MXS16300
MXS16400
MXS16500
MXS16600
MXS16700
MXS16800
MXS16900
MXS17000
MXS17100
MXS17200
MXS17300
MXS17400
MXS17500
MXS17600
MXS17700
MXS17800
MXS17900
MXS18000
MXS18100
MXS18200
MXS18300
MXS18400
MXS18500
MXS18600
MXS18700
MXS18800
MXS18900
MXS19000

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191\*  
192\*  
193\*  
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218\*  
219\*  
220\*  
221\*  
222\*  
223\*  
224\*  
225\*  
226\*  
227\*  
228\*

```

TS(N850) = T(2)
TV(N850) = (1.0+0.01*Q(2)/(1.0-Q(2)))*T(2)
US(N850) = U(2)
VS(N850) = V(2)
GO TO 740
730 IF (TS(N850) .LE. 0.0) GO TO 800
T850 = TS(N850)-TSS
IF (ABS(T850) .LE. 5.0) GO TO 740
IFLAG1 = 0
GO TO 800
C REMOVE LEVELS BETWEEN 850 MB AND SURFACE
740 DO 741 L=1,8
741 PTIUS(2,L) = PTIUS(N850,L)
N850 = 2
N = 2
M = N850+1
IF (M .GT. NLVLT) GO TO 781
REMOVE LEVELS BETWEEN 850 AND 800 MB
DO 755 L=M,NLVLT
IF (PS(L) .GT. 79900.0) GO TO 755
N = N+1
DO 750 K=L,8
750 PTIUS(N,K) = PTIUS(L,K)
IF (ABS(PS(L)-70000.0) .LE. 100.0) N700 = N
755 CONTINUE
NLVLT = N
IF (IFLAG2 .EQ. 3) GO TO 780
IF (IFLAG3 .EQ. 4) GO TO 781
REMOVE LEVELS BETWEEN 850 AND 700 MB
C 765 N = N850
DO 766 K=N700,NLVLT
N = N+1
DO 766 L=1,8
766 PTIUS(N,L) = PTIUS(K,L)
NLVLT = N
GO TO 781
780 IF (IFLAG3 .EQ. 4) GO TO 765
781 L = 0

```

MXS19100  
MXS19200  
MXS19300  
MXS19400  
MXS19500  
MXS19600  
MXS19700  
MXS19800  
MXS19900  
MXS20000  
MXS20100  
MXS20200  
MXS20300  
MXS20400  
MXS20500  
MXS20600  
MXS20700  
MXS20800  
MXS20900  
MXS21000  
MXS21100  
MXS21200  
MXS21300  
MXS21400  
MXS21500  
MXS21600  
MXS21700  
MXS21800  
MXS21900  
MXS22000  
MXS22100  
MXS22200  
MXS22300  
MXS22400  
MXS22500  
MXS22600  
MXS22700  
MXS22800

```

229*      782 L = L+1
230*      IF (L.GT. NLVLT) GO TO 800
231*      IF (ZS(L).GE. ZS(L-1)) GO TO 782
232*      M = L+1
233*      IF (M.GT. NLVLT) GO TO 786
234*      DO 785 K=1,NLVLT
235*      DO 785 N=1,8
236*      785 PTTUS(K-1,N) = PTTUS(K,N)
237*      L = L-1
238*      786 NLVLT = NLVLT-1
239*      GO TO 782
240*      800 CONTINUE
241*      C*
242*      IF (KFLG2.EQ. 0) GO TO 850
243*      WRITE (XOTFIL,9000)
244*      IF (IFLAG3.EQ. 0) GO TO 840
245*      WRITE (XOTFIL,9001) SFCBLK,J,I,SFCSTN(I),SFSINX(I),SFSINY(I),
246*      1SFSINZ(I),STIME
247*      WRITE (XOTFIL,9005) WU,WS,WG,SLP,BT,TSS,TD,AS,PA,TSC,PW,VV,WV1,WV2,MX$24700
248*      1,WV3,WV4,NH,CL,H,CM,CH,NS,K,CT,HSHS
249*      IF (IFLAG3.GE. 2) WRITE (XOTFIL,9002)
250*      840 IF (IFLAG3.EQ. 0) WRITE (XOTFIL,9003)
251*      WRITE (XOTFIL,9004) NEIRDN,ALPHA,SNRISE,SUNSET,AST1,YST1,LON,LAT,
252*      1SF52
253*      850 CONTINUE
254*      9000 FORMAT ('1 *** SURFACE DATA PROCESSED ***')
255*      9001 FORMAT ('0 BLCK=,I4, RUN INDEX=,I3, STA INDEX=,I3, STATION=MX$25500
256*      1,16, UTM X=,F8.3, UTM Y=,F9.3, UTM Z=,F8.3, SURF OBS TIME=MX$25600
257*      2,16)
258*      9002 FORMAT (' RAWIN MODIFICATIONS MADE')
259*      9003 FORMAT ('0 NO SURFACE DATA FOUND, DEFAULT NET RADIATION INDEX')
260*      9004 FORMAT ('0 NET RAD INDEX=,I3, SOL ALT ANG=,F8.3, SUN RISE +1HRMX$26000
261*      1=,F9.3, SUN SET -1HR=,F9.3, UTM X=,F10.2, UTM Y=,F11.2, LMX$26100
262*      2ONGITUDE=,F9.4, LATITUDE=,F9.4, SURFACE Z=,F9.3)
263*      9005 FORMAT ('0SURFACE DATA, DIR (DEG)=,F7.2, SPD (M/S)=,F7.2, WIMX$26300
264*      1ND GUSTS (M/S)=,F7.2, PRESS (MB)=,F7.2, BAROMETRIC TEND.=,IMX$26400
265*      28, TEMP (DEG K)=,F7.2, DEW PNT DEP (DEG K)=,F7.2, ALTIM SETMX$26500
266*      3TING (IN HG)=,F6.2, 6HR PRECIP (MM)=,F6.2, TOT SKY COVER (8IMX$26600

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```

4HS)=',I4,' PAST WEATHLR (WMO 4500)=',I6,', VIS (M)=',I6,', PRES *EMXS26700
5A *WI I=1,4 (WMO 4677)=',I4,', LOW CLDS (8THS)=',I4/', TYPE LOW CLMXS26800
6DS (WMO 513)=',I4,', HT LOW CLD (WMO 1600)=',I6,', TYPE MID CLD (WMO 515)=',I4,', AMT CLDS (8THS)=',I4, MXS26900
7MO 515)=',I4,', TYPE HI CLD (WMO 509)=',I4/', HT TO BASE CLMXS27000
8', CLASSIF CLDS=',I4,', TYPE CLD IN HT CLASS=',I4,', HT TO BASE CLMXS27100
9DS (WMO 1677)=',I6)

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C\*U

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RETURN
END

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MXS27200
MXS27300
MXS27400
MXS27500

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272*
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274*
275*

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1* SUBROUTINE LYRAHM(UBRLYR,VBRLYR,HMLYR)
2* INCLUDE FILES,LIST
3* INCLUDE NEWPRM,LIST
4* INCLUDE TDATA,LIST
5* INCLUDE WDATA,LIST
6* INCLUDE METPRM,LIST
7* INCLUDE SFDATA,LIST
8* INCLUDE GWDATA,LIST
9* REAL MINDPT
10* EQUIVALENCE (STATHT,STATNZ)
11* DATA OPDZMN/-0.0005/,MINDPT/100.0/,HMMAX/3000.0/,HMMIN/30.0/,
12* 1DMISS/0.0/
13* ISW = 0
14* HMLYR = -1.0
15* IF (IFLAG1.EQ. 0) GO TO 860
16* I = 0
17* I = I+1
18* IF (I.GT. NLVLT) GO TO 860
19* IF (PS(I).GT. 0.0.AND.PS(I).LT. 70000.0) GO TO 860
20* IF (ZS(I).LE. 0.0.OR.TV(I).LE. 0.0) GO TO 350
21* TLAST = TV(I)
22* ZLAST = ZS(I)
23* ZBASE = STATHT
24* HM = HMMAX+ZBASE
25* BASE = 0.0
26* HB = 0.0
27* ISW1 = 0
28* IB = 0
29* I = I+1
30* IF (I.GT. NLVLT) GO TO 540
31* IF (PS(I).GT. 0.0.AND.PS(I).LT. 70000.0) GO TO 540
32* IF (TV(I).LE. DMIS.OR.ZS(I).LE. DMIS) GO TO 490
33* TUIFF = TV(I)-TLAST
34* ZUIFF = ZS(I)-ZLAST
35* IF (ZUIFF.LE. 0.0) GO TO 490
36* OPDZ = TUIFF/ZUIFF
37* IF (OPDZ.LT. OPDZMN) GO TO 510
38* HB = HB+ZUIFF

```

B-48

```

LYR00100
LYR00200
LYR00300
LYR00400
LYR00500
LYR00600
LYR00700
LYR00800
LYR00900
LYR01000
LYR01100
LYR01200
LYR01300
LYR01400
LYR01500
LYR01600
LYR01700
LYR01800
LYR01900
LYR02000
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LYR02600
LYR02700
LYR02800
LYR02900
LYR03000
LYR03100
LYR03200
LYR03300
LYR03400
LYR03500
LYR03600
LYR03700
LYR03800

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LYR03900  
LYR04000  
LYR04100  
LYR04200  
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LYR04400  
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LYR05000  
LYR05100  
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LYR05300  
LYR05400  
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LYR06200  
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LYR06400  
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LYR06600  
LYR06700  
LYR06800  
LYR06900  
LYR07000  
LYR07100  
LYR07200  
LYR07300  
LYR07400  
LYR07500  
LYR07600

```

      IB = IB+1
      IF (IB .NE. 1) GO TO 505
      BASE = ZLAST
      TSAV = TLAST
505  CONTINUE
      IF (HB .GE. MINDPT) GO TO 530
      ISW1 = 1
      GO TO 520
510  HB = 0.0
      IF (ISW1 .NE. 1) GO TO 515
      I = I-1
      ISW1 = 0
      ZLAST = BASE
      TLAST = TSAV
      BASE = 0.0
      GO TO 490
515  BASE = 0.0
520  ZLAST = ZS(I)
      TLAST = TV(I)
      GO TO 490
530  HM = BASE
      IF (HM .LT. HMIN+ZBASE) HM = HMIN+ZBASE
      IF (HM .GT. HMAX+ZBASE) HM = HMAX+ZBASE
540  HMLYR = HM
      ISW = 1
      CALC LAYER SPU AND DIR
      ZLAST = HMLYR
      SUM1 = 0.0
      SUM2 = 0.0
      SUM3 = 0.0
      ILVL = 0
      ZLST1 = ZBASE
      IB = 0
      J = 0
      J = J+1
600  IF (ZLST1 .GE. ZLAST) GO TO 850
      IF (J .GT. NLVLT) GO TO 850

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LYR07700  
LYR07800  
LYR07900  
LYR08000  
LYR08100  
LYR08200  
LYR08300  
LYR08400  
LYR08500  
LYR08600  
LYR08700  
LYR08800  
LYR08900  
LYR09000  
LYR09100  
LYR09200  
LYR09300  
LYR09400  
LYR09500  
LYR09600  
LYR09700  
LYR09800  
LYR09900  
LYR10000  
LYR10100  
LYR10200  
LYR10300  
LYR10400  
LYR10500  
LYR10600  
LYR10700  
LYR10800  
LYR10900  
LYR11000  
LYR11100  
LYR11200  
LYR11300  
LYR11400

```

IF (ZS(J) .LE. DMIS) GO TO 800
IF (ZS(J) .LT. ZLST1) GO TO 800
IF (ID .EQ. 0) GO TO 830
IF (ZS(J) .LE. ZLAST) GO TO 810
INTERP
UB = US(J) - (ZS(J) - ZLAST) * (US(J) - ULST) / (ZS(J) - ZLST1)
VB = VS(J) - (ZS(J) - ZLAST) * (VS(J) - VLST) / (ZS(J) - ZLST1)
HT = ZLAST
GO TO 820
810 UB = US(J)
VB = VS(J)
HT = ZS(J)
820 SUM1 = SUM1 + (HT - ZLST1) * 0.5 * (UB + ULST)
SUM2 = SUM2 + (HT - ZLST1) * 0.5 * (VB + VLST)
SUM3 = SUM3 + (HT - ZLST1)
GO TO 840
830 UB = US(J)
VB = VS(J)
HT = ZS(J)
IB = 1
840 ULST = UB
VLST = VB
ZLST1 = HT
GO TO 800
850 IF (SUM3 .LE. 0.0) GO TO 860
UBRLYR = SUM1/SUM3
VBRLYR = SUM2/SUM3
GO TO 900
860 CONTINUE
900 CONTINUE
IF (KFLG2 .EQ. 0) GO TO 921
IF (ISW .EQ. 0) GO TO 910
WRITE (XOTFIL,9000) HMLYR
GO TO 911
910 WRITE (XOTFIL,9001)
911 WRITE (XOTFIL,9002)
DO 920 I=1,NLVL
WRITE (XOTFIL,9003) I,PS(I),TS(I),ZS(I),TV(I),US(I),VS(I)

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116*
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120*
121*
122*
123*

920 CONTINUE
921 CONTINUE
9000 FORMAT ('0',5X,'*--* CALCULATED HM =',F9.3)
9001 FORMAT ('0',5X,'*--* HM NOT CALCULATED, MUST DEFAULT')
9002 FORMAT ('0 DATA USED TO CALC HM -',' LEVEL PRESS. TEMP.
1. VIRT TEMP U-SPD COMP V-SPD COMP,/6X,',(PASCALS) (DEG K)
2. (DEG K) (M/S)')
9003 FORMAT (2X,I2,F10.2,3F9.2,F10.2,F11.2)
END

```

```

LYR11500
LYR11600
LYR11700
LYR11800
ELEV LYR11900
(M) LYR12000
LYR12100
LYR12200
LYR12300

```

```

1* SUBROUTINE LYKDHM(HMLYR,SFSZ)
2* INCLUDE TIMES,LIST
3*
4* SUBROUTINE PROVIDES DEFAULT MIXING LAYER DEPTH DEPENDING ON THE
5* HOUR AND MONTH
6*
7* DIMENSION IDFHM(12,16)
8* DATA IDFHM/ 3*30,50,11*30,107,110,139,103,35,6*30,114,326,467,403,
9* 329,238,129,69,2*30,64,122,387,740,865,691,688,615,490,271,165,96,
10* 232,329,832,1255,1298,1274,1034,1042,933,539,400,239,434,639,1247,
11* 1761,1907,2053,1342,1431,1343,873,593,369,645,1054,1518,2177,2521,
12* 2654,1868,1840,1708,1217,792,533,822,1363,1804,2513,2915,2983,
13* 2388,2347,1896,1554,1025,734,907,1543,2145,2872,3195,3162,2503,
14* 2749,1940,1711,1126,718,753,1586,2276,2843,3292,3144,2116,2484,
15* 2038,1344,1039,435,386,1148,1635,1954,2727,3065,1279,1572,1762,
16* 696,609,206,102,436,946,824,1578,2606,516,816,932,280,231,102,30,
17* 68,255,229,549,1466,191,398,252,181,71,35,30,111,30,63,77,427,172,
18* 115,30,164,45,2*30,142,4*30,153,2*30,77,14*30/
19* DETERMINE HOUR INDEX
20* IF (HOUR .GT. 4.AND.HOUR .LT. 14) GO TO 10
21* HOUR = HOUR-13
22* IF (HOUR .LE. 0) HOUR = 24+HOUR
23* GO TO 20
24* 10 HOUR = 16
25* 20 CONTINUE
26* HMLYR = FLOAT(IDFHM(MONTH,HOUR))+SFSZ
27* RETURN
28* END

```



```

1* SUBROUTINE CLSSTN(NSTATN,X,Y,IDXSTA,STADST,STNMAX,DISTMN)
2* INCLUDE NEWPRM,LIST
3*
4* C DETERMINE THE CLOSEST STATION WITHIN DISTANCE DISTMN AND ORDER
5* C STATIONS IN ASCENDING ORDER OF DISTANCE
6* C DIMENSION X(1),Y(1),IDXSTA(1),STADST(1)
7* C INTEGER STNMAX
8* C NSTATN = 0
9* C XSOURS = XSOURN*1.0E-3
10* C YSOURS = YSOURN*1.0E-3
11* C N = STNMAX
12* C IF (N.GT. 25) N = 25
13* C DO 100 I=1,N
14* C CALCULATE DISTANCE FROM RELEASE TO STATION
15* C D = SQRT((X(I)-XSOURS)**2+(Y(I)-YSOURS)**2)
16* C IF (D.GT. DISTMN) GO TO 100
17* C NSTATN = NSTATN + 1
18* C IUXSTA(NSTATN) = I
19* C STADST(NSTATN) = D
20* C
21* C 100 CONTINUE
22* C IF (NSTATN.LT. 2) GO TO 120
23* C DO 110 J=2,NSTATN
24* C DO 110 I=2,NSTATN
25* C IF (STADST(I-1) .LE. STADST(I)) GO TO 110
26* C D = STADST(I)
27* C K = IUXSTA(I)
28* C STADST(I) = STADST(I-1)
29* C IUXSTA(I) = IUXSTA(I-1)
30* C STADST(I-1) = D
31* C IUXSTA(I-1) = K
32* C 110 CONTINUE
33* C 120 RETURN
    END
CLS00100
CLS00200
CLS00300
CLS00400
CLS00500
CLS00600
CLS00700
CLS00800
CLS00900
CLS01000
CLS01100
CLS01200
CLS01300
CLS01400
CLS01500
CLS01600
CLS01700
CLS01800
CLS01900
CLS02000
CLS02100
CLS02200
CLS02300
CLS02400
CLS02500
CLS02600
CLS02700
CLS02800
CLS02900
CLS03000
CLS03100
CLS03200
CLS03300

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```

COMPILER(DIAG=3)
SUBROUTINE UADATA(STN,RUN,FLAG)
INCLUDE ABUFER
INCLUDE OBUFER
INCLUDE FILES
INCLUDE TDATA
INCLUDE WDATA
INCLUDE TRPDIA
REAL OP(40),D(40),S(40)
REAL ANGLE,OFFSET,PO,RADPDG
REAL GAMA,PSTU(2),TSTD(2),ZSTD
INTEGER BLOCK,NEWBLK
INTEGER STN,RUN
INTEGER TADS,WADS
INTEGER FLAG
EQUIVALENCE (OP,GS),(D,UW),(S,VW)
DATA PO,RADPDG /100000.,0.01745329252/
DATA GAMA, PSTD, TSTD, ZSTD,
* /,0.005, 101325.,20980., 288.15,216.65, 11476./
DATA CONSTA /0.0341672473/

C EXTRACT DATA
NEWBLK = TADRES(STN,RUN)/10000
IF(NEWBLK.EQ.BLOCK) GO TO 50
BLOCK = NEWBLK
CALL BLKIN(5000,A(1),BLOCK,UAFILE,ISTAT)
50 CONTINUE
NEWBLK = NEWBLK*10000
TADS = TADRES(STN,RUN) + 1 - NEWBLK
WADS = WADRES(STN,RUN) + 1 - NEWBLK
FLAG = FLU(2,2,A(TADS-1))
IF(FLD(0,6,A(WADS)).EQ.0) GO TO 60
U(1) = 0.0
S(1) = 0.0
ZM(1) = UASTNZ(STN)
KMAX = KMAX + 1
GO TO 70
60 CONTINUE
FLAG = FLAG+4

```

UAD00100  
UAD00200  
UAD00300  
UAD00400  
UAD00500  
UAD00600  
UAD00700  
UAD00800  
UAD00900  
UAD01000  
UAD01100  
UAD01200  
UAD01300  
UAD01400  
UAD01500  
UAD01600  
UAD01700  
UAD01800  
UAD01900  
UAD02000  
UAD02100  
UAD02200  
UAD02300  
UAD02400  
UAD02500  
UAD02600  
UAD02700  
UAD02800  
UAD02900  
UAD03000  
UAD03100  
UAD03200  
UAD03300  
UAD03400  
UAD03500  
UAD03600  
UAD03700  
UAD03800

```

39* 70 CONTINUE
40*   IF(IMAX,GT,40) IMAX = 40
41*   CALL XTRCUA(A(TADS),PS,IMAX,40,FLAG,1)
42*   IF(IMAX,LE,1) GO TO 800
43*   IF(KMAX,GT,40) KMAX = 40
44*   CALL XTRCUA(A(WADS),U,KMAX,40,FLAG,2)
45*   IF(KMAX,LE,1) GO TO 800
46*   NMAX = FLU(18,9,A(TADS-1)) / 3
47*   IF(NMAX,EG,0) GO TO 80
48*   IF(NMAX,GT,3) NMAX = 3
49*   TAUS = TAUS + FLU(9,9,A(TADS-1)) - 1
50*   CALL XTRCUA(A(TADS),PT,NMAX,3,FLAG,3)
51*
52* 80 CONTINUE
53*  C EVALUATE WIND COMPONENTS RELATIVE TO BNL UTM GRID
54*   OFFSET = UASTNA(STN)
55*   DO 100 K = 1,KMAX
56*     ANGLE = RADPDG*(D(K) + OFFSET)
57*     UW(K) = -S(K)*SIN(ANGLE)
58*     VW(K) = -S(K)*COS(ANGLE)
59*
60* 100 CONTINUE
61*  C EVALUATE PRESSURE LEVEL DATA
62*   IF(FLU(32,1,FLAG),NE,0) GO TO 135
63*   K = 2
64*   ZS(1) = UASTNZ(STN)
65*
66* 105 CONTINUE
67*   IF(DP(K),LT,0) GO TO 110
68*   DZ = 62.2*SATVP(TS(K) - DP(K)) / PS(K)
69*   DZ = DZ / (1.-0.61*DZ)
70*   TV(K) = TS(K) * (1.0 + 0.61 * DZ)
71*   GO TO 115
72*
73* 110 CONTINUE
74*   TV(K) = TS(K)
75*
76* 115 CONTINUE
77*   IF(ZS(K),GT,0.) GO TO 120
78*   K = K + 1
79*   GO TO 105
80*
81* 120 CONTINUE
82*   IF(K,EQ,2) GO TO 130

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UAD03900
UAD04000
UAD04100
UAD04200
UAD04300
UAD04400
UAD04500
UAD04600
UAD04700
UAD04800
UAD04900
UAD05000
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UAD06400
UAD06500
UAD06600
UAD06700
UAD06800
UAD06900
UAD07000
UAD07100
UAD07200
UAD07300
UAD07400
UAD07500
UAD07600

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```

77*      DO 125 I = K,3,-1
78*      DELTA(I) = ALOG(PS(I) / PS(I-1)) / ALOG(TV(I) / TV(I-1))
79*      ZS(I-1) = ZS(I) + DELTA(I) * (TV(I) - TV(I-1)) / CONSTA
80*      125 CONTINUE
81*      130 CONTINUE
82*      DZ = ZS(2) - ZS(1)
83*      TS(1) = TS(2) + GAMA * DZ
84*      DP(1) = DP(2)
85*      PS(1) = PS(2) * (TS(1) / TS(2))**(CONSTA / GAMA)
86*      135 CONTINUE
87*      K = 2
88*      DZA = (ZW(2) - ZW(1))
89*      DO 400 I = 1,IMAX
90*      IF(DP(I).LT.0.) GO TO 140
91*      QS(1) = 62.2*SATVP(TS(I) - DP(I))/PS(I)
92*      GS(1) = QS(1)/(1. - 0.61*GS(I))
93*      TV(1) = (1. + 0.61*QS(I))*TS(I)
94*      GO TO 160
95*      140 CONTINUE
96*      GS(I) = 0.0
97*      TV(I) = TS(I)
98*      160 CONTINUE
99*      TA(1) = TS(I)*(PO/PS(I))*0.286
100*      IF(1.EQ.1) GO TO 300
101*      IF(TV(I).EQ.TV(I-1)) GO TO 200
102*      DELTA(I) = ALOG(PS(I)/PS(I-1))/ALOG(TV(I)/TV(I-1))
103*      IF (ZS(I).LT.0.)
104*      125(I) = ZS(I-1) - DELTA(I)*(TV(I) - TV(I-1))/CONSTA
105*      GO TO 300
106*      200 CONTINUE
107*      DELTA(I) = 0.0
108*      IF (ZS(I).LT.0.)
109*      125(I) = ZS(I-1) - TV(I)*ALOG(PS(I)/PS(I-1))/CONSTA
110*      300 CONTINUE
111*      DZ = ZW(K) - ZS(I)
112*      IF(DZ) 320,340,360
113*      320 CONTINUE
114*      IF(K.GE.KMAX) GO TO 500

```

UAD07700  
UAD07800  
UAD07900  
UAD08000  
UAD08100  
UAD08200  
UAD08300  
UAD08400  
UAD08500  
UAD08600  
UAD08700  
UAD08800  
UAD08900  
UAD09000  
UAD09100  
UAD09200  
UAD09300  
UAD09400  
UAD09500  
UAD09600  
UAD09700  
UAD09800  
UAD09900  
UAD10000  
UAD10100  
UAD10200  
UAD10300  
UAD10400  
UAD10500  
UAD10600  
UAD10700  
UAD10800  
UAD10900  
UAD11000  
UAD11100  
UAD11200  
UAD11300  
UAD11400



```

115*      K = K+1
116*      DZw = Zw(K) - Zw(K-1)
117*      GO TO 300
118* 340 CONTINUE
119*      Us(1) = Uw(K)
120*      Vs(1) = Vw(K)
121*      GO TO 370
122* 360 CONTINUE
123*      Dz = Dz/DZw
124*      Us(1) = Uw(K) - Dz*(Uw(K) - Uw(K-1))
125*      Vs(1) = Vw(K) - Dz*(Vw(K) - Vw(K-1))
126* 370 CONTINUE
127*      IF (PS(1).LT.PSTD(2)) GO TO 380
128*      PU(1) = Zs(1) - TSTD(1)*(1.0-(PS(1)/PSTD(1))**(GAMA/CONSTA))/GAMA
129*      GO TO 400
130* 380 CONTINUE
131*      PU(1) = Zs(1) - ZSTD + TSTD(2)*ALOG(PS(1)/PSTD(2))/CONSTA
132* 400 CONTINUE
133*      GO TO 600
134* 500 CONTINUE
135*      IMAX = I-1
136* 600 CONTINUE
137*      IF (NMAX.EQ.0) GO TO 760
138*      I = 1
139*      K = 1
140* 610 CONTINUE
141*      K = K + 1
142*      IF (K.GT.IMAX) GO TO 720
143*      IF (PS(K) - PT(1)) 640,620,610
144* 620 CONTINUE
145*      VT(1) = GS(K)
146*      TB(1) = TV(K)
147*      TI(1) = TA(K)
148*      TD(1) = PD(K)
149*      ZT(1) = ZS(K)
150*      IF ((UT(1).LT.0.0).OR. (VT(1).LT.0.0)) GO TO 630
151*      ANGLE = RADPDG*(UT(1) + OFFSET)
152*      UT(1) = -VT(1) * SIN(ANGLE)

```

```

153* VT(I) = -VT(I) * COS(ANGLE)
154* US(K) = UT(I)
155* VS(K) = VT(I)
156* GO TO 700
157* 630 CONTINUE
158* UT(I) = US(K)
159* VT(I) = VT(K)
160* GO TO 700
161* 640 CONTINUE
162* IF(UT(I).LT.0.) GO TO 650
163* QT(I) = 62.2 * SATVP(TT(I) - QT(I)) / PT(I)
164* QT(I) = QT(I) / (1.0-0.61*QT(I))
165* TB(I) = (1.0+0.61*QT(I)) * TT(I)
166* GO TO 680
167* 650 CONTINUE
168* GT(I) = 0.0
169* TB(I) = TT(I)
170* 660 CONTINUE
171* TI(I) = TT(I) * (PO/PT(I)) ** 0.286
172* IF(TB(I).EQ.TV(K-1)) GO TO 670
173* DZW = ALOG(PT(I)/PS(K-1)) / ALOG(TB(I) / TV(K-1))
174* ZT(I) = ZS(K-1) - DZW * (TB(I) - TV(K-1)) / CONSTA
175* GO TO 680
176* 670 CONTINUE
177* ZT(I) = ZS(I-1) - TB(I) * ALOG(PT(I) / PS(K-1)) / CONSTA
178* 680 CONTINUE
179* IF((UT(I).LT.0.0).OR.(VT(I).LT.0.0)) GO TO 690
180* ANGLE = RADPDG * (UT(I) + OFFSET)
181* UT(I) = -VT(I) * SIN(ANGLE)
182* VT(I) = -VT(I) * COS(ANGLE)
183* GO TO 700
184* 690 CONTINUE
185* DZW = (ZT(I) - ZS(K-1)) / (ZS(K) - ZS(K-1))
186* UT(I) = US(K-1) + (US(K) - US(K-1)) * DZW
187* VT(I) = VS(K-1) + (VS(K) - VS(K-1)) * DZW
188* 700 CONTINUE
189* I = I + 1
190* IF(I.LE.NMAX) GO TO 610

```

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UAD15300
UAD15400
UAD15500
UAD15600
UAD15700
UAD15800
UAD15900
UAD16000
UAD16100
UAD16200
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UAD16700
UAD16800
UAD16900
UAD17000
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UAD17900
UAD18000
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UAD19000

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GO TO 760  
720 CONTINUE  
NMAX = I - 1  
760 CONTINUE  
RETURN  
800 CONTINUE  
C INADEQUATE DATA, ELIMINATE OB FROM INVENTORY  
WRITE(6,900) FLAG,IMAX,KMAX,TADS,WADS,  
\* A(TADS-1),A(TADS),A(WADS-1),A(WADS)  
900 FORMAT(' FL,IMX,KMX,TAD,WAD',5I10/  
\* , A(T-1),A(T),A(W-1),A(W)',4(2X012))  
FLAG = 0  
TLVLMX(STN, RUN) = 0  
WLVLMX(STN, RUN) = 0  
RETURN  
END

UAD19100  
UAD19200  
UAD19300  
UAD19400  
UAD19500  
UAD19600  
UAD19700  
UAD19800  
UAD19900  
UAD20000  
UAD20100  
UAD20200  
UAD20300  
UAD20400  
UAD20500  
UAD20600

XTR00100  
XTR00200  
XTR00300  
XTR00400  
XTR00500  
XTR00600  
XTR00700  
XTR00800  
XTR00900  
XTR01000  
XTR01100  
XTR01200  
XTR01300  
XTR01400  
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XTR01700  
XTR01800  
XTR01900  
XTR02000  
XTR02100  
XTR02200  
XTR02300  
XTR02400  
XTR02500  
XTR02600  
XTR02700  
XTR02800  
XTR02900  
XTR03000  
XTR03100  
XTR03200  
XTR03300  
XTR03400  
XTR03500  
XTR03600  
XTR03700  
XTR03800

```

SUBROUTINE XTRCUA (A,B,LEVEL,N,FLAG,BRANCH)
  REAL    B(N,4)
  INTEGER A(1),BRANCH,FLAG,INDI,LEVEL,SIGN(3)
  DATA SIGN /00000000007777,
              00000000001777,
              00000000377777 /
  *
  *
  C
  J = 1
  L = 1
  IF (BRANCH - 1) 1000,20,400
20 CONTINUE
  INDI = FLD(0,0,A(J))
  IF (INDI.EQ.0) GO TO 80
  INDI = FLD(13,12,A(J))
  J = J + 2
  IF (INDI.NE.SIGN(1)) GO TO 60
  LEVEL = LEVEL - 1
  IF (LEVEL.GT.0) GO TO 20
  GO TO 700
60 CONTINUE
  L = 2
  LEVEL = LEVEL + 1
  IF (LEVEL.GT.N) LEVEL = N
  GO TO 100
80 CONTINUE
  FLAG = FLAG + 8
100 CONTINUE
  INDI = FLD(0,0,A(J))
  IF (INDI.GT.2) GO TO 360
  INDI = FLD(13,12,A(J))
  IF (INDI.EQ.SIGN(1)) GO TO 360
  B(L,3) = FLOAT(INDI)/10,
  INDI = FLD(26,10,A(J))
  IF (INDI.NE.SIGN(2)) GO TO 160
  B(L,2) = -1.0
  GO TO 200
160 CONTINUE
  B(L,2) = FLOAT(INDI)/10.0

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200 CONTINUE  
INDI = FLD(1,17,A(J+1))  
IF(INDI.EQ.SIGN(3)) GO TO 360  
B(L,1) = INDI\*10  
INDI = FLD(19,17,A(J+1))  
IF(INDI.NE.SIGN(3)) GO TO 260  
B(L,4) = -1.0  
GO TO 300  
260 CONTINUE  
B(L,4) = INDI  
300 CONTINUE  
L = L+1  
320 CONTINUE  
IF(L.GT.LEVEL) GO TO 700  
J = J+2  
GO TO 100  
360 CONTINUE  
LEVEL = LEVEL - 1  
GO TO 320  
400 CONTINUE  
IF(BRANCH.NE.2) GO TO 800  
IF(FLD(2,1,FLAG).EQ.1) GO TO 420  
L = 2  
420 CONTINUE  
INDI = FLD(0,6,A(J))  
IF(INDI.GT.2) GO TO 660  
INDI = FLD(12,12,A(J))  
IF(INDI.EQ.SIGN(1)) GO TO 660  
B(L,1) = INDI  
INDI = FLD(24,12,A(J))  
IF(INDI.EQ.SIGN(1)) GO TO 660  
B(L,2) = FLOAT(INDI)/10.  
500 CONTINUE  
INDI = FLD(19,17,A(J+1))  
IF(INDI.EQ.SIGN(3)) GO TO 660  
B(L,3) = INDI  
600 CONTINUE  
L = L+1

XTR03900  
XTR04000  
XTR04100  
XTR04200  
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XTR04400  
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XTR11200  
XTR11300  
XTR11400

```

620 CONTINUE
    IF(L.GT.LEVEL) GO TO 700
    J = J+2
    GO TO 420
660 CONTINUE
    LEVEL = LEVEL - 1
    GO TO 620
700 CONTINUE
    IF(LEVEL.LT.0) LEVEL = 0
    RETURN
800 CONTINUE
    IF(BRANCH.NE.3) GO TO 1000
    INDI = FLD(0,6,A(J))
    IF(INDI.NE.5) GO TO 960
    INDI = FLD(13,12,A(J))
    IF(INDI.EQ.SIGN(1)) GO TO 980
    B(L,3) = FLOAT(INDI)/10.
    INDI = FLD(26,10,A(J))
    IF(INDI.NE.SIGN(2)) GO TO 820
    B(L,2) = -1.0
    GO TO 840
820 CONTINUE
    B(L,2) = FLOAT(INDI)/10.0
840 CONTINUE
    INDI = FLD(1,17,A(J+1))
    IF(INDI.EQ.SIGN(3)) GO TO 980
    B(L,1) = INDI*10
    INDI = FLD(19,17,A(J+1))
    IF(INDI.NE.SIGN(3)) GO TO 860
    B(L,4) = -1.0
    GO TO 900
860 CONTINUE
    B(L,4) = INDI
900 CONTINUE
    INDI = FLD(12,12,A(J+2))
    IF(INDI.EQ.SIGN(1)) GO TO 960
    B(L,7) = INDI
    INDI = FLD(24,12,A(J+2))

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XTR11500
XTR11600
XTR11700
XTR11800
XTR11900
XTR12000
XTR12100
XTR12200
XTR12300
XTR12400
XTR12500
XTR12600
XTR12700
XTR12800
XTR12900
XTR13000
XTR13100
XTR13200

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```

IF(INDI.EQ.SIGN(1)) GO TO 960
B(L,8) = FLOAT(INDI)/10.
920 CONTINUE
L = L + 1
940 CONTINUE
IF(L.GT.LEVEL) GO TO 700
J = J + 3
GO TO 800
960 CONTINUE
B(L,7) = -1.0
B(L,8) = -1.0
GO TO 920
980 CONTINUE
LEVEL = LEVEL - 1
GO TO 920
1000 CONTINUE
STOP
END

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131*
132*

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SAT00100  
SAT00200  
SAT00300  
SAT00400  
SAT00500  
SAT00600  
SAT00700

FUNCTION SATVP(T)

C

SATVP = 10.0\*(23.83224-2949.076/T-5.02808\*ALOG10(T)  
1 -1.3816E-7\*10.\*\*((11.344-.0303998\*T)+8.1328E-3\*10.\*\*((3.49149-  
2 1302.8844/T))  
RETURN  
END

1\*  
2\*  
3\*  
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6\*  
7\*



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26* 26*
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31* 31*
32* 32*
33* 33*
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37* 37*
38* 38*

COMPILER(UIAG=3)
SUBROUTINE SFCDTA(STN,RUN,FLAG)
C THE PURPOSE OF THIS ROUTINE IS TO EXTRACT SURFACE OBSERVATION DATA
C FROM THE DATA BASE .
    INCLUDE SFCDATA,LIST
    INCLUDE ABLUFER,LIST
    INCLUDE SBLUFER,LIST
    DIMENSION WW(4)
    EQUIVALENCE (WW,WW1),(TS,TSS)
    INTEGER WW
    INTEGER JUNK/-1/,RUN,FLAG,STN
    II = STN
C FIND THE ADDRESS FOR THE DATA CORRESPONDING TO THE GIVEN STATION AND
C TIME . IF THIS ADDRESS HAS NOT BEEN SET (IT IS ZERO) , RETURN TO
C THE CALLING PROGRAM . OTHERWISE , FIND J , WHERE THE FIRST WORD OF
C THE 11-WORD LOGICAL RECORD IS THE J-TH ELEMENT IN ARRAY A .
    FLAG = 0
    IF (SADRES(II,RUN).EQ.0) RETURN
    I = SADRES(II,RUN)/10000
    J = SADRES(II,RUN) - I*10000
    FLAG = FLD(0,18,A(J))
C RETURN TO THE CALLING PROGRAM IF THE VALUE OF FLAG IS ZERO .
    IF (FLAG.EQ.0) RETURN
C EXTRACT THE DATA IN THE (SURFACE) MANDATORY WORD 1 .
    CALL TESTFD(0,12,A(J+2),INDI)
    WD = INDI
    CALL TESTFD(12,12,A(J+2),INDI)
    IF (INDI.EQ.JUNK) INDI = -10
    WS = FLOAT(INDI)/10.
    CALL TESTFD(24,12,A(J+2),INDI)
    IF (INDI.EQ.0) INDI = -10
    WG = FLOAT(INDI)/10.
C EXTRACT THE DATA IN THE (SURFACE) MANDATORY WORD 2 .
    CALL TESTFD(0,18,A(J+3),INDI)
    IF (INDI.EQ.JUNK) INDI = -10
    SLP = FLOAT(INDI)/10.
    CALL TESTFD(18,18,A(J+3),BT)
    IF (BT.EQ.0) BT = JUNK

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39* C      EXTRACT THE DATA IN THE (SURFACE) MANDATORY WORD 3 .
40*   CALL TESTFD(0,18,A(J+4),INDI)
41*   IF (INDI.EQ.JUNK) INDI = -10
42*   IS = FLOAT(INDI)/10.
43*   CALL TESTFD(18,18,A(J+4),INDI)
44*   IF (INDI.EQ. JUNK) INDI = -10
45*   IS = FLOAT(INDI)/10.
46* C      EXTRACT THE DATA IN THE (SURFACE) MANDATORY WORD 4 .
47*   CALL TESTFD(0,18,A(J+5),INDI)
48*   IF (INDI.EQ.JUNK) INDI = -100
49*   AS = FLOAT(INDI)/100.
50*   CALL TESTFD(18,18,A(J+5),INDI)
51*   PA = INDI
52* C      EXTRACT THE DATA IN THE (SURFACE) MANDATORY WORD 5 .
53*   CALL TESTFD(0,6,A(J+6),TSC)
54*   CALL TESTFD(6,6,A(J+6),PW)
55*   CALL TESTFD(18,18,A(J+6),VV)
56* C      EXTRACT THE DATA IN THE (SURFACE) MANDATORY WORD 6 . TEST THAT THERE
57*   ARE CODED DATA ON THE PRESENT WEATHER .
58*   IF (A(J+7).NE.0) GO TO 15
59*   DO 20 I = 1,4
60*   20 WW(I) = JUNK
61*       GO TO 16
62*   15 DO 25 I = 1,4
63*       CALL TESTFD((I-1)*9,9,A(J+7),WW(I))
64*   25 CONTINUE
65* C      EXTRACT THE DATA IN THE (SURFACE) MANDATORY WORD 8 .
66*   16 CALL TESTFD(6,6,A(J+9),NH)
67*       CALL TESTFD(12,6,A(J+9),CL)
68*       CALL TESTFD(18,6,A(J+9),H)
69*       CALL TESTFD(24,6,A(J+9),CM)
70*       CALL TESTFD(30,6,A(J+9),CH)
71* C      EXTRACT THE DATA IN THE (SURFACE) MANDATORY WORD 9 .
72*       CALL TESTFD(6,6,A(J+10),NS)
73*       CALL TESTFD(12,6,A(J+10),K)
74*       CALL TESTFD(18,6,A(J+10),CT)
75*       CALL TESTFD(24,12,A(J+10),HSHS)
76*       RETURN
SFC03900
SFC04000
SFC04100
SFC04200
SFC04300
SFC04400
SFC04500
SFC04600
SFC04700
SFC04800
SFC04900
SFC05000
SFC05100
SFC05200
SFC05300
SFC05400
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SFC06100
SFC06200
SFC06300
SFC06400
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SFC07700

END

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B-67

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COMPILER(ULAGE=3)
SUBROUTINE TESTFO(LFTBIT,LGTBIT,WORD,IVALUE)
LFTBIT IS THE POSITION OF THE LEFT END OF THE FIELD BEING EXTRACTED ,
COUNTED FROM 0 (MOST SIGNIFICANT BIT) TO 35 (LEAST SIGNIFICANT
BIT) .
LGTBIT IS THE LENGTH IN BITS OF THE FIELD BEING EXTRACTED .
WORD IS THE WORD FROM WHICH THE FIELD IS BEING EXTRACTED .
IVALUE IS THE INTEGER VALUE OF THE FIELD BEING EXTRACTED . IT MAY
NEED TO BE CONVERTED TO REAL AND/OR SCALED BY A CONSTANT FACTOR .
IVALUE = FLD(IABS(LFTBIT),LGTBIT,WORD)
TEST WHETHER THE FIELD EXTRACTED LACKS MEANINGFUL DATA . IF IT DOES ,
RETURN TO CALLING PROGRAM .

NONSNS = 2*LGTBIT - 1
IF (IVALUE.NE.NONSNS) GO TO 11
IVALUE = -1
RETURN

TEST WHETHER THE FIELD EXTRACTED IS A NEGATIVE NUMBER . IF IT IS ,
CONVERT IT BY SUBTRACTING OUT A PROPER CONSTANT .
11 IBIT = FLD(IABS(LFTBIT),1,WORD)
IF (IBIT.EQ.1) IVALUE = IVALUE - NONSNS
RETURN
END

```



GWC00100  
 GWC00200  
 GWC00300  
 GWC00400  
 GWC00500  
 GWC00600  
 GWC00700  
 GWC00800  
 GWC00900  
 GWC01000  
 GWC01100  
 GWC01200  
 GWC01300  
 GWC01400  
 GWC01500  
 GWC01600  
 GWC01700  
 GWC01800  
 GWC01900  
 GWC02000  
 GWC02100  
 GWC02200  
 GWC02300  
 GWC02400  
 GWC02500  
 GWC02600  
 GWC02700  
 GWC02800  
 GWC02900  
 GWC03000  
 GWC03100  
 GWC03200  
 GWC03300  
 GWC03400  
 GWC03500  
 GWC03600  
 GWC03700  
 GWC03800

```

1*  COMPILER (DIAG=3)
2*  SUBROUTINE GWCDTA(GRID,RUN,FLAG)
3*  INCLUDE ABUFEX,LIST
4*  INCLUDE FILES
5*  INCLUDE GBUFEK
6*  INCLUDE GWDATA
7*  INTEGER FLAG,GRID,RUN,ZS(4)
8*  INTEGER A,B(4,6),X,Y
9*  INTEGER ADRES,BLOCK
10*  INTEGER OCT/0777777000000/
11*  DATA P /100000.,85000.,70000.,50000./
12*  DATA ZS/110,1460,3010,5570/
13*  IF (RUN.EQ.BLOCK) GO TO 50
14*  BLOCK = RUN
15*  CALL BLKIN(5700,A(1),BLOCK,GWCFIL,I)
16*  50 CONTINUE
17*  ADRES = GTIME - ANLTIM(RUN)
18*  IF (ADRES.LT.0) GO TO 600
19*  IF (ADRES.GT.24) ADRES = ADRES - 76
20*  IF (ADRES.GT.16) GO TO 800
21*  ADRES = 300*ADRES + 25*(GRID-1)
22*  DO 150 J = 1,6
23*  DO 100 K = 1,2
24*  L = K*K
25*  M = 2*(J-1) + ADRES
26*  X = FLD(16,18,A(M+K))
27*  Y = FLD(0,18,A(M+K))
28*  IF (X.GT.32768) X = OR(X,OCT)
29*  IF (Y.GT.32768) Y = OR(Y,OCT)
30*  B(L-1,J) = X
31*  B(L,J) = Y
32*  100 CONTINUE
33*  150 CONTINUE
34*  DO 200 L = 1,4
35*  U(L) = B(L,1)
36*  V(L) = B(L,2)
37*  Z(L) = B(L,4) + ZS(L)
38*  T(L) = B(L,5)
  
```

AD-A038 399

CRAMER (H E) CO INC SALT LAKE CITY UTAH  
MIXING-LAYER ANALYSIS ROUTINE AND TRANSPORT/DIFFUSION APPLICATI--ETC(U)  
MAR 77 R K DUMBAULD, J R BJORKKLUND

F/G 4/2

DAAD07-76-C-0023

UNCLASSIFIED

TR-76-106-01

ECOM-77-2

NL

3 OF 3  
AD  
A038 399



END

DATE  
FILMED

5-77

GWC03900  
GWC04000  
GWC04100  
GWC04200  
GWC04300  
GWC04400  
GWC04500  
GWC04600  
GWC04700  
GWC04800  
GWC04900  
GWC05000  
GWC05100  
GWC05200  
GWC05300

```

Q(L) = B(L,6)
Q(L) = T(L)-Q(L)
IF (Q(L) .LT. 0.0) Q(L) = 0.0
IF (Q(L) .GT. 0.0.AND.P(L) .GT. 0.0) Q(L)=62.2*SATVP(Q(L))/P(L)
Q(L) = Q(L)/(1. - 0.61*Q(L))
200 CONTINUE
FLAG = 1
IF (RUN.EQ.41) FLAG = 0
RETURN
800 CONTINUE
WRITE(6,900)
FLAG = 0
RETURN
900 FORMAT( 'IMPRUPER GWC TIME OR BLOCK')
END

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35*

SUBROUTINE DAYNIT(LON,LAT,SNRISE,SUNSET,ALPHA)
THIS SUBROUTINE CALCULATES THE TIME OF 1 HOUR BEFORE SUNSET AND
1 HOUR AFTER SUNRISE AND THE SOLAR ALTITUDE ALPHA
REAL LON,LAT
INCLUDE TIMES,LIST
TIME = FLOAT(HOUR)+FLOAT(MINUTE)*1.66666666E-2
LON IS POS. WEST OF GREENWICH UK.
CPHI = LAT*.01745329
SPHI = SIN(CPHI)
CPHI = COS(CPHI)
D1= (JULIAN+DAY-1.0)*360.0/365.242
D2 = D1*.01745329
D3 = 2*D2
CU1 = COS(D2)
SD1 = SIN(D2)
S2D1 = SIN(D3)
C2D1 = COS(D3)
GAM = 279.9348+D1+1.914827*SD1-7.9525E-2*CD1+1.9938E-2*S2D1-
11.62E-3*C2D1
SD = .39785*SIN(GAM*.01745329)
CU= Sqrt(1.0-SD*SD)
TM = 12.0+.1257*SD1-4.289E-3*CD1+.153809*S2D1+.6.0783E-2*C2D1
TH = ACOS((-1.5707E-2-SPHI*SD)/(CPHI*CD))*57.2957795
SNRISE = (LON-TH)*6.6666666E-2+TM+1.0
SUNSET = (LON+TH)*6.6666666E-2+TM-1.0
ALPHA = SPHI*SD+CPHI*CD*COS(.01745329*(15.0*(TIME-TM)-LON))
IF (ALPHA .GT. 1.0) ALPHA = 1.0
IF (ALPHA .LT.-1.0) ALPHA =-1.0
ALPHA = ASIN(ALPHA)*57.2957795
IF (SNRISE .LT. 0.0) SNRISE = SNRISE+24.0
IF (SNRISE .GE. 24.0) SNRISE = SNRISE-24.0
IF (SUNSET .LT. 0.0) SUNSET = SUNSET+24.0
IF (SUNSET .GE. 24.0) SUNSET = SUNSET-24.0
RETURN
END

DAY00100
DAY00200
DAY00300
DAY00400
DAY00500
DAY00600
DAY00700
DAY00800
DAY00900
DAY01000
DAY01100
DAY01200
DAY01300
DAY01400
DAY01500
DAY01600
DAY01700
DAY01800
DAY01900
DAY02000
DAY02100
DAY02200
DAY02300
DAY02400
DAY02500
DAY02600
DAY02700
DAY02800
DAY02900
DAY03000
DAY03100
DAY03200
DAY03300
DAY03400
DAY03500

```



```

1* SUBROUTINE LONLAT(X,Y,LON,LAT)
2* THIS ROUTINE CALCULATES THE LONGITUDE AND LATITUDE OF THE COORD
3* POSITION X,Y RELATIVE TO UTM ZONE - ZONENO = 13 **
4* REAL LON,LAT
5* DOUBLE PRECISION ESQ,PI,MTOF,MTOFI,SECRD,FE,CONS1,CONS2,
6* 1CONS3,CONS4,A,SCALE,PPRD,SEPO,SINLT,CSLT,CSSQ,EP SQ,SNONS,
7* 2PHRD,PHIS,Q,SNLAT,CSLAT,SN SQ,CCSQ,TNLAT,TNSQ,ENSQ,ENSNS,QSQ,QFR,
8* 3GSX,EPCSQ,SVN,EHT,D6,DLAM,EPCS,QCU,QFV,SCLAT,ENSNS,ANINE,
9* 4TEN,E3
10* DATA ESQ/.006768658D0/,PI/3.1415926535898D0/,A/6378206.4D0/,
11* 1ZONENO/13./,SCALE/.9996D0/,ISW/0/,CONS1/.24682D0/,CONS2/30.02335D0/,
12* 2/,CONS3/5078.64977D0/,CONS4/.157049981D0/,SEPO/.0408887094D0/,
13* CM = (6.0*ZONENO-183.0)*3600.
14* MTOF = 39.37/12.0
15* MTOFI = 12.0/39.37
16* SECRD = 648000.0/PI
17* FE = 500000.0*MTOF
18* EPSQ = ESQ/(1.0-ESQ)
19* SNONS = 1.0/SECRD
20* LAT = X*MTOF
21* LON = Y*MTOF
22* PPRD = (Y*CONS4*1.0E-6)/SCALE
23* SINLT = DSIN(PPRD)
24* CSLT = DCOS(PPRD)
25* CSSQ = CSLT*CSLT
26* PHRD = ((CONS1*CSSQ+CONS2)*CSSQ+CONS3)*(SINLT*CSLT)*1.0E-6+PPRD
27* PHIS = PHRD*SECRD
28* Q = ((LAT-FE)*MTOFI)*1.0E-6
29* IF (Q) 300,200,300
30* 200 DLAM = 0.0
31* LAT = PHIS/3600.0
32* GO TO 400
33* 300 SNLAT = DSIN(PHRD)
34* CSLAT = DCOS(PHRD)
35* SN SQ = SNLAT*SNLAT
36* CCSQ = CSLAT*CSLAT
37* TNLAT = SNLAT/CSLAT
38* TNSQ = TNLAT*TNLAT

```

```

39*      ENU = A/DSQRT(1.0-ESQ*SNSQ)
40*      ENSNS = ENU*SVNS
41*      EPS = EPSQ*CCSQ
42*      EPCSQ = 1.0+EPCS
43*      QSQ = Q*Q
44*      QCU = QSQ*Q
45*      QFR = QCU*Q
46*      GFV = QFR*Q
47*      QSX = GFV*Q
48*      SCLAT = 1.0/CSLAT
49*      ENSNS = ENU**4*ENSNS
50*      SVN = (((TNLAT/(2.0*ENU*ENSNS))*EPCSQ)/SCALE**2)*10.0D11
51*      EGT = ((TNLAT/(24.0*ENU**3*ENSNS))*(5.+3.*TNSQ+SEPG*(CCSQ-SNSQ)
52*      1-(3.0*EPSQ**2*CCSQ)*(CCSQ+3.*SNSQ))/SCALE**4)*10.0D3
53*      D6 = (QSX*(TNLAT/(720.*ENU**5*ENSNS))*(61.+(45.*TNSQ)*(2.+TNSQ-
54*      1EPSQ*SNSQ)+EPSQ*(107.*CCSQ-162.*SNSQ))/SCALE**6)*10.0D35
55*      ANINE = (SCLAT/ENSNS)/SCALE * 1.0E6
56*      TEN = (SCLAT/(6.*ENU**2*ENSNS))*(1.+2.*TNSQ+EPSQ)/SCALE**3*1.0D18
57*      E5 = GFV*(SCLAT/(120.*ENSNS))*(5.+(4.*TNSQ)*(7.+6.*TNSQ)
58*      1+(2.*EPSQ)*(3.*CCSQ+4.*SNSQ))/SCALE**5*1.0D30
59*      LAT = (PHIS-SVN*QSQ+EGT*QFR-Q6)/3600.0
60*      DLAM = ANINE*Q-TEN*QCU+E5
61*      400 CONTINUE
62*      LON = -(CM+DLAM)/3600.0
63*      RETURN
64*      END

```

```

LON03900
LON04000
LON04100
LON04200
LON04300
LON04400
LON04500
LON04600
LON04700
LON04800
LON04900
LON05000
LON05100
LON05200
LON05300
LON05400
LON05500
LON05600
LON05700
LON05800
LON05900
LON06000
LON06100
LON06200
LON06300
LON06400

```

```

1* SUBROUTINE SOLVMX
2* 2-LAYER MESOSCALE MODEL SOLUTION
3* INCLUDE MESSAGE,LIST
4* INCLUDE FILES,LIST
5* INCLUDE MXBUF,LIST
6* INCLUDE NEWPRM,LIST
7* INCLUDE WNDFLD,LIST
8* INCLUDE WNDCOM,LIST
9* INCLUDE WNDOTA,LIST
10* INCLUDE WNDOTb,LIST
11* INCLUDE TIMES,LIST
12* CALL INITIALIZATION ROUTINE
13* 10 CONTINUE
14* CALL MXSTRT
15* IF (TYPE3 .LT. 0) GO TO 30
16* IS SOLUTION SAME AS LAST CALCULATED
17* IF (KFLG1 .EQ. 9) GO TO 30
18* CALL SOLUTION
19* CALL MXSOLV
20* IF (IFLG .NE. -1) GO TO 20
21* ICNT = ICNT+1
22* IF (ICNT .LT. 3) GO TO 10
23* WRITE (XOTFIL,9000)
24* 9000 FORMAT ('0 *** CANNOT RECOVER FROM MODEL INSTABILITY. NO SOLUTION
25* 10OUTPUT. PROG RETURNS CONTROL TO EXEC AND SETS TYPE3 = -1./')
26* TYPE3 = -1
27* GO TO 30
28* 20 CONTINUE
29* CALL OUTPUT
30* CALL MXLOUT
31* WRITE (XOTFIL,9001)
32* 9001 FORMAT ('0 *** MESOSCALE WIND FIELD SOLUTION COMPLETED AND OUTPUT
33* 1TO SAVE FILE./')
34* 30 CONTINUE
35* RETURN
36* END

```



```

1* SUBROUTINE MXSTRT
2* SUBROUTINE TO INITIALIZE THE 2-LAYER MESOSCALE MODEL
3* INCLUDE MESSAGE,LIST
4* INCLUDE FILES,LIST
5* INCLUDE MXBUFK,LIST
6* INCLUDE N*PKM,LIST
7* INCLUDE W*DFLD,LIST
8* INCLUDE W*DCOM,LIST
9* INCLUDE TIMES,LIST
10* EQUIVALENCE (G1,G0),(DILMDA,DILMDO),(NCNT,NCNT0),(ABLK,ABLK0),
11* 1(ISMTH,ISMTH0)
12* IDM = IDP-1
13* JDM = JDP-1
14* IFLG = 0
15* IF (PN .GE. HMIN+ABLK0) GO TO 100
16* WRITE (XOTFIL,9000) PN
17* TYPE3 = -1
18* RETURN
19*
20* 100 CONTINUE
21* INPUT THE TERRAIN ELEVATION DATA WHERE THERE ARE IDP*JDP POINTS
22* AND THE FIRST 5 (LAST 5) ROWS AND COLUMNS ARE EQUAL TO HMIN.
23* CALL BLKIN(IDP*JDP,H,1,WSTRN,ISTS)
24* INPUT LAST SOLUTION
25* N*RD5 = 3*IDP*JDP+68
26* CALL BLKIN(N*RD5,NETRAD,2,M*LYRF,ISTS)
27* MOVE LAST SOLUTION DOWN FILE
28* CALL BLKOUT(N*RD5,NETRAD,1,M*LYRF,ISTS)
29* ABLK0 = ABLKN
30* DILMDO = DILMDN
31* G0 = GN
32* ISMTH0 = ISMTHN
33* NCNT0 = NCNTN
34* NETRAD = NETRUN
35* XSOURC = XSOURN
36* YSOURC = YSOURN
37* ZSOURC = ZSOURN
38* DO 250 I=1,25
39* POTMPN(I) = POTMPN(I)

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250 ZELEV(1) = ZELEV(1)  
SURFTA = SURFTN  
A1 = PN-PO  
A2 = UN-UO  
A3 = VN-VO  
A4 = PO-HMIN  
C DETERMINE IF COLD OR HOT START  
IULIAN = JULIAN+DAY  
IMONTH = MONTH  
IDAY = DAY  
IHOUR = HOUR  
MINUTE = MINUTE  
IF (ABS(A1)+ABS(A2)+ABS(A3)-.001) 400,400,270  
270 CONTINUE  
IF (KFLG1 .GT. 0) GO TO 300  
IFLG1 = 2  
C MAKE THE NEW INITIALIZATION PARAMETERS VELOCITY AND LAYER HEIGHT  
C WITHIN 25% OF OLD VALUE AND IS DIFF IN OLD AND NEW DIR <= 10 DEG  
C IF YES UPDATE OLD SOLUTION , ELSE COLD START  
VL1 = UO  
VR1 = VO  
VL2 = UN  
VR2 = VN  
CALL HEC003(VL1,VR1)  
CALL HEC003(VL2,VR2)  
IF (0.75\*VL1 .GT. VL2.OR.1.75\*VL1 .LT. VL2) GO TO 300  
IF (.075\*PO .GT. PN.OR.1.75\*PO .LT. PN) GO TO 300  
VL1 = ABS(VR1-VR2)  
IF (VL1 .GT. 180.0) VL1 = 360.0-VL1  
IF (VL1 .LE. 10.0) GO TO 310  
300 CONTINUE  
A1 = PN  
A2 = UN  
A3 = VN  
A4 = -HMIN  
IFLG1 = 1  
310 CONTINUE  
UO = UN

MXS03900  
MXS04000  
MXS04100  
MXS04200  
MXS04300  
MXS04400  
MXS04500  
MXS04600  
MXS04700  
MXS04800  
MXS04900  
MXS05000  
MXS05100  
MXS05200  
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VU = VN
PO = PN
DO 360 J=1,JDP
DO 360 I=1,IDP
GO TO (320,330),IFLG1
320 M(I,J) = 0.0
    N(I,J) = 0.0
    P(I,J) = 0.0
330 A5 = P(I,J)-H(I,J)
    P(I,J) = A5+A1
    IF (P(I,J) .LT. ABLK) GO TO 350
340 M(I,J) = A5*M(I,J)+A4*A2+UN*A1
    N(I,J) = A5*N(I,J)+A4*A3+VN*A1
    GO TO 360
C      MINIMUM DEPTH CONSTRAINT
350 P(I,J) = ABLK
    M(I,J) = 0.0
    N(I,J) = 0.0
360 CONTINUE
C      ARRAYS INITIALIZED
C      CALC TIME ITERATION LOOP CONSTANTS
STPN = 1.0/((IDP-10)*(JDP-10))
G2 = 0.5*G1
DTL = DTLMDA*.70710678*XMIN
NN = 0
ISM = 0
TIM = 0.0
ICNT = NCNT
DPMAX = 20000.
UVMIN = 1.0E-19*SGRT(UPMAX/AMIN1(DXPI(1),DYPJ(1)))
UVEQU = 1.0E-37/AMIN1(2.0*DELXI(1),2.0*DELYJ(1))
UVMAX = AMAX1(10.0*ABS(UN),10.0*ABS(VN))
IF (UVMAX .LT. 5.0) UVMAX = 5.0
IF (IFLG1 .EQ. 1) WRITE (XOTFIL,9002)
IF (IFLG1 .EQ. 2) WRITE (XOTFIL,9003)
GO TO 410
400 WRITE (XOTFIL,9001)
KFLG1 = 9

```

MXS07700  
MXS07800  
MXS07900  
MXS08000  
MXS08100  
MXS08200  
MXS08300  
MXS08400  
MXS08500  
MXS08600  
MXS08700  
MXS08800  
MXS08900  
MXS09000  
MXS09100  
MXS09200  
MXS09300  
MXS09400  
MXS09500  
MXS09600  
MXS09700  
MXS09800  
MXS09900  
MXS10000  
MXS10100  
MXS10200  
MXS10300  
MXS10400  
MXS10500  
MXS10600  
MXS10700  
MXS10800  
MXS10900  
MXS11000  
MXS11100  
MXS11200  
MXS11300  
MXS11400

115*	CALL BLKOUT(NWRDS,NETRAD,2,MXLRYF,ISTS)	MXS11500
116*	410 CONTINUE	MXS11600
117*	9000 FORMAT ('0 *--* ERROR - LAYER HEIGHT IS LESS THAN MINIMUM + ABLKIN	MXS11700
118*	1CONSTRAINF, PROG CANNOT CONTINUE, PNE',F7.2)	MXS11800
119*	9001 FORMAT ('0 *--* MESOSCALE WINDFIELD SOLUTION SAME AS LAST SOLUTION,	MXS11900
120*	1 PROG DOES NOT RECALC, PROG USES LAST SOLUTION *--*')	MXS12000
121*	9002 FORMAT ('0 *--* COLD START USED FOR MESOSCALE INITIALIZATION')	MXS12100
122*	9003 FORMAT ('0 *--* HOT START USED FOR MESOSCALE INITIALIZATION')	MXS12200
123*	RETURN	MXS12300
124*	END	MXS12400

```

1* SUBROUTINE MXSOLV
2* ROUTINE TO SOLVE 2-LAYER MESOSCALE MODEL
3* INCLUDE FILES,LIST
4* INCLUDE MXEUF,LIST
5* INCLUDE WNDFLU,LIST
6* INCLUDE WNDCOM,LIST
7* INCLUDE NEAPRM,LIST
8* INCLUDE MESSAGE,LIST
9* EQUIVALENCE (GI,GO),(DTLMDA,DTLMDO),(NCNT,NCINTO),(ABLK,ABLK0),
10* 1(ISMOTH,ISMTHO)
11* FILTER(A,B,C,D,E,F,G,H,O) = A+0.125*(U+C+D+E-4.0*A)+0.0625*(F+G+H+
12* 10-4.0*A)
13* BEGIN TIME ITERATION LOOP
14* CALL MYPRG(1,1,J,IFLG,KFLG2)
15* SET TIME TO START TO CHECK FOR CONVERGENCE
16* TIMMIN = 1200.0
17* IF (IFLG1.NE. 2) GO TO 170
18* TIMMIN = 600
19* TIMMAX = 1800
20*
21* 170 CONTINUE
22* JUPM5 = JUP-5
23* IUPM5 = IUP-5
24* NN = NN+1
25*
26* C FILTER COUNTER
27* IF (ISM.GE. ISMOTH) ISM = 0
28* ISM = ISM+1
29* DT RECALCULATION COUNTER
30* IF (ICNT.GE. NCNT) ICNT = 0
31* ICNT = ICNT+1
32* IF (ICNT.GT. 1) GO TO 300
33* C CALC TIME STEP INCREMENT DT
34* XMAX = -1.0E5
35* DO 220 J=1,JDP
36* DO 220 I=1,IDP
37* IF (P(I,J).LE. 0.0) GO TO 220
38* CHK = SQRT(M(1,J)*M(I,J)+N(I,J)*N(I,J))/P(I,J)+SQRT(ABS(GI*P(I,J)
39* 1)
40* XMAX = AMAX1(CHK,XMAX)
41*
42* MXV00100
43* MXV00200
44* MXV00300
45* MXV00400
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220 CONTINUE  
 DT = ABS(DTL/XMAX)  
 IF (DT.LT. 1.0) DT = 1.0  
 A0 = 0.5\*DT  
 300 TIM = TIM+DT  
 CALL MYPRG(2,1,J,IFLG,KFLG2)  
 D1 = 0.0  
 D2 = 0.0  
 D3 = 0.0  
 D4 = 0.0  
 JUPM5 = JUP-5  
 IUPM5 = IUP-5  
 DO 600 J=1,JOM  
 DELYJJ = DELYJ(6)  
 DLYJJ = DYPJ(6)  
 IF (J.GT. 6) GO TO 350  
 IF (J.EQ. 1) GO TO 340  
 DELYJJ = DELYJ(J-1)  
 340 DLYJJ = DYPJ(J)  
 GO TO 360  
 350 IF (J.LT. JUPM5) GO TO 360  
 DELYJJ = DELYJ(JUP-J)  
 DLYJJ = DYPJ(JUP-J)  
 360 A1 = 2.0\*DELYJJ  
 A2 = 0.5\*DELYJJ  
 DO 600 I=1,IDM  
 DELXII = DELXI(6)  
 DXII = DXPI(6)  
 IF (I.GT. 6) GO TO 380  
 IF (I.EQ. 1) GO TO 370  
 DELXII = DELXI(I-1)  
 370 DXII = DXPI(I)  
 GO TO 390  
 380 IF (I.LT. IUPM5) GO TO 390  
 DELXII = DELXI(IUP-I)  
 DXII = DXPI(IUP-I)  
 390 CONTINUE  
 PIJ = 1.0/P(I,J)

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77*      PIPJP = 1.0/P(I+1,J+1)
78*      PIPJ = 1.0/P(I,J+1)
79*      PIPJ = 1.0/P(I+1,J)
80*      A3 = M(I+1,J+1)*N(I+1,J+1)/P(I+1,J+1)
81*      A3 = (PIPJ*M(I+1,J+1))*N(I+1,J+1)
82*      A4 = P(I,J)*P(I,J)
83*      A5 = N(I,J)/P(I,J)
84*      A5 = N(I,J)*PIJ
85*      A6 = P(I+1,J+1)*P(I+1,J+1)
86*      A7 = M(I,J+1)*N(I,J+1)/P(I,J+1)
87*      A7 = (PIJP*M(I,J+1))*N(I,J+1)
88*      A8 = M(I,J)/P(I,J)
89*      A8 = M(I,J)*PIJ
90*      A9 = M(I,J)*N(I,J)/P(I,J)
91*      A9 = A8*N(I,J)
92*      A10 = M(I+1,J)**2/P(I+1,J)
93*      A10 = (PIPJ*M(I+1,J))*M(I+1,J)
94*      A11 = P(I+1,J)*P(I+1,J)
95*      A12 = M(I+1,J)*N(I+1,J)/P(I+1,J)
96*      A12 = (PIPJ*M(I+1,J))*N(I+1,J)
97*      A13 = P(I,J+1)*P(I,J+1)
98*      A14 = N(I,J+1)**2/P(I,J+1)
99*      A14 = (PIJP*N(I,J+1))*N(I,J+1)
100*      A15 = M(I,J)*N(I,J)/P(I,J)**2
101*      A15 = A9*PIJ
102*      IF (J.EQ.1) GO TO 400
103*      A16 = G2*(P(I+1,J)+P(I,J))
104*      PIJ = 1.0/P(I,J-1)
105*      PIPJM = 1.0/P(I+1,J-1)
106*      A17 = M(I,J+1)*N(I,J+1)/P(I,J+1)*N(I,J-1)/P(I,J-1)
107*      A17 = A7-(PIJM*M(I,J-1))*N(I,J-1)
108*      A18 = M(I+1,J)/P(I+1,J)
109*      A18 = M(I+1,J)*PIPJ
110*      A19 = N(I,J+1)**2/P(I,J+1)-N(I,J-1)**2/P(I,J-1)
111*      A19 = A14-(PIJM*N(I,J-1))*N(I,J-1)
112*      A20 = P(I,J+1)**2-P(I,J-1)**2
113*      A20 = A13-P(I,J-1)*P(I,J-1)
114*      A21 = H(I,J+1)-H(I,J-1)

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A22 = N(I,J+1)-N(I,J-1)  
A23 = ((M(I+1,J)-M(I,J))\*DLXII+A2\*(N(I+1,J+1)-N(I+1,J-1))+A22)  
A24 = M(I+1,J)/P(I+1,J)+M(I,J)/P(I,J)  
A24 = A18 + A8  
FM = FP  
FP = A2\*(A3-(PIPJ\*M(I+1,J-1))\*N(I+1,J-1)+A17)+DLXII\*((A10-M(I,J)  
1)\*A8+G2\*(A11-A4))+A16\*(H(I+1,J)-H(I,J)))  
C2M = C2P  
C2P = 0.5\*((N(I+1,J)\*PIPJ+A5)\*FP+A24\*(DLXII\*(A12-A9)+A2\*((PIPJ\*  
1N(I+1,J+1))\*N(I+1,J+1)-(PIPJ\*M(I+1,J-1))\*N(I+1,J-1))+A19+G2\*(A6-P  
2I+1,J-1))\*P(I+1,J-1)+A20))+A16\*A2\*(H(I+1,J+1)-H(I+1,J-1))+A21))-(A12M  
3\*PIPJ+A15)\*A23)  
B2M = B2P  
B2P = FP\*A24+A23\*(A16-0.5\*(A18\*A18+A8\*A8))  
400 IF (I.EQ. 1) GO TO 600

C

A25 = 0.5\*DELXII  
PIMJ = 1.0/P(I-1,J)  
PIMJ = 1.0/P(I-1,J+1)  
A26 = M(I+1,J)\*N(I+1,J)/P(I+1,J)-M(I-1,J)\*N(I-1,J)/P(I-1,J)  
A26 = A12-(PIMJ\*M(I-1,J))\*N(I-1,J)  
A27 = G2\*(P(I,J+1)+P(I,J))  
A28 = N(I,J+1)\*PIJP  
A29 = M(I+1,J)\*\*2/P(I+1,J)-M(I-1,J)\*\*2/P(I-1,J)  
A29 = A10-(PIMJ\*M(I-1,J))\*M(I-1,J)  
A30 = P(I+1,J)\*\*2-P(I-1,J)\*\*2  
A30 = A11-P(I-1,J)\*P(I-1,J)  
A31 = H(I+1,J)-H(I-1,J)  
A32 = M(I+1,J)-M(I-1,J)  
A33 = ((N(I,J+1)-N(I,J))\*DLYJJ+A25\*(M(I+1,J+1)-M(I-1,J+1))+A32))  
A34 = N(I,J+1)/P(I,J+1)+N(I,J)/P(I,J)  
A34 = A28+A5  
GM = GP(I-1)  
GP(I-1) = A25\*(A3-(PIMJ\*M(I-1,J+1))\*N(I-1,J+1)+A26)+DLYJJ\*((A14  
1-N(I,J)\*A5+G2\*(A13-A4))+A27\*(H(I,J+1)-H(I,J)))  
B3M = B3P(I-1)  
B3P(I-1) = 0.5\*((M(I,J+1)\*PIJP+A8)\*GP(I-1)+A34\*(DLYJJ\*(A7-A9) +A2M  
15\*(PIPJ\*M(I+1,J+1))\*M(I+1,J+1)-(PIMJ\*M(I-1,J+1))\*M(I-1,J+1))+A29M  
2+G2\*(A6-P(I-1,J+1)\*P(I-1,J+1)+A30))+A27\*A25\*(H(I+1,J+1)-H(I-1,J+1))M  
XV11500  
XV11600  
XV11700  
XV11800  
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3+A31))-(A7\*P1JP+A15)\*A33)  
C3M = C3P(I-1)  
C3P(I-1) = GP(I-1)\*A34+A33\*(A27-0.5\*(A28\*A28+A5\*A5))  
500 IF (I.EQ. 1.OR.J.EQ. 1) GO TO 600  
A35 = 2.0\*DELXII  
A36 = G2\*P(I,J)  
A37 = DELXII\*A32+DELYJJ\*A22  
B1 = (DELXII\*(A29+G2\*A30)+DELYJJ\*A17+A36\*A35\*A31)  
C1 = (DELYJJ\*(A19+G2\*A20)+DELXII\*A26+A36\*A1\*A21)  
CHANGE IN M  
A34 = B2P-B2M  
IF (ABS(A34) .LT. UVEGU) A34 = 0.0  
A33 = B3P(I-1)-B3M  
IF (ABS(A33) .LT. UVEGU) A33 = 0.0  
E1 = UT\*(-B1+A0\*(A35\*A34+A1\*A33+G1\*DELXII\*A31\*A37))  
CHANGE IN N  
A34 = C2P-C2M  
IF (ABS(A34) .LT. UVEGU) A34 = 0.0  
A33 = C3P(I-1)-C3M  
IF (ABS(A33) .LT. UVEGU) A33 = 0.0  
E2 = UT\*(-C1+A0\*(A35\*A34+A1\*A33+G1\*DELYJJ\*A21\*A37))  
CHANGE IN P  
A34 = FP-FM  
IF (ABS(A34) .LT. UVEGU) A34 = 0.0  
A33 = GP(I-1)-GM  
IF (ABS(A33) .LT. UVEGU) A33 = 0.0  
E3 = UT\*(-A37+A0\*(A35\*A34+A1\*A33))  
M(I-1,J-1) = M(I,J)+E1  
N(I-1,J-1) = N(I,J)+E2  
P(I-1,J-1) = P(I,J)+E3  
IF (ABS(M(I-1,J-1)) .LT. UVMIN) M(I-1,J-1) = 0.0  
IF (ABS(N(I-1,J-1)) .LT. UVMIN) N(I-1,J-1) = 0.0  
CALL MYPRG(3,I,J,IFLG,KFLG2)  
IF (ISMOTH.GT.0.AND.ISM.NE.0) GO TO 600  
IF (I.LT. 6.OR.I.GT. IDPM5) GO TO 600  
IF (J.LT. 6.OR.J.GT. JDPMS) GO TO 600  
D1 = U1+P(I-1,J-1)  
D2 = U2+P(I-1,J-1)\*P(I-1,J-1)

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MXV17900  
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MXV18700  
MXV18800  
MXV18900  
MXV19000



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03 = D3+E3
D4 = D4+E3+E3
600 CONTINUE
CALL MYPRG(4,I,J,IFLG,KFLG2)
DO 720 J=2,JDM
L = JJP-J
IF (ISM.NE. ISMOTH) GO TO 700
L1 = L-1
L2 = L+1
IF (L1.LT. 1) L1 = 1
IF (L2.GT. JDM-1) L2 = JDM-1
700 DO 720 I=2,IDM
K = IDP-I
IF (ISM.EQ. ISMOTH) GO TO 710
M(K+1,L+1) = M(K,L)
N(K+1,L+1) = N(K,L)
P(K+1,L+1) = P(K,L)
GO TO 720
710 K1 = K-1
K2 = K+1
IF (K1.LT. 1) K1 = 1
IF (K2.GT. IDM-1) K2 = IDM-1
M(K+1,L+1) = FILTER(M(K,L),M(K2,L),M(K,L),M(K,L2),M(K,L1),M(K,L1),M(K,L1),M(K,L1),M(K,L1),M(K,L1))
N(K+1,L+1) = FILTER(N(K,L),N(K2,L),N(K,L),N(K,L2),N(K,L1),N(K,L1),N(K,L1),N(K,L1),N(K,L1),N(K,L1))
P(K+1,L+1) = FILTER(P(K,L),P(K2,L),P(K,L),P(K,L2),P(K,L1),P(K,L1),P(K,L1),P(K,L1),P(K,L1),P(K,L1))
GO TO 720
720 CONTINUE
C
FIX BOUNDARY
DO 730 J=2,JDM
M(1,J) = M(2,J)
N(1,J) = N(2,J)
P(1,J) = P(2,J)
M(IDP,J) = M(IDM,J)
N(IDP,J) = N(IDM,J)
P(IDP,J) = P(IDM,J)
730 DO 740 I=1,IDP

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MXV22900  
 MXV23000  
 MXV23100  
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M(I,1) = M(I,2)
N(I,1) = N(I,2)
P(I,1) = P(I,2)
M(I,JDP) = M(I,JDM)
N(I,JDP) = N(I,JDM)
P(I,JDP) = P(I,JDM)
740 CHECK FOR MINIMUM, MAXIMUM DEPTH AND VELOCITY VIOLATIONS
DO 1400 J=1,JDP
DO 1400 I=1,IUP
IF (P(I,J) .GE. ABLK) GO TO 1350
M(I,J) = 0.0
N(I,J) = 0.0
P(I,J) = ABLK
1350 CONTINUE
IF (ABS(M(I,J)) .LE. UVMAX*P(I,J)) GO TO 1360
E3 = UVMAX*P(I,J)
IF (M(I,J) .LT. 0.0) E3 = -E3
M(I,J) = E3
1360 IF (ABS(N(I,J)) .LE. UVMAX*P(I,J)) GO TO 1370
E3 = UVMAX*P(I,J)
IF (N(I,J) .LT. 0.0) E3 = -E3
N(I,J) = E3
1370 CONTINUE
IF (P(I,J) .GT. DPMAX) P(I,J) = DPMAX
1400 CONTINUE
C CHECK FOR CONVERGENCE OF SOLUTION
IF (ISMOTH .EQ. 0) GO TO 1600
IF (ISM .NE. ISMOTH) GO TO 1620
1600 CONTINUE
D4 = (D4-D3*D3*STPN)/(D2-D1*D1*STPN)
CHK = 0.0
IF (TIM .LT. TIMMIN) GO TO 1610
SIX = SIX+TIM
SIY = SIY+D4
SIXY = SIXY+D4*TIM
SIXX = SIXX+TIM*TIM
KK = KK+1
IF (KK .EQ. 1) GO TO 1610

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CHK = (SIX\*SIY-KK\*SIX)/(SIX\*SIX-KK\*SIX)  
IF (CHK .GT. 0.0) GO TO 1610  
IF (U4LAST-D4 .GT. 1.0E-5) GO TO 1610  
IF (U4LAST-D4 .LT. 0.0) GO TO 1610  
C SOLUTION CONVERGENCE REACHED  
IFLG = 1  
1610 CONTINUE  
U4LAST = D4  
1620 CONTINUE  
CALL MYPRG(5,1,J,IFLG,KFLG2)  
IF (IFLG .EQ. 1) GO TO 1630  
IF (TIM .LT. TIMMAX) GO TO 200  
IF (ISMOTH .EQ. 0) GO TO 1630  
IF (ISM .NE. ISMOTH) GO TO 200  
1630 CONTINUE  
CALL MYPRG(6,1,J,IFLG,KFLG2)  
RETURN  
END

MXV26700  
MXV26800  
MXV26900  
MXV27000  
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MXV27200  
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SUBROUTINE MXLOUT
  INCLUDE FILES,LIST
  INCLUDE MXBUF,LIST
  INCLUDE WNDCOM,LIST
  INCLUDE WNDFLD,LIST
  DO 100 J=1,JDP
  DO 100 I=1,IDP
    DTL = 1.0/P(I,J)
    M(I,J) = M(I,J)*DTL
    N(I,J) = N(I,J)*DTL
    100 P(I,J) = P(I,J)+H(I,J)
    NOUT = 3*IDP*JDP+68
    CALL BLKOUT(NOUT,RETRAD,2,MXLYRF,ISTS)
  RETURN
END

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SUBROUTINE MYPRG(ILFQ,I,J,JFLG,KFLG2)
INCLUDE MXBUFR,LIST
INCLUDE WNDFLO,LIST
INCLUDE WNDCOM,LIST
INCLUDE FILES,LIST
EQUIVALENCE (ISMTHO,ISMOTH)
DATA RAD/.01745/
EQUIVALENCE (ABLK,ABLK0),(DTLMDA,DTLMDO),(NCNT,NC,TO),(G1,G0)
COMMON /SWELL/ PLTM(200),VAR(200,2),VOL(200,2)
DIMENSION PRINT(4),OUTR(1),OUTS(1),OUTT(1)
EQUIVALENCE (OUTR,M),(OUTS,PLTM),(OUTT,H)
DIMENSION X(41),Y(41)
DATA PRINT/30.,60.,90.,120./,ITSTP/200/
BEGIN TIME ITERATION LOOP
GO TO (8031,8032,8033,8034,8035,8036),ILFQ

8031 CONTINUE
IST = 6
JST = 6
IND = IDP-5
JND = JDP-5
NX = IND-JST+1
NY = JND-JST+1
EO = 1.0/(NX*NY)
I1 = IST+1
JJ = JST+1
X(b) = XSTRT
X(5) = X(6)-2.0*XINC
X(4) = X(5)-4.0*XINC
X(3) = X(4)-8.0*XINC
X(2) = X(3)-16.0*XINC
X(1) = X(2)-32.0*XINC
DO 6 I=II,IND
6 X(I) = X(I-1)+XINC
X(IND+1) = X(IND)+2.0*XINC
X(IND+2) = X(IND+1)+4.0*XINC
X(IND+3) = X(IND+2)+8.0*XINC
X(IND+4) = X(IND+3)+16.0*XINC
X(IND+5) = X(IND+4)+32.0*XINC
MYP00100
MYP00200
MYP00300
MYP00400
MYP00500
MYP00600
MYP00700
MYP00800
MYP00900
MYP01000
MYP01100
MYP01200
MYP01300
MYP01400
MYP01500
MYP01600
MYP01700
MYP01800
MYP01900
MYP02000
MYP02100
MYP02200
MYP02300
MYP02400
MYP02500
MYP02600
MYP02700
MYP02800
MYP02900
MYP03000
MYP03100
MYP03200
MYP03300
MYP03400
MYP03500
MYP03600
MYP03700
MYP03800

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MYP04000  
MYP04100  
MYP04200  
MYP04300  
MYP04400  
MYP04500  
MYP04600  
MYP04700  
MYP04800  
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MYP05000  
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MYP05400  
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MYP06100  
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MYP06300  
MYP06400  
MYP06500  
MYP06600  
MYP06700  
MYP06800  
MYP06900  
MYP07000  
MYP07100  
MYP07200  
MYP07300  
MYP07400  
MYP07500  
MYP07600

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Y(6) = YSTRT
Y(5) = Y(6)-2.0*YINC
Y(4) = Y(5)-4.0*YINC
Y(3) = Y(4)-8.0*YINC
Y(2) = Y(3)-16.0*YINC
Y(1) = Y(2)-32.0*YINC
DO 7 J=J,JND
7 Y(J) = Y(J-1)+YINC
Y(JND+1) = Y(JND)+2.0*YINC
Y(JND+2) = Y(JND+1)+4.0*YINC
Y(JND+3) = Y(JND+2)+8.0*YINC
Y(JND+4) = Y(JND+3)+16.0*YINC
Y(JND+5) = Y(JND+4)+32.0*YINC
MAXLL = 4
LL = 1
IN = 1
LINES = 60
RETURN

C* C* C
8032 CONTINUE
IF (ISW1 .NE. 0) GO TO 330
310 ISW1 = 1
C CALC INITIAL MOMENTUM AND VOLUME
PLTM(1) = 0.0
VAR(1,1) = 0.0
VAR(1,2) = 0.0
E1 = 0.0
E3 = 0.0
DO 320 J=2,JDM
E4 = 0.25*(Y(J+1)-Y(J-1))
DO 320 I=2,IDM
B1 = E4*(X(I+1)-X(I-1))
E1 = E1+B1*SQRT(M(I+1,J+1)*M(I+1,J+1)+N(I+1,J+1))
E3 = E3+P(I+1,J+1)*B1
320 CONTINUE
VOL(1,1) = E1
VOL(1,2) = E3
330 CONTINUE

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113\*  
114\*

E5 = 0.0  
E6 = 0.0  
E7 = 0.0  
E8 = 0.0  
E9 = 0.0  
E10 = 0.0  
E11 = 0.0  
E12 = 0.0  
RETURN

C\*  
8033

CONTINUE

IF (I .LT. IST.OR.I .GT. IND) GO TO 600  
IF (J .LT. JST.OR.J .GT. JND) GO TO 600

C

CALCULATE REL VAR OF MOMENTUM AND DEPTH  
E1 = 0.25\*(X(I+1)-X(I-1))\*(Y(J+1)-Y(J-1))

E3 = SQRT(M(I-1,J-1)\*M(I-1,J-1)+N(I-1,J-1)\*N(I-1,J-1))

E4 = E1+E3

E9 = E9+E4

E11 = E11+E4+E4

E3 = E3/P(I-1,J-1)

E10 = E10+P(I-1,J-1)

E12 = E12+P(I-1,J-1)\*P(I-1,J-1)

E2 = SQRT(M(I,J)\*M(I,J)+N(I,J)\*N(I,J))

E4 = E4-E1+E2

E5 = E5+E4

E7 = E7+E4+E4

E3 = P(I-1,J-1)-P(I,J)

E6 = E6+E3

E8 = E8+E3+E3

CONTINUE

600 RETURN

C\*  
8034

CONTINUE

E1 = (E7-E5+E5+E0)

E2 = (E8-E6+E6+E0)

E3 = E1/(E11-E9+E9+E0)

E4 = E2/(E12-E10+E10+E0)

CALC MOMENTUM AND VOLUME

C

MYP07700  
MYP07800  
MYP07900  
MYP08000  
MYP08100  
MYP08200  
MYP08300  
MYP08400  
MYP08500  
MYP08600  
MYP08700  
MYP08800  
MYP08900  
MYP09000  
MYP09100  
MYP09200  
MYP09300  
MYP09400  
MYP09500  
MYP09600  
MYP09700  
MYP09800  
MYP09900  
MYP10000  
MYP10100  
MYP10200  
MYP10300  
MYP10400  
MYP10500  
MYP10600  
MYP10700  
MYP10800  
MYP10900  
MYP11000  
MYP11100  
MYP11200  
MYP11300  
MYP11400

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```

E5 = 0.0
E7 = 0.0
DO 610 J=2,JDM
  E8 = 0.25*(Y(J+1)-Y(J-1))
  DO 610 I=2,IDM
    E9 = E8*(X(I+1)-X(I-1))
  E5 = E5+E9*SQRT(M(I,J)*M(I,J)+N(I,J)*N(I,J))
  E7 = E7+P(I,J)*E9
610 CONTINUE
E1 = E5
E2 = E7
IN = IN+1
IF (IN.GT. 200) GO TO 620
PLTM(IN) = TIM
VAR(IN,1) = E3
VAR(IN,2) = E4
VOL(IN,1) = E1
VOL(IN,2) = E2
IF (NN.GT. 1) GO TO 620
E5 = VOL(1,1)
E6 = VOL(1,2)
E7 = 0.0
IF (KFLG2.EQ. 0) GO TO 630
WRITE (XOTFIL,2001)
WRITE (XOTFIL,2000) JFLG,E5,E6,E7,E7,E7
LINES = 1
620 IF (KFLG2.EQ. 0) GO TO 630
IF (LINES.GT. 57) WRITE (XOTFIL,2001)
LINES = 1
WRITE (XOTFIL,2000) ISM,E1,E2,E3,E4,TIM
630 CONTINUE
RETURN
C*C*C
8035 CONTINUE
LLST = LL
C OUTPUT CALCULATIONS IF CORRECT TIME STEP
IF (JFLG.EQ. 1) GO TO 1410
IF (PRINT(LL)*60.0.GT. TIM) GO TO 1700

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MYP11500  
MYP11600  
MYP11700  
MYP11800  
MYP11900  
MYP12000  
MYP12100  
MYP12200  
MYP12300  
MYP12400  
MYP12500  
MYP12600  
MYP12700  
MYP12800  
MYP12900  
MYP13000  
MYP13100  
MYP13200  
MYP13300  
MYP13400  
MYP13500  
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MYP13700  
MYP13800  
MYP13900  
MYP14000  
MYP14100  
MYP14200  
MYP14300  
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MYP14500  
MYP14600  
MYP14700  
MYP14800  
MYP14900  
MYP15000  
MYP15100  
MYP15200



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153* IF (ISMOTH.EQ. 0) GO TO 1405
154* IF (ISM.NE. ISMOTH) GO TO 1700
155* LL = LL+1
156* IS1 = NETRAD
157* NETRAD = JFLG
158* TS1 = SURFTA
159* IS2 = NCNTO
160* SURFTA = TIM
161* NCNTO = NN
162* IOF = IOF +1
163* CALL BLKOUT(S111,NETRAD,IOF,SPARE,ISTS)
164* NETRAD = IS1
165* SURFTA = TS1
166* NCNTO = IS2
167* IF (KFLG2.GT. 0) WRITE (XOTFIL,2007) IOF
168* CONTINUE
169* RETURN
170*
C* C* C
8036 END OF ITERATIONS
C
IF (IN.GT. 200) IN = 200
IS1 = NETRAD
NETRAD = -IN
IOF = IOF+1
DO 1810 I=1,1000
OUTT(I) = OUTR(I)
DO 1820 I=1,1000
OUTR(I) = OUTS(I)
CALL BLKOUT(S111,NETRAD,IOF,SPARE,ISTS)
NETRAD = IS1
DO 1830 I=1,1000
OUTR(I) = OUTT(I)
CALL BLKIN(1801,H,1,WSTRRI,ISTS)
WRITE (XOTFIL,2002) IOF
IF (KFLG2.EQ. 0) GO TO 1850
IF (JFLG.EQ. 1) GO TO 1840
WRITE (XOTFIL,2003) NN,TIM
GO TO 1850
1810
1820
1830
1840
1850
1860
1870
1880
1890
1900
MYP15300
MYP15400
MYP15500
MYP15600
MYP15700
MYP15800
MYP15900
MYP16000
MYP16100
MYP16200
MYP16300
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MYP16900
MYP17000
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MYP17900
MYP18000
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MYP18200
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MYP18500
MYP18600
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MYP18800
MYP18900
MYP19000

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191*	1840	WRITE (XOTFIL,2004) NR,TIM	MYP19100
192*	1850	CONTINUE	MYP19200
193*		RETURN	MYP19300
194*	2000	FORMAT ('ISM=',I3,'MOMENTUM=',E12.6,'/VOLUME=',E12.6,'/REL VARMYP19400	MYP19500
195*	1	MOMENTUM=',E12.6,'/REL VAR DEPTH=',E12.6,'/TIME=',F10.4)	MYP19600
196*	2001	FORMAT ('1')	MYP19700
197*	2002	FORMAT ('0',20X,'*** ANALYSIS - MESO-SCALE SOLUTION COMPLETED, ',IMYP19800	MYP19900
198*	12,	'BLOCKS WRITTEN TO FILE SPARE **')	MYP20000
199*	2003	FORMAT ('* SOLUTION STOPPED AT TIME STEP ',I3,'MODEL TIME ',F8.3MYP20100	MYP20200
200*	1,	'SECONDS')	MYP20300
201*	2004	FORMAT ('* SOLUTION CONVERGED AT TIME STEP ',I3,'MODEL TIME ',F8MYP20400	
202*	1.3,	'SECONDS')	
203*	2007	FORMAT ('0 BLOCK ',I6,'WRITTEN TO TEMP FILE SPARE')	
204*		END	

```

1* SUBROUTINE TRYDIF
2* INCLUDE MESSAGE,LIST
3* CALCULATE TRAJECTORY AND ASSOCIATED PARAMETERS
4* INCLUDE DIFUZZ,LIST
5* INCLUDE COMWIND,LIST
6* INCLUDE WNDOTB,LIST
7* INCLUDE SOURCE,LIST
8* INCLUDE FILES,LIST
9* DATA GAMMA/-1.0/
10* DATA KINDSO,SIGXO,SIGYO,SIGZO/0.3*-1.0/
11* NAMELIST /ULST2/ XSOUR,YSOUR,Q,SIGXO,SIGYO,SIGZO,H,Z,TAU,ALPHA,
12* 1BETA,ZSOUR,KINDSO,DECAY,BLAMDA,GAMMA,STTEMP,RADIUS,EXTVEL,VS,
13* 2CONISS,DOSISS,TEMPSF,RTLAPS,KFLG1,KFLG2
14* IF (TYPE3 .GT. 0) READ (XINFIL,QLST2)
15* IF (TYPE3 .LT. 0) KINDSO = IABS(TYPE3)
16* TYPE3 = IABS(TYPE3)
17* IF (KINDSO .NE. 0) GO TO 10
18* IF (ALPHA .LE. 0.0) ALPHA = 1.0
19* IF (BETA .LE. 0.0) BETA = 1.0
20* IF (Q .LE. 0.0) Q = 1.0
21* IF (TAU .LE. 0.0) TAU = 2.5
22* GO TO 20
23* 10 IF (ALPHA .LE. 0.0) ALPHA = 0.9
24* IF (BETA .LE. 0.0) BETA = 1.0
25* IF (KINDSO .EQ. 2) GO TO 15
26* IF (Q .LE. 0.0) Q = 2520.0
27* IF (STTEMP .LE. 0.0) STTEMP = 366.3
28* IF (RADIUS .LE. 0.0) RADIUS = 4.877
29* IF (EXTVEL .LE. 0.0) EXTVEL = 2.1476
30* IF (H .LE. 0.0) H = 252.4
31* IF (XSOUR .LE. 0.0) XSOUR = 356000.0
32* IF (YSOUR .LE. 0.0) YSOUR = 3520100.0
33* IF (ZSOUR .LE. 0.0) ZSOUR = 1150.6
34* GO TO 20
35* 15 IF (Q .LE. 0.0) Q = 1764.0
36* IF (STTEMP .LE. 0.0) STTEMP = 352.4
37* IF (RADIUS .LE. 0.0) RADIUS = 3.658
38* IF (EXTVEL .LE. 0.0) EXTVEL = 2.7512

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IF (H .LE. 0.0) H = 186.5
IF (XSOUR .LE. 0.0) XSOUR = 356000.0
IF (YSOUR .LE. 0.0) YSOUR = 3520100.0
IF (ZSOUR .LE. 0.0) ZSOUR = 1150.6
20 CONTINUE
IF (GAMMA .LT. 0.0) GAMMA = 1.0
IF (CONISS(1) .GT. 0.0) GO TO 30
CONISS(1) = 1.0E-4
CONISS(2) = 1.0E-6
CONISS(3) = 1.0E-12
30 IF (DOSISS(1) .GT. 0.0) GO TO 40
DOSISS(1) = 1.0E-4
DOSISS(2) = 1.0E-6
DOSISS(3) = 1.0E-12
40 CONTINUE
IF (KFLG2 .GT. 0) WRITE (XOTFIL,QLST2)
CALL TRNPRT
IF (TYPE3 .LT. 0) RETURN
CALCULATE DIFFUSION
CALL DIFFUZ
RETURN
END

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TRY03900  
TRY04000  
TRY04100  
TRY04200  
TRY04300  
TRY04400  
TRY04500  
TRY04600  
TRY04700  
TRY04800  
TRY04900  
TRY05000  
TRY05100  
TRY05200  
TRY05300  
TRY05400  
TRY05500  
TRY05600  
TRY05700  
TRY05800  
TRY05900  
TRY06000



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1* SUBROUTINE TRNPRT
2* INCLUDE DIFUZZ,LIST
3* INCLUDE COMMON,LIST
4* INCLUDE WDDOTB,LIST
5* INCLUDE FILES,LIST
6* INCLUDE SOURCE,LIST
7* REAL MM,NN
8*
9* C
10* C
11* C
12* C
13* C
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37* C
38* C

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      DEFINE AN ARRAY STOR FROM XX(1) IN COMMON DIFUZZ TO END OF COMMON
      TO PROVIDE AN EQUIVALENCE INDEX. STOR(9) IS MM OR THE 13 TH
      VARIABLE IN COMMON. STOR(1690) IS NN OR 41X41 PNTS. AWAY,
      STOR(3371) IS PP OR 41X41 PNTS. AWAY.
      DIMENSION STOR(5000),MM(41,41),NN(41,41),PP(41,41)
      EQUIVALENCE (STOR(1),XX(1))
      SET STORAGE ADDRESSES FOR SOLUTION ARRAYS OBTAINED FROM SAVE FILE
      MXLYRF
      EQUIVALENCE (STOR(9),MM(1,1)),(STOR(1690),NN(1,1)),(STOR(3371),PP(
11,1))
      DEFINE ARRAYS U,V AND W TO HOLD INTERNAL 31X31 REGION OF ARRAYS
      MM,MM AND PP, ALSO X AND Y AXES ARRAYS
      DIMENSION U(31,31),V(31,31),W(31,31),X(31),Y(31)
      SET STORAGE ADDRESSES FOR U,V AND W ARRAYS (INTERNAL 31X31 PNTS OF
      MM,NN AND PP) AT UPPER END OF COMMON DIFUZZ
      EQUIVALENCE (STOR(2169),U(1,1)),(STOR(3130),V(1,1)),(STOR(4091),W(
11,1))
      SET STORAGE ADDRESS FOR X AND Y AXES OF 31X31 INTERNAL GRID
      EQUIVALENCE (R(1),X),(R(32),Y)
      DEFINE WHERE IB,NX AND NY COME FROM
      EQUIVALENCE (IB,HMIN),(NX,IDP),(NY,JDP)
      NO. OF PNTS. IN TRAJECTORY IB IS PASSED TO SUB DIFUZZ THROUGH HMIN
      REMAINING EQUIVALENCE IS TO SAVE STORAGE
      EQUIVALENCE (K1,R(66)),
1(UVMX,R(67)),(DX,R(68)),(UUL,R(69)),(VVL,R(70)),(HXYM,R(71)),
2(HXM,R(72)),(HX,R(73)),(HY,R(74)),(HX1,R(75)),(HY1,R(76)),
3(HX5,R(77)),(HY5,R(78)),(HX21,R(79)),(HY21,R(80)),(HXY4,R(81)),
4(U1,R(82)),(V1,R(83)),(U2,R(84)),(V2,R(85)),(XD,R(86)),(DT,R(87)),
5(T,R(88)),(X0,R(89)),(Y0,R(90)),(N,R(91)),(K,R(92)),(NT,R(93)),
6(X1,R(94)),(Y1,R(95)),(UX,R(96)),(UY,R(97)),(UXX,R(98)),
7(UYY,R(99)),(UXY,R(100)),(VX,R(101)),(VY,R(102)),(VXX,R(103)),

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39*      8(VVY,R(104)),(VXY,R(105)),(AH,R(106)),(AK,R(107)),(UU,R(108)),      TRN03900
40*      9(VV,R(109)),(UU1,R(110)),(VV1,R(111))                                TRN04000
41*      EQUIVALENCE (HM1,R(112)),(HMJ,R(113)),(XP,R(114)),(YP,R(115)),      TRN04100
42*      1(S1,R(116)),(S2,R(117))                                              TRN04200
43*                                                                              TRN04300
44*      C C THIS SUBROUTINE CALCULATES THE TRAJECTORY OF THE CENTROID OF THE   TRN04400
45*      C C CLOUD FROM THE RELEASE (SOURCE) POINT XSOURC,YSOURC. THE INCREMENT TRN04500
46*      C C BETWEEN SUCCESSIVE POINTS IS 1/10 THE GRID SPACING (DX). ALSO,    TRN04600
47*      C C THIS SUB CALCULATES THE LAYER WIND SPEED AND DEPTH AT EACH       TRN04700
48*      C C TRAJECTORY POINT AND PASSES THIS INFO TO SUB DIFFUZ. THIS SUB    TRN04800
49*      C C ASSUMES THE REAL TERRAIN GRID REGION IS A 31X31 MATRIX (WITH     TRN04900
50*      C C EXPANDED REGION 41X41).                                           TRN05000
51*      C C U,V,W - ARE THE U AND V COMPONENTS OF THE WIND FIELD SOLUTION     TRN05100
52*      C C AND W IS THE LAYER HEIGHT (CONVERTED TO DEPTH) OF THE           TRN05200
53*      C C WIND FIELD SOLUTION OVER THE REAL TERRAIN (31X31) MATRIX.        TRN05300
54*      C C THESE DATA ARE TAKEN FROM THE ARRAYS MM,NN,PP.                  TRN05400
55*      C C MM,NN,PP - ARE THE U,V AND P COMPONENTS OF THE WIND FIELD        TRN05500
56*      C C TAKEN FROM THE FILE HOLDING THE LATEST WIND FIELD              TRN05600
57*      C C SOLUTION                                                         TRN05700
58*      C C THE LATEST SOLUTION FILE IS READ INTO COMMON DIFUZZ WHICH IS     TRN05800
59*      C C GREATER THAN OR EQUAL IN SIZE TO COMMON MAXRUFZ DEFINED IN SUB    TRN05900
60*      C C MAXSTR. THE INFO THAT IS NEEDED FROM THE FILE IS NETRAD (NET -    TRN06000
61*      C C RADIATION INDEX), XSOURC,YSOURC,ZSOURC (COORDINATES OF SOURCE    TRN06100
62*      C C ANALYSIS) AND THE M,N AND P ARRAYS FROM THE ANALYSIS PHASE. TO   TRN06200
63*      C C SAVE STORAGE THE U,V,W AND MM,NN,PP ARRAYS SHARE THE SAME        TRN06300
64*      C C BLOCK IN COMMON DIFUZZ. WE MUST INPUT MM,NN AND PP AS 41X41     TRN06400
65*      C C ARRAYS, BUT WE ARE ONLY GOING TO USE THE INTERNAL 31X31 PART OF   TRN06500
66*      C C THE ARRAYS. IF THE PRESENT ARRAY SIZE IS CHANGED THE USER        TRN06600
67*      C C SHOULD STUDY THE COMMON DIFUZZ AND THE ABOVE DIMENSION AND        TRN06700
68*      C C STATEMENTS TO MAKE SURE STORAGE IS ALIGNED CORRECTLY..          TRN06800
69*      C C                                                                    TRN06900
70*      C C                                                                    TRN07000
71*      C C                                                                    TRN07100
72*      C C                                                                    TRN07200
73*      C C                                                                    TRN07300
74*      C C                                                                    TRN07400
75*      C C                                                                    TRN07500
76*      C C                                                                    TRN07600

```

HOURS = IHOURL\*100+MINUTE  
 GET LAST WINDFIELD SOLUTION  
 N2 = 3\*IDP\*JUP+68  
 K2 = 2  
 IF (KFLG1.NE. 0) K2 = 1  
 CALL BLKIN(N2,NETRAD,K2,MXL,YRF,ISTS)

```

77*      N2 = IDP-5
78*      K2 = JDP-5
79*      C      PACK ARRAYS DOWN TO 31X31 MATRICES
80*      DO 10 J=6,K2
81*      DO 10 I=6,N2
82*      10 W(N2-I+1,K2-J+1) = PP(IDP-I+1,JDP-J+1)
83*      DO 20 J=6,K2
84*      DO 20 I=6,N2
85*      20 V(N2-I+1,K2-J+1) = NN(IDP-I+1,JDP-J+1)
86*      DO 30 J=6,K2
87*      DO 30 I=6,N2
88*      30 U(N2-I+1,K2-J+1) = MM(IDP-I+1,JDP-J+1)
89*      C      GET TERRAIN ELEVATION HEIGHTS
90*      N1 = IDP*JDP
91*      CALL BLKIN(N1,MM(1,1),1,WSTRN,ISTS)
92*      C      CONVERT HEIGHT W TO DEPTH
93*      DO 40 J=6,K2
94*      DO 40 I=6,N2
95*      40 W(I-5,J-5) = W(I-5,J-5)-MM(I,J)
96*      C      IF XSOUR AND YSOUR ARE INPUT USE THOSE
97*      IF (XSOUR.GT. 0.0) XSOURC = XSOUR
98*      IF (YSOUR.GT. 0.0) YSOURC = YSOUR
99*      IF (ZSOUR.GT. 0.0) ZSOURC = ZSOUR
100*      C      CALCULATE X AND Y AXES
101*      IDP = IDP-10
102*      JDP = JDP-10
103*      X(1) = XSTRT
104*      Y(1) = YSTRT
105*      DO 50 I=2,IDP
106*      50 X(I) = X(I-1)+XINC
107*      DO 60 J=2,JDP
108*      60 Y(J) = Y(J-1)+YINC
109*      N2 = IDP-1
110*      K2 = JDP-1
111*      XMIN = AMIN1(XINC,YINC)
112*      C      CALL MAXIMIM VECTOR
113*      UVMX = 0.0
114*      DO 70 J=1,JDP

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TRN07700
TRN07800
TRN07900
TRN08000
TRN08100
TRN08200
TRN08300
TRN08400
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TRN09800
TRN09900
TRN10000
TRN10100
TRN10200
TRN10300
TRN10400
TRN10500
TRN10600
TRN10700
TRN10800
TRN10900
TRN11000
TRN11100
TRN11200
TRN11300
TRN11400

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115* DO 70 I=1,IDP
116* 70 UVMX = AMAX1(UVMX,U(I,J)*U(I,J)+V(I,J)*V(I,J))
117* UVMX = SQRT(UVMX)
118* C CALC INCREMENT IN METERS FOR TRAJECTORY POINTS
119* DX = 0.1*XMIN
120* C LAST U AND V COMP CALCULATED
121* UUL = UVMX
122* VVL = UVMX
123* C SET CONSTANTS BECAUSE EVENLY SPACED GRID
124* HXYM = XMIN
125* HXM = 0.05*HXYM
126* HX = X(2)-X(1)
127* HY = Y(2)-Y(1)
128* HX1 = 0.5/HX
129* HY1 = 0.5/HY
130* HX5 = .5*HX
131* HY5 = .5*HY
132* HX21 = 2.0*HX1*HX1
133* HY21 = 2.0*HY1*HY1
134* HXY4 = HX1*HY1
135* U1 = 0.0
136* V1 = 0.0
137* U2 = 0.0
138* V2 = 0.0
139* XD = 0.0
140* C DELTA - TIME
141* DT = DX/(0.5*UVMX)
142* T = 0.0
143* N1 = 0
144* K1 = 0
145* IB = 0
146* XU = XSOURC
147* YU = YSOURC
148* IF (XU .GT. X(NX).OR.XO .LT. X(1)) GO TO 200
149* IF (YU .GT. Y(NY).OR.YO .LT. Y(1)) GO TO 200
150* C LOOP THROUGH TRAJ POINTS UNTIL 310 OR LEAVES GRID.
151* LINES = 80
152* 80 CONTINUE

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B-100

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N = INT((XO-X(1))*HX1*2,0)+1
IF (XO-X(N) .GT. HX5) N = N+1
IF (N .GE. NX) N = NX-1
IF (N .LE. 1) N = 2
K = INT((YO-Y(1))*HY1*2,0)+1
IF (YO-Y(K) .GT. HY5) K = K+1
IF (K .GE. NY) K=NY-1
IF (K .LE. 1) K = 2
CALC NEXT UU,VV
NT = 0
X1 = XO
Y1 = YO
IF (N1 .EQ. N.AND.K1 .EQ. K) GO TO 140
N1 = N
K1 = K
UX = (U(N+1,K)-U(N-1,K))*HX1
UY = (U(N,K+1)-U(N,K-1))*HY1
UXX = HX21*(U(N-1,K)-U(N,K)-U(N,K)+U(N+1,K))
UYX = HY21*(U(N,K-1)-U(N,K)-U(N,K)+U(N,K+1))
UXY = HXY4*(U(N+1,K+1)-U(N-1,K-1)-U(N+1,K-1)+U(N-1,K-1))
VX = (V(N+1,K)-V(N-1,K))*HX1
VY = (V(N,K+1)-V(N,K-1))*HY1
VXX = HX21*(V(N-1,K)-V(N,K)-V(N,K)+V(N+1,K))
VYX = HY21*(V(N,K-1)-V(N,K)-V(N,K)+V(N,K+1))
VXY = HXY4*(V(N+1,K+1)-V(N-1,K-1)-V(N-1,K-1)+V(N-1,K-1))
140 CONTINUE
AH = X1-X(N)
AK = Y1-Y(K)
UU = U(N,K)+AH*UX+AK*UY+AH*AH*UXX+AH*AK*UXY+AK*AK*UYY
VV = V(N,K)+AH*VX+AK*VY+AH*AH*VXX+AH*AK*VXY+AK*AK*VYY
IF (NT .NE. 0) GO TO 150
NT = 3
X1 = X1+UU*DT
Y1 = Y1+VV*DT
UU1 = UU
VV1 = VV
GO TO 140
150 CONTINUE

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TRN15300  
TRN15400  
TRN15500  
TRN15600  
TRN15700  
TRN15800  
TRN15900  
TRN16000  
TRN16100  
TRN16200  
TRN16300  
TRN16400  
TRN16500  
TRN16600  
TRN16700  
TRN16800  
TRN16900  
TRN17000  
TRN17100  
TRN17200  
TRN17300  
TRN17400  
TRN17500  
TRN17600  
TRN17700  
TRN17800  
TRN17900  
TRN18000  
TRN18100  
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TRN19000

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191*      UU = 0.5*(UU+UU1)
192*      VV = 0.5*(VV+VV1)
193*      160 IF (IB.NE. 0) GO TO 170
194*      GO TO 175
195*      165 HMI = HMJ
196*      IB = IB+1
197*      170 IF (UU) 173,171,173
198*      171 IF (VV) 173,172,173
199*      172 UU = UUL
200*      VV = VVL
201*      173 X1 = SQRT(UU*UU+VV*VV)
202*      UUL = UU
203*      VVL = VV
204*      DT = DX/X1
205*      X0 = X0+DT*UU
206*      Y0 = Y0+DT*VV
207*      IF (X0.LT.X(1).OR.X0.GT.X(NX).OR.Y0.LT.Y(1).OR.Y0.GT.Y(NY)) GO TO
1200
208*      T = 1+UT
209*      XU = XU+DX
210*      175 IF (X0.GE. X(N2).AND.X0.LE. X(N2+1)) GO TO 177
211*      N2 = NX-1
212*      176 IF (X0.GE. X(N2)) GO TO 177
213*      N2 = N2-1
214*      IF (N2.GT. 1) GO TO 176
215*      177 IF (Y0.GE. Y(K2).AND.Y0.LE. Y(K2+1)) GO TO 179
216*      K2 = NY-1
217*      178 IF (Y0.GE. Y(K2)) GO TO 179
218*      K2 = K2-1
219*      IF (K2.GT. 1) GO TO 178
220*      C      CALC MIXING LAYER DEPTH
221*      XP = (X0-X(N2))/(X(N2+1)-X(N2))
222*      YP = (Y0-Y(K2))/(Y(K2+1)-Y(K2))
223*      HMJ = (1.0-XP)*(1.0-YP)*W(N2,K2)+XP*(1.0-YP)*W(N2+1,K2)+
224*      1(1.0-XP)*YP*W(N2,K2+1)+XP*YP*W(N2+1,K2+1)
225*      IF (IB.EQ. 0) GO TO 165
226*      HMI = 0.5*(HMJ+HMI)
227*      XX(IB) = X0
228*

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TRN19100
TRN19200
TRN19300
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TRN19800
TRN19900
TRN20000
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TRN20200
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TRN21600
TRN21700
TRN21800
TRN21900
TRN22000
TRN22100
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TRN22300
TRN22400
TRN22500
TRN22600
TRN22700
TRN22800

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1* SUBROUTINE DIFFUZ
2* INCLUDE TIMES,LIST
3* INCLUDE MESSAGE,LIST
4* INCLUDE FILES,LIST
5* INCLUDE DIFFUZ,LIST
6* INCLUDE COMMON,LIST
7* INCLUDE SOURCE,LIST
8* DATA NUMX/310/
9* SET LENGTH OF ARRAYS XX,YY,ETC IN NUMX
10*
11* THIS SUBROUTINE CALCULATES THE DIFFUSION PARAMETERS CONCENTRATION,
12* DOSAGE, DEPOSITION, ETC AND OUTPUTS THE SOLUTION TO SAVE FILE
13* DIMENSION SIGAT(7,5),SIGAM(7,5),SIGET(7,5),PWR(7,5),UBRT(5)
14* 1,SIGEN(7,5)
15* DIMENSION CHIT(310),DOST(310),SIGMY(310),YCHIT(310,3),YDOST(310,3)
16* PASS NO. OF PNTS. IN TRAJECTORY THROUGH COMMON VIA HMIN
17* EQUIVALENCE (HMIN,NPNT)
18* DEFINE STORAGE ADDRESSES FOR DIFFUSION CALCULATION ARRAYS
19* EQUIVALENCE (CHIT,R(1)),(DOST,R(311)),(SIGMY,R(621)),
20* 1(YCHIT,R(931)),(YDOST,R(1861))
21*
22* EQUIVALENCE (NCALC,NETRAD)
23* DIMENSION CONI(3),DOSI(3)
24* EQUIVALENCE (KINDS,SURFTA),(CONI,POTMPR(1)),(DOSI,POTMPR(4))
25* DIMENSION KLAPE(3,4),TEMPSD(4,12)
26* DATA KLAPE/.005,.003,.001,.015,.010,.005,.030,.020,.015,.040,.030/
27* 1,.020/
28* DATA TEMPSD/292.,286.,279.,272.,296.,290.,282.,275.,300.,294.,286.,
29* 1,277.,303.,299.,290.,282.,308.,304.,295.,287.,312.,308.,300.,292.,
30* 2312.,308.,301.,294.,310.,307.,300.,293.,308.,304.,297.,289.,303.,
31* 3299.,291.,283.,297.,292.,284.,275.,293.,287.,280.,272./
32* DATA SIGAT/26.,26.,21.,15.,11.,8.,6.,26.,22.,16.,11.,10.,8.,6.,
33* 1,19.,16.,13.,2*9.,2*7.,8.,14.,2*11.,7.,2*6.,7.,2*8.,7.,2*6.,7/
34* DATA SIGAM/2*-.109,-.133,-.112,-.120,2*-.189,-.109,-.128,-.123,
35* 1-.112,-.120,2*-.189,-.122,-.123,-.103,-.120,-.134,-.207,-.189,
36* 2-.105,2*-.117,-.148,-.126,-.287,-.189,-.1,-.117,-.11,-.146,-.126,
37* 3-.287,-.189/
38* DATA SIGEN/2*1.,07,2*0.,-.20,-.3,1.,13,.07,2*0.,-.2,-.25,.15,

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1.15,.13,2\*0,.2\*-2,2\*2,.15,2\*0,.2\*-15,.25,2\*2,2\*0,.2\*-15/  
DATA SIGET/2\*8.7,7.0,5.0,3.7,2\*2.9,8.7,7.4,5.3,3.7,3.3,2\*2.9,6.3,  
15.3,4.3,2\*3.0,2\*2.6,4.7,2\*3.7,2\*2.7,2\*2.2,2\*3.0,3\*2.7,2\*2.2/  
DATA PWR/6\*.20,.30,.20,.17,4\*.2,.25,2\*.15,2\*.17,3\*.2,2\*.10,5\*.15,  
1.05,3\*.10,3\*.15/  
DATA UBRT/1.0,3.0,5.0,7.0,99.0/RAD/.01745329/  
PTERP(A,B,C,D,E) = A-(B-C)\*(A-D)/(B-E)  
CISO(A,B) = Sqrt(A\*ALOG(B))  
  
CHIL = 1.0E20  
IF (KINDSO .EQ. 0) KFLG = 1  
SUMN = 0.0  
ALPHA1 = 1.0/ALPHA  
BETA1 = 1.0/BETA  
LFLG = 0  
MFLG = 0  
IF (KINDSO .NE. 0) GO TO 10  
GP = 0\*6.3493636E-2  
HP = H  
HPP = H  
IF (HP.LI. 5.0) HP = 5.0  
MFLG = 1  
GO TO 20  
10 GP = 0\*.159154943  
IF (TEMPSF .GT. 0.0) SURFIA = TEMPSF  
IF (SURFTA .GT. 0.0) GO TO 20  
DEFAULT SURFACE TEMP  
IF (NETRAD .EQ. 4) GO TO 17  
IF (NETRAD .GE. 2) GO TO 16  
IF (NETRAD .GE. 0) GO TO 15  
L1 = 4  
GO TO 18  
15 L1 = 3  
GO TO 18  
16 L1 = 2  
GO TO 18  
17 L1 = 1  
18 SURFIA = TEMPSD(L1,MONTH)  
  
DIF03900  
DIF04000  
DIF04100  
DIF04200  
DIF04300  
DIF04400  
DIF04500  
DIF04600  
DIF04700  
DIF04800  
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DIF06400  
DIF06500  
DIF06600  
DIF06700  
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DIF06900  
DIF07000  
DIF07100  
DIF07200  
DIF07300  
DIF07400  
DIF07500  
DIF07600

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77* 20 CONTINUE
78*   LINE = 80
79*   BEGIN LOOP OVER TRAJECTORY POINTS
80*   SIGXL = SIGXO
81*   SIGZL = SIGZO
82*   SIGYL = SIGYO
83*   XO = XSOURC
84*   YO = YSOURC
85*   DO 500 K=1,NPNT
86*   DX = SQRT((XX(K)-XO)**2+(YY(K)-YO)**2)
87*   XU = XX(K)
88*   YU = YY(K)
89*   CHI = 0.0
90*   DOS = 0.0
91*   CALCULATE WIND SPEED POWER LAW EXPONENT CATEGORY
92*   DO 50 J=1,5
93*   IF (UBAR(K) .LT. UBRT(J)) GO TO 51
50 CONTINUE
94*   J = 5
51 CONTINUE
95*   I = 5-NETRAD
96*   PWR5 = PWR(I,J)
97*   CALCULATE WIND SPEED AT 5 METERS
98*   UBAR5 = UBAR(K)*(HM(K)-5.0)*5.0**PWR(I,J)*(1.0+PWR(I,J))/
99*   1(HM(K)**(1.0+PWR(I,J))-5.0*(1.0+PWR(I,J)))
100*   IF INSTANTANEOUS OR CONTINUOUS SOURCE
101*   IF (JFLG .NE. 0 .OR. KINDSO .EQ. 0) GO TO 85
102*   JFLG = 1
103*   UBARH = UBAR5*(H*0.2)**PWR5
104*   F = 1.0
105*   IF (UBARH .LE. EXTVEL*6.6666666E-1) GO TO 61
106*   IF (UBARH .GT. EXTVEL) GO TO 60
107*   F = (3.0*EXTVEL-3.0*UBARH)/EXTVEL
108*   GO TO 61
109*   60 F = 0.0
110*   61 IF (NETRAD .GE. 2.0*UBARH .GE. 5.0) GO TO 83
111*   CALC LAPSE RATE OF POTENTIAL TEMP
112*   IF (RTLAPS .GT. 0.0) GO TO 81
113*
114*

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B = 0.0
L = 0
b2 L = L + 1
IF (POTMPR(L) .LE. 0.0) GO TO 65
IF (ZELEVR(L) .LE. ZSOURC+H) GO TO 62
A1 = PTERP(POTMPR(L),ZELEVR(L),ZSOURC+H,POTMPR(L-1),ZELEVR(L-1))
B = ZELEVR(L)-ZSOURC-H
A = (POTMPR(L)-A1)*B
b3 L = L+1
IF (L .GT. 25) GO TO 65
IF (POTMPR(L) .LE. 0.0) GO TO 65
IF (ZELEVR(L) .GT. ZSOURC+H+200.0) GO TO 64
A1 = ZELEVR(L)-ZELEVR(L-1)
A = A+(POTMPR(L)-POTMPR(L-1))*A1
B = B+A1
GO TO 63
64 A1 = PTERP(POTMPR(L),ZELEVR(L),ZSOURC+H+200.0,POTMPR(L-1),ZELEVR(L-1))
A2 = ZSOURC+H+200.0-ZELEVR(L-1)
A = A+(A1-POTMPR(L-1))*A2
B = B+A2
65 IF (B .GT. 0.0) GO TO 80
DEFAULT LAPSE RATE
IF (UGARH .LE. 1.4) GO TO 67
IF (UGARH .LE. 2.9) GO TO 66
L1 = 3
GO TO 68
b6 L1 = 2
GO TO 68
67 L1 = 1
68 IF (NETRAU .GE. 1) GO TO 71
IF (NETRAU .EQ. 0) GO TO 70
IF (NETRAU .EQ. -1) GO TO 69
L2 = 4
GO TO 72
b9 L2 = 3
GO TO 72
70 L2 = 2

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153*      GO TO 72
154*      71 L2 = 1
155*      72 RTLAPS = RLAPSE(L1,L2)
156*      GO TO 81
157*      80 RTLAPS = A/B
158*      81 IF (RTLAPS .LE. 0.0) GO TO 71
159*      A2 = EXTVEL*RADIUS*RADIUS*SURFTA/(UBARH*RTLAPS)
160*      A4 = 9.8*RTLAPS/SURFTA
161*      A1 = 0.1*UBARH/SQRT(A4)
162*      A3 = H/A1
163*      A1 = 3.1415926*A1
164*      IF (A1 .GE. H) GO TO 62
165*      HP = 2.397*F*(A2*(1.0-SURFTA/STTEMP))**.3333333
166*      GAMT = .60
167*      GO TO 84
168*      82 HP = 1.903*F*(A2*(1.0-COS(A3))**.3333333)
169*      GAMT = .66
170*      GO TO 84
171*      83 HP = F*((15.98/UBARH)*(RADIUS*RADIUS*EXTVEL*(1.0-SURFTA/STTEMP)
172*      1*H*H))**.3333333)
173*      GAMT = .6
174*      SIGYL = (GAMT*HP+RADIUS)*.465116279
175*      SIGXL = SIGYL
176*      SIGZL = SIGYL
177*      HP = HP+H
178*      IF (HP .LT. 5.0) HP = 5.0
179*      HPP = HP
180*      85 IF (K .GT. 1) GO TO 86
181*      IF (HPP .LE. HM(1)) GO TO 86
182*      WRITE (XOTFIL,1005)
183*      1005 FORMAT ('0 SOURCE RISE HEIGHT IS ABOVE HM NO CALCULATIONS PRODUCED, OUTPUT HAS ZERGES')
184*      TYPE3 = -1
185*      GO TO 501
186*      86 IF (LFLG .EQ. 1) GO TO 87
187*      IF (HPP .LE. HM(K)) GO TO 88
188*      LFLG = 1
189*      87 HPP = HM(K)
190*
DIF15300
DIF15400
DIF15500
DIF15600
DIF15700
DIF15800
DIF15900
DIF16000
DIF16100
DIF16200
DIF16300
DIF16400
DIF16500
DIF16600
DIF16700
DIF16800
DIF16900
DIF17000
DIF17100
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DIF18900
DIF19000

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191* 86 CONTINUE
192* C CALCULATE WIND SPEED CATEGORY
193* DO 100 J=1,5
194* IF (UBARS.LT. UBRT(J)) GO TO 101
195* 100 CONTINUE
196* J = 5
197* 101 CONTINUE
198* C CALCULATE SIGMA-A
199* SIGAP = SIGAT(I,J)*RAD*(HP*.2)**SIGAM(I,J)
200* IF (KINDSO.EQ. 0) SIGAP = SIGAP*(TAU*1.666666E-3)**.2
201* C CALCULATE SIGMA-E
202* SIGEP = SIGET(I,J)*RAD*(HP*.2)**SIGEN(I,J)
203* C CALCULATE SIGMA-Y
204* SIGY = SIGAP*(DX+(SIGYL/SIGAP)**ALPHA)**ALPHA
205* C CALCULATE SIGMA-Z
206* SIGZ = SIGEP*(DX+(SIGZL/SIGEP)**BETA)**BETA
207* C CALCULATE THE TOP AND BOTTOM OF THE CLOUD
208* ZT = AMIN1(H+2.15*SIGZ, HM(K))
209* ZB = AMAX1(H-2.15*SIGZ, 0.0)
210* C CALCULATE THE MEAN WIND SPEED IN THE LAYER CONTAINING THE CLOUD
211* UBARN = UBARS*(ZT**((1.0+PWRS)-ZB**((1.0+PWRS)))/((1.0+PWRS)*5.0**PWRS)
212* 1S*(ZT-ZB))
213* C CALCULATE THE WIND SPEED SHEAR
214* DELTAU = UBARS*(ZT**PWRS-ZB**PWRS)/5.0**PWRS
215* C CALCULATE SIGMA-X
216* SIGX = 1.395348E-1*DELTAU*DX/UBARN +SIGXL
217* C CALCULATE THE DEPLETION TERMS
218* SUMN = SUMN+DX/UBARN
219* DEAYS = 1.0
220* IF (DECAY.LE. 0.0) GO TO 120
221* DEAYS = EXP(-DECAY*SUMN)
222* 120 CONTINUE
223* TLAMDA = 1.0
224* IF (BLAMDA.LE. 0.0) GO TO 130
225* TLAMDA = EXP(-BLAMDA*SUMN)
226* 130 CONTINUE
227* C CALCULATE THE VERTICAL TERM
228* SIGZI = -0.5/(SIGZ*SIGZ)

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DIF19100
DIF19200
DIF19300
DIF19400
DIF19500
DIF19600
DIF19700
DIF19800
DIF19900
DIF20000
DIF20100
DIF20200
DIF20300
DIF20400
DIF20500
DIF20600
DIF20700
DIF20800
DIF20900
DIF21000
DIF21100
DIF21200
DIF21300
DIF21400
DIF21500
DIF21600
DIF21700
DIF21800
DIF21900
DIF22000
DIF22100
DIF22200
DIF22300
DIF22400
DIF22500
DIF22600
DIF22700
DIF22800

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229*      VERT = 0.0
230*      IF (SIGZI .GE. 0.0) GO TO 220
231*      AR2 = VS*SUMN
232*      AR1 = -HPP+Z+AR2
233*      AR2 = HPP+Z-AR2
234*      C = AR2*AR2*SIGZI
235*      IF (C .LT. -30.0) GO TO 220
236*      D = AR1*AR1*SIGZI
237*      IF (D .LT. -30.0) GO TO 200
238*      VERT = EXP(D)
239*      VERT = VERT+GAMMA*EXP(C)
240*      C = 1
241*      D = GAMMA
242*      E = D*D
243*      A = 0.0
244*      A = A+2.0
245*      B = A*HM(K)
246*      A1 = B-AR2
247*      A1 = A1*A1*SIGZI
248*      IF (A .LE. 2.0.AND.A1 .GT. -30.0) GO TO 215
249*      IF (A1 .LT. -10.0) GO TO 220
250*      215 CONTINUE
251*      A2 = B+AR1
252*      A3 = B-AR1
253*      A4 = B+AR2
254*      VERT = VERT +C*EXP(A1)+D*(EXP(A2*A2*SIGZI)+EXP(A3*A3*SIGZI))+
255*      1E*EXP(A4*A4*SIGZI)
256*      C = D
257*      D = E
258*      E = E*GAMMA
259*      GO TO 210
260*      220 CONTINUE
261*      CHI = (QP/(SIGZ*SIGY))*VERT*DECAYS*TLAMDA
262*      IF (KINDSO .NE. 0) GO TO 230
263*      C      CALCULATE CONCENTRATION EXCEPT FOR LATERAL TERM FOR INSTANTANEOUS
264*      C      VOLUME SOURCE
265*      CHI = CHI/SIGX
266*      GO TO 240

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267* C          CALCULATE CONCENTRATION EXCEPT FOR LATERAL TERM FOR CONTINUOUS
268* C          VOLUME SOURCE
269*   230 CHI = CHI/UBARN
270*   240 CONTINUE
271*       IF (K.EG.1) GO TO 300
272*       IF (MFLG.EQ. 0.AND.CHI.LT. CHIL) MFLG = 1
273*       IF (CHI.LE. CHIL) GO TO 300
274*       IF (MFLG.EQ. 0) GO TO 300
275*       CON IS GREATER - CHANGE SIGX AND SIGY
276*       A1 = SQRT(CHI/CHIL)
277*       SIGX = A1*SIGX
278*       SIGY = A1*SIGY
279*       CHI = CHIL
280*   300 CONTINUE
281*       CHIL = CHI
282*       SIGXL = SIGX
283*       SIGYL = SIGY
284*       SIGZL = SIGZ
285*       IF (KINDSO.NE. 0) GO TO 310
286*       CALCULATE WIND SPEED AT THE CALCULATION HEIGHT Z
287*       A1 = 0.2
288*       IF (Z.GT. 1.0) A1 = A1*Z
289*       UBARZ = UBARS*(A1)**PWKS
290*       C          CALCULATE THE DOSAGE FOR AN INSTANTANEOUS SOURCE
291*       DOS = CHI*2.50662827*SIGX/UBARZ
292*       C          SAVE CALCULATED VALUES
293*   310 CONTINUE
294*       CHIT(K) = CHI
295*       DOST(K) = DOS
296*       SIGMY(K) = SIGY
297*       C          CALCULATE ISOPLETHS OF CON, DOS AND/OR DEP
298*       N = 0
299*       SIGY = 2.0*SIGY*SIGY
300*   320 N = N+1
301*       IF (CONISS(N).LE. 0.0) GO TO 330
302*       A = CHI/CONISS(N)
303*       IF (A.LE. 1.0) GO TO 330
304*       YCHIT(K,N) = CISO(SIGY,A)

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DIF26700  
DIF26800  
DIF26900  
DIF27000  
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DIF29200  
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DIF29500  
DIF29600  
DIF29700  
DIF29800  
DIF29900  
DIF30000  
DIF30100  
DIF30200  
DIF30300  
DIF30400

[illegible]



DIF34300  
DIF34400  
DIF34500  
DIF34600  
DIF34700

CONI(1) = CONISS(1)  
550 DUSI(1) = DOSISS(1)  
CALL BLKOUT(4090,NCALC,1,TRDFFL,ISTS)  
RETURN  
END

343\*  
344\*  
345\*  
346\*  
347\*

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1* SUBROUTINE PLTPRG
2* INCLUDE MESSAGE,LIST
3* INCLUDE BUFKMX,LIST
4* INCLUDE FILES,LIST
5* INCLUDE CONDOWN,LIST
6* INCLUDE WNDTID,LIST
7* INCLUDE NI,LIST
8* DIMENSION COND(310,3,2),DCONC(3,2)
9* DIMENSION IMTL(4),IMTL(4),IMTN(3)
10* DIMENSION CNISS(3),DSISS(3),CDONC(3,2)
11* COMMON /DTAI/J1,J2,J3,J4,J5,J6,J7,J8,J9,J10,J11,J12,J13,RAG,MAXLL
12* 1,XM,YM,MFLGS,SCLX,SCLY,XNCH,YNCH,J14,J15,J16,ISW7,IPLOT,MCORE
13* DIMENSION XX(310),YY(310),SIGMY(310),CHIT(310),DOST(310),
14* 1YCHIT(310,3),YDOST(310,3),DOSI(3),CONI(3)
15* DIMENSION PLTM(200),SPACE(1),VAR(200,2),VOL(200,2),AREA(1),ITL(8),
16* 1UM(1),X(31),Y(31),H(41,41),OUTS(1000),OUTR(3410),IDLBL(4,2)
17* EQUIVALENCE (SPACE,P),(AREA,H),(UM,M),(OUTS,M),(TIM,SURFTA),(KINDS,
18* 10,SURFTA),(CONI,POTMPR(1)),(DOSI,POTMPR(4)),(NN,NCNT0)
19* EQUIVALENCE (YCHIT,CONI),(CONI,DCONC)
20* EQUIVALENCE (CNISS(1),CDONC(1,1)),(DSISS(1),CDONC(1,2))
21* EQUIVALENCE (M,PLTM),(OUTS(201),VAR),(OUTS(601),VOL),(OUTR,UG),
22* 1(X,OUTR(1)),(YY,OUTR(311)),(SIGMY,OUTR(1661)),(CHIT,OUTR(1241)),
23* 2(DOST,OUTR(1551)),(YCHIT,OUTR(2171)),(YDOST,OUTR(3101))
24* DATA IMTL/,INSTANTANEOUS SOURCE,/
25* DATA IMTM/,CONTINUOUS SOURCE '//
26* DATA IMTN/,COPPER/,LEAD/,',',/
27* DATA RAD/,01745/
28* DATA ITL/,TERKAIN HT.,',', (METERS)',', VORTICITY',2*,',',/
29* DATA SCL/1.0E-4/
30* DATA IEVEN/1/
31* DATA ISW/0,1,18*0/
32* DATA CONT/1219.2,1524.,1828.8,2133.6,2438.4,2743.2,3048.,3352.8/
33* DATA NCNT/8/,NCNTS/16/,CNTS/50.,100.,200.,300.,400.,600.,800.,
34* 11000.,1200.,1400.,1600.,1800.,2000.,2200.,2400.,2600./
35* DATA NCRV/1/
36* DATA X/300000.,305000.,310000.,315000.,320000.,325000.,330000.,
37* 1335000.,340000.,345000.,350000.,355000.,360000.,365000.,370000.,
38* 2375000.,380000.,385000.,390000.,395000.,400000.,405000.,410000.,

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39*      3415000.,420000.,425000.,430000.,435000.,440000.,445000.,450000./
40*      DATA Y/3520000.,3525000.,3530000.,3535000.,3540000.,3545000.,
41*      13550000.,3555000.,3560000.,3565000.,3570000.,3575000.,3580000.,
42*      23585000.,3590000.,3595000.,3600000.,3605000.,3610000.,3615000.,
43*      33620000.,3625000.,3630000.,3635000.,3640000.,3645000.,3650000.,
44*      43655000.,3660000.,3665000.,3670000./
45*      DATA XST/5*0.0./YST/5*0.0/
46*      DATA RUNID/10* , /
47*      DATA IULBL/,'CONCENTRATION ISOPLETHS','DOSAGE ISOPLETHS', , /
48*      CISO(A,B) = SQRT(A*ALOG(B))
49*      NAMELIST /OLST3/ ISW,XST,YST,CONT,NCONT,CONTS,NCONTS,
50*      1SCL,CN1SS,DS1SS
51*      IF (TYPE3.EQ. 0) GO TO 1020
52*      READ (XINFIL,OLST3)
53*      DO 1000 NCRV = 1,5
54*      IF (XST(NCRV) .LE. 0.0) GO TO 1010
55*      1000 CONTINUE
56*      NCRV = 6
57*      1010 NCRV = NCRV-1
58*      1020 IF (NCRV .GT. 0) GO TO 1030
59*      NCRV = 1
60*      1030 CONTINUE
61*      IF (ISW(11) .LT. 0) NCRV = -NCRV
62*      IF (ISW(11) .EQ. 0) NCRV = 0
63*      IOF = 0
64*      IST = 6
65*      JST = 6
66*      IND = IDP-5
67*      JND = JDP-5
68*      NX = IND-JST+1
69*      NY = JND-JST+1
70*      INTO = IDP*JDP
71*      IDIM = IDP
72*      JDIM = JDP
73*      NPLOT = ISW(3)+ISW(5)+ISW(8)+IABS(ISW(9))+IABS(ISW(10))+IABS(ISW(11))
74*      1))
75*      IPLOT = NPLOT+ISW(2)
76*      IF (NPLOT .EQ. 0) GO TO 1900

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77*      1300 CONTINUE
78*      JNTO = INTO*3+68
79*      LSW = 0
80*      1400 CONTINUE
81*      IOF = IOF+1
82*      CALL BLKIN(JNTO,NETRAL,IOF,SPARE,ISTS)
83*      IF (NETRAD .LT. 0) GO TO 1700
84*      CALL BLKIN(INTO,H,1,WSTRN,ISTS)
85*      E1 = TIM*1.6666666E-2
86*      IHOURS = IHOUR*100+MINUTE
87*      ENCODE (60,2001,RUNID,J) JULIAN,IMONTH,IDAY,IHOURS,NCNTO,E1
88*      MFLGS = 0
89*      IF (XST(1) .LE. 0.0) XST(1) = XSOURC
90*      IF (YST(1) .LE. 0.0) YST(1) = YSOURC
91*      IF (ISW(1) .EQ. 0) GO TO 1520
92*      IF (ISW(1) .LT. 0.AND.LSW .EQ. 0) GO TO 1520
93*      IF (ISW(1) .GT. 0.AND.LSW .EQ. 1) GO TO 1520
94*      E9 = TIM*.27777777E-3
95*      DO 1510 J=JST,JND
96*      LINES = 60
97*      DO 1510 I=IST,IND
98*      E1 = 1.0/P(I,J)
99*      E2 = M(I,J)*E1
100*      E3 = N(I,J)*E1
101*      E1 = P(I,J)+H(I,J)
102*      E4 = H(I,J)
103*      J3 = 1
104*      1485 LINES = LINES+1
105*      IF (LINES .LT. 57) GO TO 1501
106*      LINES = 7
107*      WRITE (XOIFIL,2002) JULIAN,IMONTH,IDAY,IHOURS,IIL(J3),ITL(J3+1),
108*      1NN,E9
109*      J4 = J3+3
110*      IF (IABS(ISW(1)).EQ. 2) GO TO 1500
111*      WRITE (XOIFIL,2003) (ITL(J5),J5=J3,J4)
112*      GO TO 1502
113*      1500 WRITE (XOIFIL,2004) (ITL(J5),J5=J3,J4)
114*      1501 IF (IABS(ISW(1)).EQ. 1) GO TO 1502

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PLT07700  
 PLT07800  
 PLT07900  
 PLT08000  
 PLT08100  
 PLT08200  
 PLT08300  
 PLT08400  
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 PLT08700  
 PLT08800  
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 PLT09000  
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 PLT09900  
 PLT10000  
 PLT10100  
 PLT10200  
 PLT10300  
 PLT10400  
 PLT10500  
 PLT10600  
 PLT10700  
 PLT10800  
 PLT10900  
 PLT11000  
 PLT11100  
 PLT11200  
 PLT11300  
 PLT11400



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115*      CALL HEC003(E2,E3)
116*      J4 = I-IST+1
117*      J5 = J-JST+1
118*      WRITE (X0IFIL,2005) J4,J5,X(J4),Y(J5),E2,E3,E1,E4
119*      CONTINUE
120*      LINES = 60
121*      CONTINUE
122*      IF (ISW(8) .EQ. 0) GO TO 1600
123*      C      PLOT TERRAIN CONTOURS
124*      ISW(8) = 0
125*      CALL HEC004(X(1),X(NX),Y(1),Y(NY),1)
126*      CALL HEC005(X(1),Y(1),M,H,P,0,N)
127*      CALL HEC015(U,0,0)
128*      1600 IF (ISW(9) .EQ. 0) GO TO 1620
129*      IF (ISW(9) .LT. 0.AND.LSW .EQ. 0) GO TO 1620
130*      IF (ISW(9) .GT. 0.AND.LSW .EQ. 1) GO TO 1620
131*      C      PLOT TERRAIN CONTOURS FOR VECTORS
132*      CALL HEC004(X(1),X(NX),Y(1),Y(NY),2)
133*      IF (IABS(ISW(9)) .EQ. 2) GO TO 1610
134*      CALL HEC005(X(1),Y(1),M,H,P,0,N)
135*      MFLGS = MFLGS+1
136*      1610 CONTINUE
137*      C      PLOT VECTORS AND TRAJECTORIES
138*      CALL BLKIN(JNTO,NL,TRAD,IOF,SPARE,ISTS)
139*      J2 = 0
140*      DO 1615 J=JST,JND
141*      J2 = J2+1
142*      J1 = (J2-1)*NX
143*      DO 1615 I=IST,IND
144*      J1 = J1+1
145*      E1 = 1.0/P(I,J)
146*      UM(J1) = M(I,J)*E1
147*      SPACE(J1) = P(I,J)
148*      AREA(J1) = N(I,J)*E1
149*      1615 CONTINUE
150*      CALL HEC006(X(1),Y(1),UM,AREA,NX,NY,SPACE,XMIN)
151*      MFLGS = MFLGS+1
152*      IF (IABS(ISW(10)) .EQ. 1) GO TO 1620

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PLT11500
PLT11600
PLT11700
PLT11800
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PLT12600
PLT12700
PLT12800
PLT12900
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PLT13900
PLT14000
PLT14100
PLT14200
PLT14300
PLT14400
PLT14500
PLT14600
PLT14700
PLT14800
PLT14900
PLT15000
PLT15100
PLT15200

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153*      CALL HEC015(0,XM)
154*      IF (ISW(10) .EQ. 0) GO TO 1640
155*      IF (IABS(ISW(10)) .EQ. 2) GO TO 1624
156*      ISW(10) = 1 OR -1
157*      IF (ISW(9) .LT. 0 .AND. LSW .EQ. 0) GO TO 1640
158*      IF (ISW(9) .GT. 0 .AND. LSW .EQ. 1) GO TO 1640
159*      GO TO 1625
160*      IF (ISW(10) .LT. 0 .AND. LSW .EQ. 0) GO TO 1640
161*      IF (ISW(10) .GT. 0 .AND. LSW .EQ. 1) GO TO 1640
162*      CONTINUE
163*      C
164*      PLOT LAYER DEPTH OR HEIGHT
165*      CALL BLKIN(INTO,H,1,WSIRRN,ISTS)
166*      CALL PLKIN(JNTO,NETRAD,IOF,SPARE,ISTS)
167*      IF (IABS(ISW(10)) .EQ. 1) GO TO 1630
168*      CALL HEC004(X(1),X(NX),Y(1),Y(NY),3)
169*      IF (IABS(ISW(10)) .NE. 2) GO TO 1630
170*      CALL HEC005(X(1),Y(1),M,H,P,0,N)
171*      MFLGS = MFLGS+1
172*      CALL HEC005(X(1),Y(1),M,H,P,1,N)
173*      CALL HEC015(0,XM)
174*      CONTINUE
175*      GO TO 1400
176*      CONTINUE
177*      IF (LSW .EQ. 1) GO TO 1710
178*      LSW = 1
179*      IOF = IOF-2
180*      IF (ISW(1) .LT. 0 .OR. ISW(9) .LT. 0 .OR. ISW(10) .EQ. -2) GO TO 1400
181*      CONTINUE
182*      IN = IABS(NETRAD)
183*      IF (ISW(3) .EQ. 0) GO TO 1820
184*      C
185*      PLOT REL VAR OF MOMENTUM AND DEPTH VS. TIME
186*      E2 = 1.0E5
187*      DO 1810 J=1,2
188*      E1 = 0.0
189*      DO 1805 I=1,IN
190*      E1 = AMAX1(E1,VAR(I,J))
191*      DO 1806 I=1,IN
192*      VAR(I,J) = VAR(I,J)/E1
193*
194*      PLT15300
195*      PLT15400
196*      PLT15500
197*      PLT15600
198*      PLT15700
199*      PLT15800
200*      PLT15900
201*      PLT16000
202*      PLT16100
203*      PLT16200
204*      PLT16300
205*      PLT16400
206*      PLT16500
207*      PLT16600
208*      PLT16700
209*      PLT16800
210*      PLT16900
211*      PLT17000
212*      PLT17100
213*      PLT17200
214*      PLT17300
215*      PLT17400
216*      PLT17500
217*      PLT17600
218*      PLT17700
219*      PLT17800
220*      PLT17900
221*      PLT18000
222*      PLT18100
223*      PLT18200
224*      PLT18300
225*      PLT18400
226*      PLT18500
227*      PLT18600
228*      PLT18700
229*      PLT18800
230*      PLT18900
231*      PLT19000

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1800 E2 = AMIN1(E2,VAR(I,J))
1810 CONTINUE
      E1 = 1.0
      CALL HEC004(0.0,PLTM(IN),E2,E1,4)
      CALL HEC007(PLTM,VAR,IN,1,E2)
      CALL HEC015(0,XM)
1820 CONTINUE
      IF (ISW(5) .EQ. 0) GO TO 1900
      E2 = 1.0E5
      DO 1850 J=1,2
        E1 = 0.0
        DO 1830 I=1,IN
          E1 = AMAX1(E1,VOL(I,J))
          DO 1840 I=1,IN
            VOL(I,J) = VOL(I,J)/E1
          VOL(I,J) = AMIN1(E2,VOL(I,J))
        1850 CONTINUE
        E1 = 1.0
        CALL HEC004(0.0,PLTM(IN),E2,E1,5)
        CALL HEC007(PLTM,VOL,IN,2,E2)
        CALL HEC015(0,XM)
1900 CONTINUE
2000 FORMAT ('1=',E11.6,'', 2=',E11.6,'', 3=',E11.6)
2001 FORMAT ('WSMR - JUL/M/D/H=',I3,'/',I2,'/',I2,'/',I4,'2, STEP ',I3,PLT1400
1', TIME ',F7.2,' MIN')
2002 FORMAT ('1',39X,'*-* SOLUTION FOR WSMR - JUL/M/D/H=',I3,'/',I2,'/',I2,'/',I3,PLT1600
1,12,'/',I4,'2 *-* /25X,'** WIND FIELD, LAYER HEIGHT, AND ',A6,A5,PLT1700
2 AT TIME STEP ',I4,' (',F7.2,' HOURS) *')
2003 FORMAT (5X,'X INDEX Y INDEX X COORDINATE Y COORDINATE U COMP,PLT1900
1ONENT V COMPONENT LAYER HEIGHT ',A6,A5/8X,'I',8X,'J',8X,'(PLT22000
2METERS) (METERS) (METERS/SEC) (METERS/SEC) (METERS/SEC)
37X,A6,A4/1X,64('---'))
2004 FORMAT (5X,'X INDEX Y INDEX X COORDINATE Y COORDINATE WIND SPLT22300
1PEED DIRECTION LAYER HEIGHT ',A6,A5/8X,'I',8X,'J',8X,'(PLT22400
2METERS) (METERS) (METERS/SEC) (DEGREES)
37X,A6,A4/1X,64('---'))
2005 FORMAT (1X,219,3X,2F14.3,2F14.6,2F16.6)
      IF (ISW(2) .EQ. 0) GO TO 2090

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MFLGS = 0
CALL BLKIN(INTO,H,1,WSTRN,ISTS)
CALL BLKIN(4090,NETRAU,1,TRDFFL,ISTS)
IHOURLS = IHOURL*100+MINUTE
IF (KINDSO .EQ. 0) GO TO 9001
I = 3
IF (KINDSO .EQ. 1) I = 1
IF (KINDSO .EQ. 2) I = 2
ENCODE (60,9000,RUNID,J) JULIAN,IMONTH,IDAY,IHOURLS,(INTIM(K),K=1,4),
1,INTIN(1)
9000 FORMAT ('*SMR- JUL/M/L/H=' ,13,'/',12,'/',14,'Z', ' ,3A6,A3,A6)
1)
GO TO 9002
9001 ENCODE (60,9000,RUNID,J) JULIAN,IMONTH,IDAY,IHOURLS,(INTIM(K),K=1,4)
1,INTIN(3)
9002 CONTINUE
CALL HEC004(X(1),X(NX),Y(1),Y(NY),2)
CALL HEC005(X(1),Y(1),M,H,P,0,N)
XD = (X(NX)-X(1))*SCL*0.5
CALL BLKIN(4090,NETRAU,1,TRDFFL,ISTS)
IF (CNISS(1) .LE. 0.0) GO TO 2010
DO 2006 L=1,3
2006 DCONC(L,1) = CUONC(L,1)
L = 0
2007 L = L+1
IF (L .GT. 3.OR.CNISS(L) .LE. 0.0) GO TO 2010
DO 2009 I=1,NETRAU
SIGY = 2.0*SIGMY(1)*SIGMY(I)
A = CHIT(I)/CNISS(L)
IF (A .LE. 1.0) GO TO 2008
YCHIT(I,L) = CISO(SIGY,A)
GO TO 2009
2008 YCHIT(I,L) = 0.0
2009 CONTINUE
GO TO 2007
2010 IF (KINDSO .NE. 0.OR.DSISS(1) .LE. 0.0) GO TO 2015
DO 2011 L=1,3
2011 DCONC(L,2) = CDONC(L,2)
  
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 PLT23000  
 PLT23100  
 PLT23200  
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 PLT24900  
 PLT25000  
 PLT25100  
 PLT25200  
 PLT25300  
 PLT25400  
 PLT25500  
 PLT25600  
 PLT25700  
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L = 0
2012 L = L+1
      IF (L.GT. 3.OR.DSISS(L) .LE. 0.0) GO TO 2015
      DO 2014 I=1,NETRAD
        SIGY = 2.0*SIGMY(I)*SIGMY(I)
        A = DOST(I)/DSISS(L)
        IF (A .LE. 1.0) GO TO 2013
        YDOST(I,L) = CISO(SIGY,A)
        GO TO 2014
      2013 YDOST(I,L) = 0.0
2014 CONTINUE
      GO TO 2012
2015 CONTINUE
      K1 = 2
      IF (KINDSO .NE. 0) K1 = 1
      E3 = 0.05/SCL
      DO 2060 K=1,K1
        MFLGS = MFLGS+1
        CALL HEC016(MFLGS)
        IF (NETRAD .LE. 0) GO TO 2080
        Y1 = -0.9
        X1 = 0.5*(XD+1.5)+XD-FLOAT(K-1)*4.1
        CALL HEC014(X1,Y1,.075,IDLBL(1,K),0.0,23)
        LIST ISOPLETH LEVELS
        ENCODE (43,2000,ZELEVVR,J) (DCONC(L,K),L=1,3)
        X1 = 0.5*(XD+.275)+XD-FLOAT(K-1)*4.125
        CALL HEC014(X1,Y1-.1,.075,ZELEVVR,0.0,43)
        DO 2017 L=1,3
          DO 2016 I=1,NETRAD
            IF (COND(I,L,K) .GT. 0.0) GO TO 2016
            IF (I-1.GT. 0.AND.COND(I-1,L,K) .GT. 0.0) GO TO 2016
            IF (I+1.LE. NETRAD.AND.COND(I+1,L,K) .GT. 0.0) GO TO 2016
            COND(I,L,K) = -1.0
          2016 CONTINUE
        2017 CONTINUE
        T = -1.0
        DO 2070 J=1,2
          T = T*-1.0

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PLT26700  
PLT26800  
PLT26900  
PLT27000  
PLT27100  
PLT27200  
PLT27300  
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PLT29000  
PLT29100  
PLT29200  
PLT29300  
PLT29400  
PLT29500  
PLT29600  
PLT29700  
PLT29800  
PLT29900  
PLT30000  
PLT30100  
PLT30200  
PLT30300  
PLT30400

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B-121

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DO 2060 L=1,3
IF (UCONC(L,K) .LE. 0.0) GO TO 2070
XLST = XSOURC
YLST = YSOURC
LS = 3
I1 = 0
2010 I1 = I1+1
IF (COND(I1,L,K) .LE. 0.0) GO TO 2018
I1 = I1-1
IF (I1 .LT. 1) I1 = 1
I2 = NETRAD+1
2019 I2 = I2-1
IF (COND(I2,L,K) .LE. 0.0) GO TO 2019
I2 = I2+1
IF (I2 .GT. NETRAD) I2 = NETRAD
IF (I2 .LE. I1) GO TO 2060
DO 2050 I=I1,I2
A1 = AX(I)-XLST
A2 = YY(I)-YLST
IF (A1) 2029,2028,2029
2028 IF (A2) 2029,2030,2029
2029 A2 = ATAN2(A2,A1)
2030 A1 = A2-1.5707963
E1 = COS(A1)*I
E2 = SIN(A1)*I
XP = COND(I,L,K)
YP = COND(I,L,K)
IF (COND(I,L,K) .GE. 0.0) GO TO 2032
XP = 0.0
YP = 0.0
2032 XP = (XX(I)-X(I)+XP*E1)*SCL
YP = (YY(I)-Y(I)+YP*E2)*SCL
XLST = XX(I)
YLST = YY(I)
IF (COND(I,L,K) .LT. 0.0) GO TO 2040
IF (XP .LT. 0.0.OR.XP .GT. XNCH) GO TO 2040
IF (YP .LT. 0.0.OR.YP .GT. YNCH) GO TO 2040
CALL PLOT(XP,YP,LS)

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PLT30500  
PLT30600  
PLT30700  
PLT30800  
PLT30900  
PLT31000  
PLT31100  
PLT31200  
PLT31300  
PLT31400  
PLT31500  
PLT31600  
PLT31700  
PLT31800  
PLT31900  
PLT32000  
PLT32100  
PLT32200  
PLT32300  
PLT32400  
PLT32500  
PLT32600  
PLT32700  
PLT32800  
PLT32900  
PLT33000  
PLT33100  
PLT33200  
PLT33300  
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LS = 2
IF (MOD(I,40) .NE. 0) GO TO 2050
E1 = (XX(I)-X(1))+(CONU(I,L,K)+E3)*E1)*SCL
E2 = (YY(I)-Y(1))+(CONU(I,L,K)+E3)*E2)*SCL
A1 = L
CALL NUMBER(E1,E2,.05,A1,0.0,-1)
CALL PLOT(XP,YP,3)
GO TO 2050
2040 LS = 3
2050 CONTINUE
2060 CONTINUE
2070 CONTINUE
2080 CONTINUE
CALL HEC015(0,XM)
2090 IF (IPLOT .NE. 0) CALL HEC015(1,XMIN)
3000 CONTINUE
IF (IPLOT .NE. 0) WRITE (XOTFIL,3001)
3001 FORMAT ('0 PLOT SECTION COMPLETED')
RETURN
END

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PLT34300  
 PLT34400  
 PLT34500  
 PLT34600  
 PLT34700  
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 PLT35700  
 PLT35800  
 PLT35900  
 PLT36000  
 PLT36100  
 PLT36200

```

1* SUBROUTINE BLKIN (NWDBLK, ISTART, NBKIN, LSFILE, ISTAT)
2* DISK VERSION, BLOCK TRANSFER FROM RANDOM ACCESS DISK FILE TO CORE. BIN00100
3* BLKIN TRANSFERS TO CORE A BLOCK FROM A RANDOM ACCESS FILE THAT BIN00200
4* CONTAINS BLOCKS THAT ARE ALL OF THE SAME SIZE. BIN00300
5* NWDBLK = NO. OF WORDS PER BLOCK IN THE FILE AND THE NO. OF WORDS TO BE BIN00400
6* TRANSFERRED TO CORE ON THIS CALL. BIN00500
7* ISTART = STARTING ADDRESS IN CORE WHERE THE BLOCK IS TO BE TRANSFERRED BIN00600
8* IO. BIN00700
9* NBKIN = NO. OF THIS BLOCK IN THE FILE. NBKIN = 1 IS THE FIRST BLOCK BIN00800
10* NO. IN THE FILE. BIN00900
11* LSFILE = LOGICAL SYSTEM FILE NO. (0-15). BIN01000
12* ISTAT = STATUS RETURNED TO USER. ISTAT = 0 INDICATES NO ERRORS. BIN01100
13* ISTAT = 1 INDICATES AN ERROR OF SOME KIND. BIN01200
14* BIN01300
15* BIN01400
16* BIN01500
17* BIN01600
18* BIN01700
19* BIN01800
20* THE STATUS ISTAT RETURNED TO THE USER WILL ALWAYS BE ZERO SINCE THE BIN01900
21* FSTRD ROUTINE DOES NOT RETURN ANY STATUS INFORMATION. FSTRD HAS IT'S BIN02000
22* OWN ERROR MESSAGES. BIN02100
23* NSECPB=(NWDBLK+27)/28 BIN02200
24* NBKML=NBKIN-1 BIN02300
25* CALL FSTRD (NWDBLK, ISTART, NSECPB, NBKML, 0, LSFILE) BIN02400
26* ISTAT=0 BIN02500
27* RETURN BIN02600
28* END BIN02700

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```

1* SUBROUTINE BLKOUT (NWDBLK, ISTART, NBKOUT, LSFILE, ISTAT) BOT00100
2* DISK VERSION. BLOCK TRANSFER FROM CORE TO RANDOM ACCESS DISK FILE. BOT00200
3* BLKOUT TRANSFERS A BLOCK FROM CORE TO A RANDOM ACCESS FILE WHICH BOT00300
4* CONTAINS BLOCKS THAT ARE ALL OF THE SAME SIZE. BOT00400
5* NWDBLK = NO. OF WORDS PER BLOCK IN THE FILE AND THE NO. OF WORDS TO BE BOT00500
6* TRANSFERRED FROM CORE ON THIS CALL. BOT00600
7* ISTART = STARTING ADDRESS IN CORE WHERE THE BLOCK IS TO BE TRANSFERRED BOT00700
8* FROM. BOT00800
9* NBKOUT = NO. OF THIS BLOCK IN THE FILE. NBKOUT = 1 IS THE FIRST BLOCK BOT00900
10* NO. IN THE FILE. BOT01000
11* LSFILE = LOGICAL SYSTEM FILE NO. (0-15). BOT01100
12* ISTAT = STATUS RETURNED TO USER. ISTAT = 0 INDICATES NO ERRORS. BOT01200
13* ISTAT = 1 INDICATES AN ERROR OF SOME KIND. BOT01300
14* BOT01400
15* BOT01500
16* BOT01600
17* BOT01700
18* BOT01800
19* BOT01900
20* THE STATUS ISTAT RETURNED TO THE USER WILL ALWAYS BE ZERO SINCE THE BOT02000
21* FSTWT ROUTINE DOES NOT RETURN ANY STATUS INFORMATION. FSTWT HAS IT'S BOT02100
22* OWN ERROR MESSAGES. BOT02200
23* ISECPB=(NWDBLK+27)/28 BOT02300
24* NBKML=NBKOUT-1 BOT02400
25* CALL FSTWT (NWDBLK, ISTART, NSECPB, NBKML, 0, LSFILE) BOT02500
26* ISTAT=0 BOT02600
27* RETURN BOT02700
28* END BOT02800

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H0300100  
H0300200  
H0300300  
H0300400  
H0300500  
H0300600  
H0300700  
H0300800  
H0300900  
H0301000  
H0301100  
H0301200  
H0301300  
H0301400

SUBROUTINE HEC003(X,Y)  
THIS SUBROUTINE CONVERTS THE U AND V COMPONENTS (X AND Y) OF THE  
WIND SPEED INTO WIND SPEED AND DIRECTION (X AND Y)  
DATA RAD/57.29582/  
IF (X) 20,10,20  
10 IF (Y) 20,30,20  
20 CONTINUE  
DIR = 270.0-ATAN2(Y,X)\*RAD  
IF (DIR .GE. 360.0) DIR = DIR-360.0  
X = SQRT(X\*X+Y\*Y)  
Y = DIR  
30 CONTINUE  
RETURN  
END

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1* SUBROUTINE HEC004(XMN, XMX, YMN, YMX, JSW)
2* INCLUDE N1,L1ST
3* COMMON /DTA1/ J1,J2,J3,J4,J5,J6,J7,J8,J9,J10,J11,J12,J13,RAD,MAXLL
4* 1,XM,YM,MFLGS,SCLX,SCLY,XNCH,YNCH,J14,J15,J16,ISW7,IPL0T,MCORE
5* COMMON/BS/LBL1(5),LBL2(7),LBL3(7),LBL6(5),LBL9(2),LBL4(4),LBL5(3)
6* EQUIVALENCE (J3,DX),(J4,DY),(J5,J),(J6,NCH),(J7,YPL),(J8,XPL),
7* 1(J9,TIC),(J10,IB),(J11,X),(J12,Y)
8* INTEGER BLNK,RUNID
9* DATA BLNK/,/,/
10* DATA LBL1,'DISTANCE (M) (SOUTH-NORTH)',/
11* DATA LBL2,'NORMALIZED REL VAR OF CHANGE IN MOMENTUM',/
12* DATA LBL3,'NORMALIZED REL VAR OF CHANGE IN DEPTH',/
13* DATA LBL4,'NORMALIZED MOMENTUM',/
14* DATA LBL5,'NORMALIZED VOLUME',/
15* DATA LBL6,'DISTANCE (M) (WEST-EAST)',/
16* DATA LBL9,'TIME (SEC)',/
17* THIS SUBROUTINE DRAWS AND LABELS THE PLOT AXES
18* IF (JSW .GE. 4) GO TO 10
19* DX = 1000.
20* DY = 1000.
21* J1 = -1
22* J2 = -1
23* XNCH = SCL*(XMX-XMN)
24* YNCH = SCL*(YMX-YNM)
25* SCLX = SCL
26* SCLY = SCL
27* GO TO 20
28* 10 DX = (XMX-XMN)/50.0
29* DY = (YMX-YNM)/50.0
30* J1 = 2
31* XNCH = 10.0
32* YNCH = 7.0
33* SCLX = XNCH/(XMX-XMN)
34* SCLY = YNCH/(YMX-YNM)
35* J2 = 6
36* 20 CONTINUE
37* XM = XNCH+2.0
38* YM = YNCH+2.0

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IF (XM .GT. 33.0) XM = 33.0
IF (YM .GT. 33.0) YM = 33.0
IF (XNCH .GT. 31.0) XNCH = 31.0
IF (YNCH .GT. 31.0) YNCH = 31.0
CALL HEC013(XM,YM,15W(20))
CALL PLOT(0.0,0.0,3)
CALL PLOT(0.0,YNCH,2)
CALL PLOT(XNCH,YNCH,2)
CALL PLOT(XNCH,0.0,2)
CALL PLOT(0.0,0.0,2)
YPL = 0.0
TIC = 1.0
DO 70 J=1,2
  IB = 9
  X = XMN-DX
  40 X = X+DX
  IB = IB+1
  XPL = (X-XMN)*SCLX
  IF (XPL .LT. XNCH) GO TO 50
  XPL = XNCH
  50 CALL PLOT(XPL,YPL,3)
  IF (IB .LT. 10) GO TO 60
  IB = 0
  CALL PLOT(XPL,YPL+.1*TIC,2)
  IF (J .EQ. 2) GO TO 61
  CALL NUMBER(XPL-.225,YPL-.1,.075,X,0.0,J1)
  GO TO 61
  60 CALL PLOT(XPL,YPL+.05*TIC,2)
  61 IF (XPL .LT. XNCH) GO TO 40
  YPL = YNCH
  TIC = -1.0
  70 CONTINUE
  XPL = 0.0
  TIC = 1.0
  DO 110 J=1,2
    IB = 9
    Y = YMN-DY
    80 Y = Y+DY

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H0403900  
H0404000  
H0404100  
H0404200  
H0404300  
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      IB = IB+1
      YPL = (Y-YNM)*SCLY
      IF (YPL.LT. YNCH) GO TO 90
      YPL = YNCH
90    CALL PLOT(XPL,YPL,3)
      IF (IB.LT. 10) GO TO 100
      IB = 0
      CALL PLOT(XPL+.1*TIC,YPL,2)
      IF (J.EQ. 2) GO TO 101
      CALL NUMBER(XPL-.1,YPL-.23,.075,Y,90.0,J2)
      GO TO 101
100   CALL PLOT(XPL+.05*TIC,YPL,2)
101   IF (YPL.LT. YNCH) GO TO 80
      XPL = XNCH
      TIC = -1.0
110   CONTINUE
C
      LABEL AXES
      IF (JSW.GE. 4) GO TO 130
      X = -.3
      Y = 0.5*(YNCH-2.7)
      CALL HEC014(X,Y,.1,LBL1,90.0,27)
      X = 0.5*(XNCH-2.5)
      Y = -.3
      CALL HEC014(X,Y,.1,LBL6,0.0,25)
      GO TO 140
130   X = 0.5*(XNCH-1.0)
      Y = -.3
      CALL HEC014(X,Y,.1,LBL9,0.0,10)
140   NCH = 66
150   J = 11
      NCH = NCH-6
      J = J-1
      IF (J.EQ. 0) GO TO 160
      IF (RUNID(J).EQ. BLNK) GO TO 150
      X = 0.5*(XNCH-0.1*FLOAT(NCH))
      Y = -.7
      CALL HEC014(X,Y,.1,RUNID,0.0,NCH)
160   CONTINUE

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H0407700  
H0407800  
H0407900  
H0408000  
H0408100  
H0408200  
H0408300  
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H0411200  
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H0411400

H0411500  
H0411600  
H0411700  
H0411800  
H0411900

XN = XNCH+2.0  
YN = YNCH+2.0  
MFLGS = 0  
RETURN  
END

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1* 2* 3* 4* 5* 6* 7* 8* 9* 10* 11* 12* 13* 14* 15* 16* 17* 18* 19* 20* 21* 22* 23* 24* 25* 26* 27* 28* 29* 30* 31* 32* 33* 34* 35* 36* 37* 38*
COMPILER (XM=1)
SUBROUTINE HEC005(X,Y,Z,H,P,JSW,W)
INCLUDE N1,LIST
COMMON /DIAL/ J1,J2,J3,J4,J5,J6,J7,J8,J9,J10,J11,J12,J13,RAD,MAXLL
1,XM,YM,MFLGS,SCLX,SCLY,XNCH,YNCH,J14,J15,J16,ISW7,IPLOT,MORE
DIMENSION X(1),Y(1),Z(1),H(IDIM,1),P(IDIM,1)
DIMENSION W(1)
C THIS SUBROUTINE SETS UP ARRAYS FOR CONTOUR PLOTTING
J6 = IND
J8 = J6-IST+1
10 IF ((X(J8)-X(1))*SCL.LE.XNCH) GO TO 20
J8 = J8-1
J6 = J6-1
IF (J6.LE. IST) GO TO 80
GO TO 10
20 J7 = JND
J9 = J7-JST+1
30 IF ((Y(J9)-Y(1))*SCL.LE.YNCH) GO TO 40
J9 = J9-1
J7 = J7-1
IF (J7.LE. JST) GO TO 80
GO TO 30
40 IF (JSW.NE. 0) GO TO 60
J2 = 0
DO 50 J=JST,J7
J2 = J2+1
J1 = (J2-1)*J8
DO 50 I=IST,J6
J1 = J1+1
Z(J1) = H(I,J)
50 CONTINUE
CALL HEC009(X,Y,Z,J8,J9,CONT,NCONT,SCL,W,0,W(J8*J9+1),Z(J8*J9+1))
GO TO 80
60 CONTINUE
J2 = 0
DO 70 J=JST,J7
J2 = J2+1
J1 = (J2-1)*J8

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H0503900  
 H0504000  
 H0504100  
 H0504200  
 H0504300  
 H0504400  
 H0504500  
 H0504600  
 H0504700  
 H0504800  
 H0504900  
 H0505000

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00 70 I=IST,Jo
J1 = J1+1
A = 0.0
IF (ISW(7) .NE. 0) A = H(I,J)
Z(J1) = P(I,J)+A
70 CONTINUE
IF (MFLGS .NE. 0) CALL HEC016(MFLGS)
CALL HEC009(X,Y,Z,J8,J9,CONTS,NCONTS,SCL,K,ISW(10),W(J8*J9+1),Z(J8H0504600
1*J9+1))
60 CONTINUE
RETURN
END
  
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```

1* SUBROUTINE HEC006(X,Y,U,V,NX,NY,P,XMIN)
2* INCLUDE N1,LIST
3* THIS SUBROUTINE DRAWS VECTORS AT EACH GRID COORDINATE
4* COMMON /DIA1/ J1,J2,J3,J4,J5,J6,J7,J8,J9,J10,J11,J12,J13,RAD,MAXLL
5* 1,XM,YM,MFLGS,SCLX,SCLY,XNCH,YNCH,J14,J15,J16,ISW7,IPLUT,MCORE
6* DIMENSION X(1),Y(1),U(NX,1),V(NX,1),XV(3),YV(3)
7* EQUIVALENCE (J1,RSCL),(J2,PSCL),(J3,YP),(J4,XP),(J5,X1),(J6,Y1),
8* 1(J7,XV),(J10,YV),(J13,X2),(J14,Y2)
9* IF (MFLGS.NE. 0) CALL HEC016(MFLGS)
10* CALC MAX VELOCITY
11* UVMAX = 0.0
12* DO 20 J=1,NY
13* DO 20 I=1,NX
14* 20 UVMAX = AMAX1(UVMAX,U(I,J)*U(I,J)+V(I,J)*V(I,J))
15* UVMAX = SQRT(UVMAX)
16* CALC VECTOR SCALE FACTOR IN INCHES PER METER/SEC
17* RSCL = .80*SCL*XM/N/UVMAX
18* PLOT VECTOR SCALE 1 INCH = PSCL M/S
19* PSCL = 1.0/RSCL
20* CALC AND DRAW VECTORS
21* DO 60 J=1,NY
22* YP = (Y(J)-Y(1))*SCL
23* DO 60 I=1,NX
24* XP = (X(I)-X(1))*SCL
25* X1 = U(I,J)*RSCL
26* Y1 = V(I,J)*RSCL
27* X2 = X1
28* Y2 = Y1
29* CALL HEC003(X2,Y2)
30* IF (X2.LE. 0.0) GO TO 60
31* Y2 = (Y2+180.)*RAD
32* X2 = COS(Y2)
33* Y2 = SIN(Y2)
34* YV(1) = SQRT(X1*X1+Y1*Y1)
35* XV(1) = 0.
36* YV(2) = YV(1)*.05
37* XV(2) = .025
38* YV(3) = YV(2)

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XV(3) = -XV(2)
DO 50 K=1,3
  X1 = YV(K)*Y2-XV(K)*X2
  Y1 = XV(K)*Y2+YV(K)*X2
  XV(K) = X1
  YV(K) = Y1
  50 CALL PLOT(XP,YP,3)
  CALL PLOT(XP+XV(1),YP+YV(1),2)
  CALL PLOT(XP+XV(2),YP+YV(2),3)
  CALL PLOT(XP+XV(1),YP+YV(1),2)
  CALL PLOT(XP+XV(3),YP+YV(3),2)
  60 CONTINUE
  CALL HEC014(0.0,-0.5,.075,22H(VECTOR SCALE 1 INCH =,0.0,22)
  CALL NUMBER(1.65,-0.5,.075,PSCL,0.0,4)
  CALL HEC014(2.175,-0.5,.075,5H M/S),0.0,5)
  CALL HEC014(0.0,-0.7,.075,15H(MAX VELOCITY =,0.0,15)
  CALL NUMBER(1.2,-0.7,.075,UVMAX,0.0,3)
  CALL HEC014(1.8,-0.7,.075,6HM/SEC),0.0,6)
  IF (NCRV.EQ. 0) GO TO 70
  CALL HEC008(U,V,X,Y,NX,NY,UVMAX,XMIN,NCRV,XST,YST,IEVEN,P)
  70 CONTINUE
  RETURN
  END

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H0603900  
 H0604000  
 H0604100  
 H0604200  
 H0604300  
 H0604400  
 H0604500  
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 H0604700  
 H0604800  
 H0604900  
 H0605000  
 H0605100  
 H0605200  
 H0605300  
 H0605400  
 H0605500  
 H0605600  
 H0605700  
 H0605800  
 H0605900  
 H0606000  
 H0606100

```

1* SUBROUTINE HEC007(TIME,VARVOL,L,K,YMIN)
2* DIMENSION TIME(1),VARVOL(200,1)
3* COMMON/BS/LBL1(5),LBL2(7),LBL3(7),LBL4(5),LBL5(3),LBL6(4),LBL7(3)
4* COMMON/DIA1/J1,J2,J3,J4,J5,J6,J7,J8,J9,J10,J11,J12,J13,RAD,MAXLL
5* 1,XM,YM,MFLGS,SCLX,SCLY,XNCH,YNCH,J14,J15,J16,ISW7,IPL0T,MCORE
6* EQUIVALENCE (J4,X),(J5,Y)
7* THIS SUBROUTINE PLOTS THE RELATIVE VARIANCE OF THE CHANGE IN
8* MOMENTUM VERSUS TIME, THE RELATIVE VARIANCE OF THE CHANGE IN DEPTH
9* VS. TIME, THE NORMALIZED MOMENTUM VS. TIME AND THE NORMALIZED
10* VOLUME VS. TIME.
11* DO 50 J=1,2
12* CALL PLOT(0.0,0.0,3)
13* IF (J.EQ. 2) CALL HEC016(1)
14* DO 10 I=1,L
15* X = TIME(I)*SCLX
16* Y = (VARVOL(I,J)-YMIN)*SCLY
17* CALL PLOT(X,Y,2)
18* IF (J.EQ. 2) GO TO 10
19* CALL PLOT(X,0.2,3)
20* CALL PLOT(X,0.4,2)
21* CALL PLOT(X,Y,3)
22* 10 CONTINUE
23* IF (J.EQ. 2) GO TO 30
24* X = -0.3
25* IF (K.EQ. 2) GO TO 20
26* Y = 0.5*(YNCH-4.0)
27* CALL HEC014(X,Y,1,LBL2,90.0,40)
28* GO TO 50
29* 20 Y = 0.5*(YNCH-1.9)
30* CALL HEC014(X,Y,1,LBL4,90.0,19)
31* GO TO 50
32* 30 X = -0.5
33* IF (K.EQ. 2) GO TO 40
34* Y = 0.5*(YNCH-3.7)
35* CALL HEC014(X,Y,1,LBL3,90.0,37)
36* GO TO 50
37* 40 Y = 0.5*(YNCH-1.7)
38* CALL HEC014(X,Y,1,LBL5,90.0,17)

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H0703900  
H0704000  
H0704100

50 CONTINUE  
RETURN  
END

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B-135



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1* SUBROUTINE HEC008(U,V,X,Y,NX,NY,UVMX,XMIN,MCRV,XST,YST,IEVEN,P)
2* INCLUDE FILES,LIST
3* DIMENSION U(NX,1),V(NX,1),X(1),Y(1),XST(1),YST(1),P(NX,1)
4* COMMON /DTA1/ J1,J2,J3,J4,J5,J6,J7,J8,J9,J10,J11,J12,J13,RAD,MAXLL
5* 1,XM,YM,MFLGS,SCLX,SCLY,XNCH,YNCH,J14,J15,J16,ISW7,IPL0T,NCORE
6* COMMON /M1/ S(124)
7* EQUIVALENCE (S(1),LINE),(S(2),DX),(S(3),T),(S(4),N2),(S(5),N),
8* 1(S(6),K2),(S(7),XP),(S(8),YP),(S(9),HXYM),(S(10),HXN),
9* 2(S(11),HX),(S(12),HY),(S(13),HX1),(S(14),HY1),(S(15),HX5),
10* 3(S(16),HY5),(S(17),HX21),(S(18),HY21),(S(19),HXY4),(S(20),N1),
11* 4(S(21),K1),(S(22),IB),(S(23),HM),(S(24),UT),(S(25),XO),
12* 5(S(26),YO),(S(27),PX),(S(28),K),(S(29),HXN),(S(30),HXN1),
13* 6(S(31),HYN),(S(32),HYN1),(S(33),NT),(S(34),X1),(S(35),Y1),
14* 7(S(36),PX1),(S(37),PY),(S(38),PY1),(S(39),UX1),(S(40),UX),
15* 8(S(41),UXA),(S(42),UY1),(S(43),UY),(S(44),UXY1),(S(45),UXY3),
16* 9(S(46),UXY),(S(47),VX1),(S(48),VX),(S(49),VXX),(S(50),VY1),
17* EQUIVALENCE (S(51),VY),(S(52),VYY),(S(53),VXY1),(S(54),VXY3),
18* 1(S(55),VXY),(S(56),UY),(S(57),AH),(S(58),AK),(S(59),UU),
19* 2(S(60),VV),(S(61),UU1),(S(62),VV1),(S(63),HMI),(S(64),XD),
20* 3(S(65),S1),(S(66),S2),(S(67),UUL),(S(68),VVL),(S(69),U1),
21* 4(S(70),U2),(S(71),V1),(S(72),V2)
22* THIS SUBROUTINE CALCULATES AND DRAWS ALL TRAJECTORIES.
23* MCRV = IABS(MCRV)
24* N2 = NX-1
25* K2 = NY-1
26* DX = 0.1*XMIN
27* UUL = UVMX
28* VVL = UVMX
29* XP = XI,CH-3.68
30* YP = -.5
31* CALL HEC014(XP,YP,.075,40H(DISTANCE BETWEEN TRAJECTORY TIC MARKS =
32* 1,0,0,40)
33* X1 = 5.0*DX
34* CALL NUMBER(XP+3,038,YP,.075,X1,0,0,-1)
35* CALL HEC014(XP+3,375,YP,.075,4H(M),0,0,4)
36* HXYM = XMIN
37* HAM = 0.05*HXYM
38* IF (IEVEN.EQ. 0) GO TO 40

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HX = X(2)-X(1)
HY = Y(2)-Y(1)
HX1 = 0.5/HX
HY1 = 0.5/HY
HXS = .5*HX
HYS = .5*HY
HX21 = 2.0*HX1*HX1
HY21 = 2.0*HY1*HY1
HXY4 = HX1*HY1
40 CONTINUE
DO 200 L=1,NCKV
U1 = 0.0
V1 = 0.0
U2 = 0.0
V2 = 0.0
XD = 0.0
DT = DX/(0.5*UVMX)
T = 0.0
N1 = 0
K1 = 0
IB = 0
X0 = XST(L)
Y0 = YST(L)
IF (X0.GT. X(NX).OR.X0.LT. X(1)) GO TO 200
IF (Y0.GT. Y(NY).OR.Y0.LT. Y(1)) GO TO 200
XP = (X0-X(1))*SCLX
YP = (Y0-Y(1))*SCLY
X1 = L
CALL NUMBER(XP+.05,YP,.075,X1,0.0,-1)
CALL PLOT(XP,YP+.02,3)
CALL PLOT(XP,YP,2)
CALL PLOT(XP+.01176,YP-.01618,2)
CALL PLOT(XP+.01902,YP+.0061803,3)
CALL PLOT(XP,YP,2)
CALL PLOT(XP-.01176,YP-.01618,2)
CALL PLOT(XP-.01902,YP+.0061803,3)
CALL PLOT(XP,YP,2)
60 IF (IEVEN.EQ. 0) GO TO 70

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H0804000  
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H0804200  
H0804300  
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H0810000  
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H0810200  
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H0810400  
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H0810800  
H0810900  
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H0811100  
H0811200  
H0811300  
H0811400

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77* N = INT((X0-X(1))*HX1*2,0)+1
78* IF (X0-X(N) .GT. HX5) N = N+1
79* IF (N .GE. NX) N = NX-1
80* IF (N .LE. 1) N = 2
81* K = INT((Y0-Y(1))*HY1*2,0)+1
82* IF (Y0-Y(K) .GT. HY5) K = K+1
83* IF (K .GE. NY) K=NY-1
84* IF (K .LE. 1) K = 2
85* GO TO 120
86* 70 IF (X0-1.0 .LT. X(1).OR.X0+1.0 .GT. X(NX)) GO TO 200
87* IF (Y0-1.0 .LT. Y(1).OR.Y0+1.0 .GT. Y(NY)) GO TO 200
88* N = 2
89* 80 IF (X0 .LT. X(N)) GO TO 90
90* N = N+1
91* GO TO 80
92* 90 IF (X(N)-X0 .GT. X0-X(N-1)) N = N-1
93* IF (N .LE. 1) N = 2
94* IF (N .GE. NX) N = NX-1
95* K = 2
96* 100 IF (Y0 .LT. Y(K)) GO TO 110
97* K = K+1
98* GO TO 100
99* 110 IF (Y(K)-Y0 .GT. Y0-Y(K-1)) K = K-1
100* IF (K .LE. 1) K = 2
101* IF (K .GE. NY) K = NY-1
102* HXN = X(N)-X(N-1)
103* HXN1 = X(N+1)-X(N)
104* HYN = Y(K)-Y(K-1)
105* HYN1 = Y(K+1)-Y(K)
106* 120 CONTINUE
107* C
108* CALC NEXT UU,VV
109* NT = 0
110* X1 = X0
111* Y1 = Y0
112* IF (N1 .EQ. N.AND.K1 .EQ. K) GO TO 140
113* N1 = N
114* K1 = K
IF (IEVEN .NE. 0) GO TO 130

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PX = 1.0/((HXN+HXN1)\*HXN)  
PX1 = 1.0/((HAN+HXN1)\*HXN1)  
PY = 1.0/((HYN+HYN1)\*HYN)  
PY1 = 1.0/((HYH+HYN1)\*HYN1)  
UX1 = PX1\*(U(N+1,K)-U(N,K))  
UX = PX\*(U(N,K)-U(N-1,K))  
UXX = 2.0\*(UX1-UX)  
UX = HXN\*UX1+HXN1\*UX  
UY1 = PY1\*(U(N,K+1)-U(N,K))  
UY = PY\*(U(N,K)-U(N,K-1))  
UYX = 2.0\*(UY1-UY)  
UY = HYN\*UY1+HYN1\*UY  
UXY1 = PX1\*HXN\*(U(N+1,K-1)-U(N,K-1))+PX\*HXN1\*(U(N,K-1)-U(N-1,K-1))  
UXY3 = PX1\*HXN\*(U(N+1,K+1)-U(N,K+1))+PX\*HXN1\*(U(N,K+1)-U(N-1,K+1))  
UXY = PY1\*HYN\*(UXY3-UX)+PY\*HYN1\*(UX-UXY1)  
VX1 = PX1\*(V(N+1,K)-V(N,K))  
VX = PX\*(V(N,K)-V(N-1,K))  
VXX = 2.0\*(VX1-VX)  
VX = HXN\*VX1+HXN1\*VX  
VY1 = PY1\*(V(N,K+1)-V(N,K))  
VY = PY\*(V(N,K)-V(N,K-1))  
VYX = 2.0\*(VY1-VY)  
VY = HYN\*VY1+HYN1\*VY  
VXY1 = PX1\*HXN\*(V(N+1,K-1)-V(N,K-1))+PX\*HXN1\*(V(N,K-1)-V(N-1,K-1))  
VXY3 = PX1\*HXN\*(V(N+1,K+1)-V(N,K+1))+PX\*HXN1\*(V(N,K+1)-V(N-1,K+1))  
VXY = PY1\*HYN\*(VXY3-VX)+PY\*HYN1\*(VX-VXY1)  
GO TO 140  
130 CONTINUE  
UX = (U(N+1,K)-U(N-1,K))\*HX1  
UY = (U(N,K+1)-U(N,K-1))\*HY1  
UXX = HX21\*(U(N-1,K)-U(N,K)-U(N,K)+U(N+1,K))  
UYX = HY21\*(U(N,K-1)-U(N,K)-U(N,K)+U(N,K+1))  
UXX = HXY4\*(U(N+1,K+1)-U(N-1,K-1)+U(N-1,K-1))  
VX = (V(N+1,K)-V(N-1,K))\*HX1  
VY = (V(N,K+1)-V(N,K-1))\*HY1  
VXX = HX21\*(V(N-1,K)-V(N,K)-V(N,K)+V(N+1,K))  
VYX = HY21\*(V(N,K-1)-V(N,K)-V(N,K)+V(N,K+1))  
VXY = HXY4\*(V(N+1,K+1)-V(N-1,K-1)+V(N-1,K-1))



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140 CONTINUE
  AH = X1-X(N)
  AK = Y1-Y(K)
  UU = U(N,K)+AH*UX+AK*UY+AH*AH*UXX+AH*AK*UXY+AK*AK*UY
  VV = V(N,K)+AH*VX+AK*VY+AH*AH*VXX+AH*AK*VXY+AK*AK*VY
  IF (NT .NE. 0) GO TO 150
  NT = 3
  X1 = X1+UU*DT
  Y1 = Y1+VV*DT
  UU = UU
  VV = VV
  GO TO 140
150 CONTINUE
  UU = 0.5*(UU+UU1)
  VV = 0.5*(VV+VV1)
  160 IF (IB .NE. 0) GO TO 170
  GO TO 175
165 HMI = HM
  X1 = SORT(UU1*UU1+VV1*VV1)
  LINE = 8
  IF (MCRV .GT. 0) GO TO 166
  WRITE (XOIFIL,2000) L,UX
  WRITE (XOIFIL,2001) IB,XO,YO,UU1,VV1,XD,X1,T,T,HMI
166 CONTINUE
  IB = IB+1
  170 IF (UU) 173,171,173
  171 IF (VV) 173,172,173
  172 UU = UUL
  VV = VVL
  173 X1 = SGRT(UU*UU+VV*VV)
  UUL = UU
  VVL = VV
  DT = DX/X1
  XO = XO+DT*UU
  YO = YO+DT*VV
  IF (XO.LT.X(1).OR.XO.GT.X(NX).OR.YO.LT.Y(1).OR.YO.GT.Y(NY)) GO TO
1200
  T = T+DT

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H0819100  
H0819200  
H0819300  
H0819400  
H0819500  
H0819600  
H0819700  
H0819800  
H0819900  
H0820000  
H0820100  
H0820200  
H0820300  
H0820400  
H0820500  
H0820600  
H0820700  
H0820800  
H0820900  
H0821000  
H0821100  
H0821200  
H0821300  
H0821400  
H0821500  
H0821600  
H0821700  
H0821800  
H0821900  
H0822000  
H0822100  
H0822200  
H0822300  
H0822400  
H0822500  
H0822600  
H0822700  
H0822800

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191* XU = XD+DX
192* 175 IF (X0 .GE. X(N2),AND,X0 .LE. X(N2+1)) GO TO 177
193* N2 = NX-1
194* 176 IF (X0 .GE. X(N2)) GO TO 177
195* N2 = N2-1
196* IF (N2 .GT. 1) GO TO 176
197* 177 IF (Y0 .GE. Y(K2),AND,Y0 .LE. Y(K2+1)) GO TO 179
198* K2 = NY-1
199* 178 IF (Y0 .GE. Y(K2)) GO TO 179
200* K2 = K2-1
201* IF (K2 .GT. 1) GO TO 178
202* 179 XP = (X0-X(N2))/(X(N2+1)-X(N2))
203* YP = (Y0-Y(K2))/(Y(K2+1)-Y(K2))
204* HM = (1.0-XP)*(1.0-YP)*P(N2,K2)+XP*(1.0-YP)*P(N2+1,K2)+
205* 1(1.0-XP)*YP*P(N2,K2+1)+XP*YP*P(N2+1,K2+1)
206* IF (Ib .EQ. 0) GO TO 165
207* HMI = 0.5*(HM+HMI)
208* IF (MCRV .GT. 0) GO TO 181
209* LINE = LINE+1
210* IF (LINE .LT. 57) GO TO 180
211* LINE = 8
212* WRITE (XOTFIL,2000) L,DX
213* 180 WRITE (XOTFIL,2001) Ib,X0,Y0,UU,VV,XD,X1,DT,I,HMI
214* 181 CONTINUE
215* HMI = HM
216* XP = (X0-X(1))*SCLX
217* YP = (Y0-Y(1))*SCLY
218* CALL PLOT(XP,YP,2)
219* IF (MOD(Ib,5) .NE. 0) GO TO 190
220* S1 = HXM/X1
221* S2 = -S1*UU*SCLY
222* S1 = S1*VV*SCLX
223* CALL PLOT(XP-S1,YP-S2,2)
224* CALL PLOT(XP+S1,YP+S2,2)
225* CALL PLOT(XP,YP,2)
226* 190 CONTINUE
227* U1 = U1+UU
228* V1 = V1+VV

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229*      U2 = U2+ABS(UU)
230*      V2 = V2+ABS(VV)
231*      S1 = U1*U1+V1*V1
232*      S2 = U2*U2+V2*V2
233*      IF (S2/S1 .GE. 49.0) GO TO 200
234*      195 CONTINUE
235*      IP = IB+1
236*      IF (IP .LT. 1000) GO TO 60
237*      200 CONTINUE
238*      RETURN
239*      2000 FORMAT ('1',4I,X,'TRAJECTORY NUMBER ',12,' ',DELTA-X =',F9.3,' METER
240*      15,'/' POINT',5X,'X',11X,'Y',9X,'U',7X,'V',5X,'DISTANCE VELOCITY (M/SEC) (METERS) (M/SEC) (METERS)
241*      2DELTA-T TIME HRS,'/' NUMBER (METERS) (SEC) (METERS),/1X,46('---')
242*      3M/SEC) (METERS) (M/SEC) (SEC)
243*      4)
244*      2001 FORMAT (2X,14,2F12.2,2F8.2,F10.2,2F9.2,F10.2,F9.2)
245*      END

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H0822900
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SUBROUTINE HEC009(X,Y,ZZ,IDIM,JDIM,CONT,NCONT,SCL,LFL,NSW,Z,IFL)
THIS SUBROUTINE DRAWS ALL CONTOUR PLOTS
COMMON /M1/ S(124)
COMMON /DTA1/ J1,J2,J3,J4,J5,J6,J7,J8,J9,J10,J11,J12,J13,RAD,MAXLL
1,XM,YM,MFLGS,SCLX,SCLY,XNCH,YNCH,J14,J15,J16,ISW7,IPL0T,MCORE
DIMENSION X(IDIM),Y(JDIM),ZZ(IDIM,1),Z(11,11),IFL(10,10),U(11),
1V(11),ZA(4,2),ZB(5),ZAB(2,3),ZX(2),ZY(2),CONT(NCONT),
2LFL(IDIM,NCONT)
EQUIVALENCE (J1,LXM2),(J2,LYM2),(J3,XMID),(J4,YMID),(J5,XD),
1(J6,YD),(J7,NSUBY),(J10,DV1),(J11,DV),(J12,NSUBY1),(J13,YJJ1),
2(J14,IYM2),(J15,IYM3),(J16,IYML)
EQUIVALENCE (S(1),V),(S(12),U),(S(23),ZA),(S(31),ZB),(S(36),ZAB),
1(S(42),ZX),(S(44),ZY),(S(46),ZXY),(S(48),P00),(S(49),P01),
2(S(50),P10),(S(51),P11),(S(52),SW),(S(53),W2),(S(54),W3),
3(S(55),WX2),(S(56),WX3),(S(57),IYML1),(S(58),IX6),(S(59),NSUBX),
4(S(60),DU1),(S(61),DU),(S(62),NSUBX1),(S(63),XI1),(S(64),IXM1),
5(S(65),IXML),(S(66),Y3),(S(67),Y4),(S(68),E3),(S(69),B3SQ),
6(S(70),X3),(S(71),ZB3),(S(72),A3),(S(73),A3SQ),(S(74),X4),
7(S(75),Z43),(S(76),A4),(S(77),X5),(S(78),Z54),(S(79),Z54),
8(S(80),Z5B1),(S(81),Z5B2),(S(82),Z5B3),(S(83),Z5B4),(S(84),Z5B5),
9(S(85),X6),(S(86),Z63),(S(87),Z64),(S(88),Z6B3),(S(89),Z62)
EQUIVALENCE (S(90),Z6B2),(S(91),Z6B4),(S(92),Z65),(S(93),Z6B1),
1(S(94),Z6B5),(S(95),A5),(S(96),ZA5B2),(S(97),ZA5B3),(S(98),ZA5B4),
2(S(99),ZX34),(S(100),ZY34),(S(101),ZXY34),(S(102),SW1),
3(S(103),ZX3B3),(S(104),ZX4B3),(S(105),ZY3A3),(S(106),ZY4A3),
4(S(107),P30),(S(108),P31),(S(109),P32),(S(110),P33),(S(111),DY),
5(S(112),DX),(S(113),I2),(S(114),J),(S(115),I),(S(116),I1),
6(S(117),KFL),(S(118),JFL),(S(119),X2),(S(120),Y2),(S(121),X1),
7(S(122),Y1),(S(123),TEMP),(S(124),FPN)
EQUIVALENCE (Z3A2,ZA(1)),(Z3A3,ZA(2)),(Z3A4,ZA(3)),(Z3A5,ZA(4)),
1(Z4A2,ZA(5)),(Z4A3,ZA(6)),(Z4A4,ZA(7)),(Z4A5,ZA(8)),(Z4B1,ZB(1)),
2(Z4B2,ZB(2)),(Z4B3,ZB(3)),(Z4B4,ZB(4)),(Z4B5,ZB(5)),(Z4B2,ZAB(1)),
3(Z4B2,ZAB(2)),(Z4B3,ZAB(3)),(Z4B3,ZAB(4)),(Z4B3,ZAB(5)),
4(Z4B4,ZAB(6)),(Z4B3,ZX(1)),(Z4B4,ZX(2)),(Z4B3,ZY(1)),(Z4B4,ZY(2)),
5(Z4B3,ZXY(1)),(Z4B4,ZXY(2)),(P00,Z33),(P01,ZY33),(P10,ZX33),
6(P11,ZXY33)
EQUIVALENCE (SW,E),(W2,WY2,A,Q0),(W3,WY3,B,Q1),(WX2,C,Q2),(WX3,D,
1Q3),(Z3A2,P02),(Z4A2,F03),(Z4B1,P12),(Z4B2,P13),(Z4B4,P20),(Z4B5,
H0900100
H0900200
H0900300
H0900400
H0900500
H0900600
H0900700
H0900800
H0900900
H0901000
H0901100
H0901200
H0901300
H0901400
H0901500
H0901600
H0901700
H0901800
H0901900
H0902000
H0902100
H0902200
H0902300
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H0902500
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H0903100
H0903200
H0903300
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H0903600
H0903700
H0903800

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39* 2P21),(ZA3B2,P22),(ZA3B4,P23)
40* LXM2 = IDIM-2
41* LYM2 = JDIM-2
42* DO 40 J=1,NCONT
43* DO 40 I=1,IDIM
44* 40 LFL(I,J) = 0
45* XMID = 0.5*(X(IDIM)+X(1))
46* YMID = 0.5*(Y(JDIM)+Y(1))
47* XD = (X(IDIM)-X(1))*SCL*0.5
48* YD = (Y(JDIM)-Y(1))*SCL*0.5
49*
50* C MAIN DO LOOP OVER INPUT DATA GRID
51* C
52* C
53* DO 1200 JJ=2,JDIM
54* NSUBY = 6
55* DV1 = (Y(JJ)-Y(JJ-1))*0.2
56* DV = DV1*SCL
57* IF (DV.LE. 0.05) GO TO 70
58* NSUBY = DV*100.0+1.5
59* IF (NSUBY.GT. 11) NSUBY = 11
60* DV1 = (Y(JJ)-Y(JJ-1))/(NSUBY-1)
61* DV = DV1*SCL
62* 70 NSUBY1 = NSUBY-1
63* YJJ1 = (Y(JJ-1)-YMID)*SCL
64* DO 110 J=1,NSUBY
65* 110 V(J) = YJJ1+(J-1)*DV
66* IYM2 = JJ-2
67* IYM3 = IYM2-1
68* IYML = JJ-JDIM
69* IYML1 = IYML+1
70* IX6 = 0
71* C MAIN DO LOOP OVER INPUT DATA GRID
72* C
73* C
74* DO 1250 II=1,IDIM
75* IF (II.EQ. 1) GO TO 130
76* NSUBX = 6
77* DU1 = (X(II)-X(II-1))*0.2

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DU = DU1*SCL
IF (DU .LE. 0.05) GO TO 117
NSUBX = DU*100.0+1.5
IF (NSUBX .GT. 11) NSUBX = 11
DU1 = (X(II)-X(II-1))/(NSUBX-1)
DU = DU1*SCL
117 NSUBX1 = NSUBX-1
X111 = (X(II-1)-X(MID))*SCL
CALL PLOT(X111+XD,YJJ1+YD,3)
CALL PLOT(X111+XD,YJJ1+YD,2)
DO 120 I=1,NSUBX
120 U(I) = X111+(I-1)*DU
150 CONTINUE
IXM1 = II-1
IXML = II-IDIM
IF (IXM1 .NE. 0) GO TO 150
Y3 = Y(JJ-1)
Y4 = Y(JJ)
B3 = 1.0/(Y4-Y3)
B3SQ = B3*B3
IF (IYM2 .GT. 0) B2 = 1.0/(Y3-Y(IYM2))
IF (IYM3 .GT. 0) B1 = 1.0/(Y(IYM2)-Y(IYM3))
IF (IYML .LT. 0) B4 = 1.0/(Y(JJ+1)-Y4)
IF (IYML1 .LT. 0) B5 = 1.0/(Y(JJ+2)-Y(JJ+1))
GO TO 180
150 Z3A2 = Z3A3
Z4A2 = Z4A3
X3 = X4
Z33 = Z43
Z3B3 = Z4B3
A3 = A4
A3SQ = A3*A3
Z3A3 = Z3A4
Z4A3 = Z4A4
ZA3B2 = ZA4B2
ZA3B3 = ZA4B3
ZA3B4 = ZA4B4
160 X4 = X5

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H0907800  
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H0908800  
H0908900  
H0909000  
H0909100  
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H0909300  
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H0910000  
H0910100  
H0910200  
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243 = 253  
24B1 = 25B1  
24B2 = 25B2  
24B3 = 25B3  
24B4 = 25B4  
24B5 = 25B5  
A4 = A5  
23A4 = 23A5  
24A4 = 24A5  
24B2 = 24B3  
24B3 = 24B4  
24B4 = 24B5  
X5 = X6  
253 = 263  
254 = 264  
25B1 = 26B1  
25B2 = 26B2  
25B3 = 26B3  
25B4 = 26B4  
25B5 = 26B5  
180 IX6 = IX6+1  
IF (IX6.GT. IDIM) GO TO 260  
X6 = X(IX6)  
263 = 22(IX6,JJ-1)  
264 = 22(IX6,JJ)  
26B3 = (264-263)\*B3  
IF (LYM2.EQ. 0) GO TO 200  
IF (LYM2.EQ. 0) GO TO 190  
262 = 22(IX6,JJ-2)  
26B2 = (263-262)\*B2  
IF (LYM1.NE. 0) GO TO 190  
26B4 = 26B3+26B3-26B2  
GO TO 210  
190 265 = 22(IX6,JJ+1)  
26B4 = (265-264)\*B4  
IF (LYM2.NE. 0) GO TO 210  
26B2 = 26B3+26B3-26B4  
GO TO 210

H0911500  
H0911600  
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H0912500  
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H0912700  
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153*	200	Z6B2 = Z6B3	H0915300
154*		Z6B4 = Z6B3	H0915400
155*	210	IF (IXM3 .LE. 0) GO TO 220	H0915500
156*		Z6B1 = (Z62-ZZ(IX6,JJ-3))*B1	H0915600
157*		GO TO 230	H0915700
158*	220	Z6B1 = Z6B2+Z6B2-Z6B3	H0915800
159*	230	IF (IXM1 .GE. 0) GO TO 240	H0915900
160*		Z6B5 = (ZZ(IX6,JJ+2)-Z65)*B5	H0916000
161*		GO TO 250	H0916100
162*	240	Z6B5 = Z6B4+Z6B4-Z6B3	H0916200
163*	250	IF (IX6 .EQ. 1) GO TO 170	H0916300
164*		A5 = 1.0/(X6-X5)	H0916400
165*		Z3A5 = (Z63-Z53)*A5	H0916500
166*		Z4A5 = (Z64-Z54)*A5	H0916600
167*		ZA5B2 = (Z6B2-Z5B2)*A5	H0916700
168*		ZA5B3 = (Z6B3-Z5B3)*A5	H0916800
169*		ZA5B4 = (Z6B4-Z5B4)*A5	H0916900
170*		IF (IX6 .EQ. 2) GO TO 160	H0917000
171*		GO TO 260	H0917100
172*	260	IF (LXM2 .EQ. 0) GO TO 270	H0917200
173*		Z3A5 = Z3A4+Z3A4-Z3A3	H0917300
174*		Z4A5 = Z4A4+Z4A4-Z4A3	H0917400
175*		IF (IXM1 .EQ. 0) GO TO 290	H0917500
176*		ZA5B2 = ZA4B2+ZA4B2-ZA3B2	H0917600
177*		ZA5B3 = ZA4B3+ZA4B3-ZA3B3	H0917700
178*		ZA5B4 = ZA4B4+ZA4B4-ZA3B4	H0917800
179*		GO TO 290	H0917900
180*	270	Z3A5 = Z3A4	H0918000
181*		Z4A5 = Z4A4	H0918100
182*		IF (IXM1 .EQ. 0) GO TO 290	H0918200
183*		ZA5B2 = ZA4B2	H0918300
184*		ZA5B3 = ZA4B3	H0918400
185*		ZA5B4 = ZA4B4	H0918500
186*	280	IF (IXM1 .NE. 0) GO TO 290	H0918600
187*		Z3A2 = Z3A4+Z3A4-Z3A5	H0918700
188*		Z3A2 = Z3A3+Z3A3-Z3A4	H0918800
189*		Z4A3 = Z4A4+Z4A4-Z4A5	H0918900
190*		Z4A2 = Z4A3+Z4A3-Z4A4	H0919000



191*	ZA3B2 = ZA4B2+ZA4B2-ZA5B2	H0919100
192*	ZA3B3 = ZA4B3+ZA4B3-ZA5B3	H0919200
193*	ZA3B4 = ZA4B4+ZA4B4-ZA5B4	H0919300
194*	GO TO 300	H0919400
195*	290 ZX33 = ZX43	H0919500
196*	ZX34 = ZX44	H0919600
197*	ZY33 = ZY43	H0919700
198*	ZY34 = ZY44	H0919800
199*	ZXY33 = ZXY43	H0919900
200*	ZXY34 = ZXY44	H0920000
201*	300 DO 350 JY=1,2	H0920100
202*	W2 = ABS(ZA(4,JY)-ZA(3,JY))	H0920200
203*	W3 = ABS(ZA(2,JY)-ZA(1,JY))	H0920300
204*	SW = W2+W3	H0920400
205*	IF (SW) 310,310,305	H0920500
206*	305 SW1 = 1.0/SW	H0920600
207*	WX2 = W2*SW1	H0920700
208*	WX3 = W3*SW1	H0920800
209*	GO TO 320	H0920900
210*	310 WX2 = 0.5	H0921000
211*	WX3 = 0.5	H0921100
212*	320 ZX(JY) = WX2*ZA(2,JY)+WX3*ZA(3,JY)	H0921200
213*	W2 = ABS(ZB(JY+3)-ZB(JY+2))	H0921300
214*	W3 = ABS(ZB(JY+1)-ZB(JY))	H0921400
215*	SW = W2+W3	H0921500
216*	IF (SW) 330,330,325	H0921600
217*	325 SW1 = 1.0/SW	H0921700
218*	WY2 = W2*SW1	H0921800
219*	WY3 = W3*SW1	H0921900
220*	GO TO 340	H0922000
221*	330 WY2 = 0.5	H0922100
222*	WY3 = 0.5	H0922200
223*	340 ZY(JY) = WY2*ZB(JY+1)+WY3*ZB(JY+2)	H0922300
224*	ZXY(JY) = WY2*(WX2*ZAB(1,JY)+WX3*ZAB(2,JY))+WY3*(WX2*ZAB(1,JY+1)+	H0922400
225*	1*WX3*ZAB(2,JY+1))	H0922500
226*	350 CONTINUE	H0922600
227*	IF (IXM1 .EQ. 0) GO TO 1250	H0922700
228*	ZX3B3 = (ZX34-ZX33)*B3	H0922800

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ZX4B3 = (ZX44-ZX43)\*B3  
ZY3A3 = (ZY43-ZY33)\*A3  
ZY4A3 = (ZY44-ZY34)\*A3  
A = ZA3B3-ZX3B3-ZY3A3+ZY33  
B = ZX4B3-ZX3B3-ZX4Y43+ZY33  
C = ZY4A3-ZY3A3-ZX4Y34+ZY33  
D = ZY44-ZX4Y43-ZX4Y34+ZY33  
E = A+A-B-C  
P02 = (2.0\*(Z3B3-ZY33)+Z3B3-ZY34)\*B3  
P03 = (-2.0\*Z3B3+ZY34+ZY33)\*B3SQ  
P12 = (2.0\*(ZX3B3-ZX4Y33)+ZX3B3-ZX4Y34)\*B3  
P13 = (-2.0\*ZX3B3+ZY34+ZY33)\*B3SQ  
P20 = (2.0\*(Z3A3-ZX33)+Z3A3-ZX43)\*A3  
P21 = (2.0\*(ZY3A3-ZX4Y33)+ZY3A3-ZX4Y34)\*A3  
P22 = (3.0\*(A+E)+D)\*A3\*B3  
P23 = (-3.0\*E-B-D)\*A3\*B3SQ  
P30 = (-2.0\*Z3A3+ZX4Y33+ZX33)\*A3SQ  
P31 = (-2.0\*ZY3A3+ZX4Y33+ZX4Y34)\*A3SQ  
P32 = (-3.0\*E-C-D)\*B3\*A3SQ  
P33 = (D+E)\*A3SQ\*B3SQ  
DO 370 JY=1,NSUBY  
DY = (JY-1)\*DU1  
Q0 = P00+DY\*(P01+DY\*(P02+DY\*(P03)))  
Q1 = P10+DY\*(P11+DY\*(P12+DY\*(P13)))  
Q2 = P20+DY\*(P21+DY\*(P22+DY\*(P23)))  
Q3 = P30+DY\*(P31+DY\*(P32+DY\*(P33)))  
DO 360 JX=1,NSUBX  
DX = (JX-1)\*DU1  
Z(JX,JY) = Q0+DX\*(Q1+DX\*(Q2+DX\*(Q3)))  
360 CONTINUE  
370 CONTINUE  
380 CONTINUE  
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DO LOOP OVER CONTOUR (ISOPLETH) VALUES  
DO 1240 K=1,NCONT  
DO 390 J=1,NSUBY1  
DO 390 I=1,NSUBX1

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H0926500  
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H0930000  
H0930100  
H0930200  
H0930300  
H0930400

305*	1060	IF ((Z(I,J+1)-C)*(Z(I+1,J+1)-C) .GT. 0.0) GO TO 1070	H0930500
306*		X2 = Z(I,J+1)-Z(I+1,J+1)	H0930600
307*		IF (X2) 1062,1061,1062	H0930700
308*	1061	X2 = 1.0	H0930800
309*		GO TO 1063	H0930900
310*	1062	X2 = (Z(I,J+1)-C)/X2	H0931000
311*	1063	X2 = U(I)+DU*X2	H0931100
312*		Y2 = V(J+1)	H0931200
313*		IF (I1.NE. 0) GO TO 1130	H0931300
314*		X1 = X2	H0931400
315*		Y1 = Y2	H0931500
316*		I1 = 3	H0931600
317*	1070	IF (I1.EQ. 0) GO TO 1190	H0931700
318*	1080	IF ((Z(I+1,J)-C)*(Z(I+1,J+1)-C) .GT. 0.0) GO TO 1040	H0931800
319*		X2 = U(I+1)	H0931900
320*		Y2 = Z(I+1,J)-Z(I+1,J+1)	H0932000
321*		IF (Y2) 1082,1081,1082	H0932100
322*	1081	Y2 = 1.0	H0932200
323*		GO TO 1083	H0932300
324*	1082	Y2 = (Z(I+1,J)-C)/Y2	H0932400
325*	1083	Y2 = V(J)+DV*Y2	H0932500
326*		GO TO 1140	H0932600
327*	1115	IFL(I,J) = 1	H0932700
328*	1117	IF (J.EQ. 1) GO TO 1150	H0932800
329*		IF (IFL(I,J-1) .NE. 0) GO TO 1150	H0932900
330*		J = J-1	H0933000
331*		IF (KFL .NE. 0) GO TO 1118	H0933100
332*		KFL = 1	H0933200
333*		CALL PLOT(X1+XD,Y1+YD,3)	H0933300
334*	1118	CALL PLOT(X2+XD,Y2+YD,2)	H0933400
335*		I1 = 3	H0933500
336*		JFL = 0	H0933600
337*		X1 = X2	H0933700
338*		Y1 = Y2	H0933800
339*		GO TO 1080	H0933900
340*	1120	IFL(I,J) = 1	H0934000
341*	1125	IF (I.EQ. 1) GO TO 1150	H0934100
342*		IF (IFL(I-1,J) .NE. 0) GO TO 1150	H0934200



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H0934400  
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H0936400  
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H0937600  
H0937700  
H0937800  
H0937900  
H0938000

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I = I-1
IF (KFL .NE. 0) GO TO 1127
KFL = 1
CALL PLOT(X1+XD,Y1+YD,3)
1127 CALL PLOT(X2+XD,Y2+YD,2)
I1 = 4
JFL = 0
X1 = X2
Y1 = Y2
GO TO 1040
1130 IFL(I,J) = 1
1135 IF (J.EQ. NSUBX1) GO TO 1150
IF (IFL(I,J+1) .NE. 0) GO TO 1150
J = J+1
IF (KFL .NE. 0) GO TO 1137
KFL = 1
CALL PLOT(X1+XD,Y1+YD,3)
1137 CALL PLOT(X2+XD,Y2+YD,2)
I1 = 1
JFL = 0
X1 = X2
Y1 = Y2
GO TO 1050
1140 IFL(I,J) = 1
1145 IF (I.EQ. NSUBX1) GO TO 1150
IF (IFL(I+1,J) .NE. 0) GO TO 1150
I = I+1
IF (KFL .NE. 0) GO TO 1147
KFL = 1
CALL PLOT(X1+XD,Y1+YD,3)
1147 CALL PLOT(X2+XD,Y2+YD,2)
I1 = 2
JFL = 0
X1 = X2
Y1 = Y2
GO TO 1060
1150 IF (JFL .NE. 0) GO TO 1160
JFL = 1

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TEMP = X1
X1 = X2
X2 = TEMP
TEMP = Y1
Y1 = Y2
Y2 = TEMP
GO TO (1117,1125,1135,1145),I1
1160 IF (KFL.EQ. 0) CALL PLOT(X2+XD,Y2+YD,3)
CALL PLOT(X1+XD,Y1+YD,2)
I2 = 1
1190 CONTINUE
1200 CONTINUE
IF (LFL(II,K)+LFL(II-1,K) .NE. 0) GO TO 1230
IF (I2 .EQ. 0) GO TO 1230
FPN = K
CALL NUMBER(X2+XD,Y2+YD,0.05,FPN,0.0,-1)
1230 LFL(II,K) = I2
1240 CONTINUE
1250 CONTINUE
1260 CONTINUE
Y1 = -0.9
Y2 = 0.0
IF (NSW .NE. 0) GO TO 1300
X1 = 0.5*(XD-1.8)
CALL HEC014(X1,Y1,.075,24HTERRAIN ELEVATION LEVELS,0.0,24)
GO TO 1321
1300 IF (NSW .LT. 0) GO TO 1310
X1 = 0.5*(XD-1.35)+XD
CALL HEC014(X1,Y1,.075,18HLAYER DEPTH LEVELS,0.0,18)
GO TO 1320
1310 X1 = 0.5*(XD-1.65)+XD
CALL HEC014(X1,Y1,.075,22HLAYER ELEVATION LEVELS,0.0,22)
1320 Y2 = XD
1321 CONTINUE
Y1 = -1.0
X1 = 0.5*(XD-2.7)-0.9+Y2
J = 0
I = 0

```

H0938100  
H0938200  
H0938300  
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H0939900  
H0940000  
H0940100  
H0940200  
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H0941100  
H0941200  
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H0941400  
H0941500  
H0941600  
H0941700  
H0941800

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1330 J = J+1  
IF (J.GT. NCONT) GO TO 1350  
I = I+1  
X1 = X1+0.9  
IF (I.LT. 4) GO TO 1340  
I = 1  
X1 = 0.5\*(XD-2.7)+Y2  
Y1 = Y1-0.1  
1340 X2 = J  
CALL NUMBER(X1,Y1,.075,X2,0.0,-1)  
CALL HEC014(X1+0.15,Y1,.075,1H,0.0,1)  
CALL NUMBER(X1+0.225,Y1,.075,CONT(J),0.0,1)  
CALL HEC014(X1+0.75,Y1,.075,2H, 0.0,2)  
GO TO 1330  
1350 CONTINUE  
RETURN  
END

H0941900  
H0942000  
H0942100  
H0942200  
H0942300  
H0942400  
H0942500  
H0942600  
H0942700  
H0942800  
H0942900  
H0943000  
H0943100  
H0943200  
H0943300  
H0943400  
H0943500

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SUBROUTINE HEC013(XM,YM,IFST)
C* C THIS SUBROUTINE IS THE WSMR VERSION, LOOK AT /UOFU FOR U OF U
C* C VERSION - DO NOT INCLUDE IN U OF U COLLECTION
IF (IFST.NE. 0) GO TO 10
IFST = 1
CALL INITAL(1,400,36,0,0,0)
CALL HEC014(-1,0,4,0,0,0,2,24)HSTART PLOTS FOR CHIMSTEDE,90.0,24)
CALL HEC014(-0,5,3,0,0,2,32)HROOM 203, BLDG 1622, PH 678-3123,90.0,
132)
10 CALL PLOT(1,5,3,0,-3)
CALL HEC016(0)
RETURN
END

H1300100
H1300200
H1300300
H1300400
H1300500
H1300600
H1300700
H1300800
H1300900
H1301000
H1301100
H1301200
H1301300

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H1400100  
H1400200  
H1400300  
H1400400  
H1400500  
H1400600

SUBROUTINE HEC014(X,Y,H,A,T,N)  
THIS SUBROUTINE IS THE WSMR VERSION, LOOK AT /UOFU FOR U OF U  
VERSION - DO NOT INCLUDE IN U OF U COLLECTION  
CALL SYMBOL(X,Y,H,A,T,N)  
RETURN  
END

1\*  
2\*  
3\*  
4\*  
5\*  
6\*

H1500100  
H1500200  
H1500300  
H1500400  
H1500500  
H1500600  
H1500700  
H1500800  
H1500900  
H1501000  
H1501100

SUBROUTINE HEC015(JSW,XM)  
C\* C THIS SUBROUTINE IS THE WSMR VERSION, LOOK AT /UOFU FOR U OF U  
C\* C VERSION - DO NOT INCLUDE IN U OF U COLLECTION  
CALL RSTR(2)  
CALL PLOT(1.5,3.0,-3)  
IF (JSW.EQ. 0) GO TO 10  
CALL HEC014(0.0,3.0,0.3,12)END OF PLOTS,0.0,12)  
CALL RSTR(3)  
10 CONTINUE  
RETURN  
END

1\*  
2\*  
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5\*  
6\*  
7\*  
8\*  
9\*  
10\*  
11\*

H1600100  
H1600200  
H1600300  
H1600400  
H1600500  
H1600600

SUBROUTINE HEC016(N)  
C\* C\* C THIS SUBROUTINE IS THE WSMR VERSION, LOOK AT /UOFU FOR U OF U  
C\* C\* C VERSION - DO NOT INCLUDE IN U OF U COLLECTION  
CALL NEWPIN(N+1)  
RETURN  
END

1\*  
2\*  
3\*  
4\*  
5\*  
6\*

1\* SUBROUTINE DRMRD/WT  
2\* DRUM MASS STORAGE HANDLER CALLABLE BY FORTRAN  
3\* CALL SEQUENCE CALL DRMRD/WT(N,IARRY,MPA,MPL,MAD,FN)  
4\* N=NO. OF 36 BIT WORDS TO TRANSFERE  
5\* IARRY STARTING ADDRESS OF DATA  
6\* STARTING DRUM ADDRESS=MPA\*MPL+MAD  
7\* FN=DRUM FILE NAME AS ON USE CARD  
8\*  
9\* RESTRICTIONS  
10\* MAX WORDS TRANSFERED 2\*\*16-1  
11\* MAX DRUM ADDRESS 2\*\*24-1  
12\* MAX FN 99999  
13\*  
14\* COMMENTS  
15\* DRUM ADDRESSING STARTS AT ZERO WHILE FORTRAN STARTS AT ONE  
16\* SUBROUTINE FSTRD/WT  
17\* FASTRAN MASS STORAGE HANDLER CALLABLE BY FORTRAN  
18\* FOR CALLING SEQUENCE AND RESTRICTIONS SEE DRMRD/WT AND SUBSTITUTE 'DISK' FOR  
19\* 'DRUM'.  
20\*  
21\* ADDITIONAL COMMENTS  
22\* THE SMALLEST ADDRESSABLE GRANULE IS 28 36 BIT WORDS  
23\* THEREFORE THE DISK ADDRESS MPA\*MPL+MAD MUST BE A MULTIPLE OF 28  
24\* DISK ADDRESS ZERO REFERS TO THE FIRST 28 WORDS  
25\* THIS MOD(26) FEATURE MUST BE HANDLED BY THE USER  
26\*  
27\* BY DCP  
28\* START 8/28/74  
29\* VERSION 1.01 9/3/74  
30\* AXRS  
31\*  
32\* FSTWT\* L A0,WRITE  
33\* J 3+2  
34\* FSTRD\* L A0,READ  
35\* L A1,F  
36\* L A2,(+'FST')  
37\* J FUNCT  
38\* L A0,WRITE  
39\* J 3+2  
40\* L A0,READ  
41\* L A1,D  
42\* L A2,(+'DRM')  
43\* S A1,DEVICE  
44\*  
45\* FUNCT





```

77*      JZ      A0,5+3      . CHECK IF DONE
78*      DSL     A0,36
79*      J       AGAIN
80*      SSL     A2,6
81*      A       A2,DEVICE
82*      S       A2,10
83*      L       A0,(PF 01000,1,ERROR) . THIS COMPLETES I/O PACKET WITH FILENAME
84*      ER      LALL$      . TELL EXEC-8 IF CONTINGENCY ERROR
85*      LU      A0,10
86*      ER      IOW$
87*      L,S1     A0,10+3
88*      JZ      A0,RETURN
89*      LU      A5,0
90*      TE,U    A0,022
91*      J       $+2
92*      LU      A5,1
93*      S,S2    A0,ERROR
94*      J       $+3
95*      +0      . PROVIDE SPACE FOR CONTINGENCY PACKET
96*      +0
97*      L
98*      SSL     A0,18
99*      LU      A2,6
100*     L       A1,BLANK
101*     DSL     A0,3
102*     SSL     A1,3
103*     A       A1,FIELD
104*     AN,U    A2,1
105*     JNZ     A2,TAG
106*     S,I3    A1,LINE2+3
107*     SSL     A1,12
108*     S,I3    A1,LINE4+3
109*     SSL     A1,12
110*     S,I3    A1,LINE3+3
111*     DL      A0,10
112*     DS      A0,LINE1+4
113*     L       A0,(PF 5,6,LINE1)
114*     ER      PRINT$

          ERROR

          TAG

          . CONVERT ERROR MESSAGE TO FIELD DATA
          . T1(A1)=ERROR TYPE
          . T2(A1)=ERROR CODE
          . T3(A1)=CONTINGENCY TYPE

```

115*	L	A0,(PF 1,4,LINE2)	
116*	ER	PRINT\$	
117*	L	A0,(PF 1,4,LINE3)	
118*	ER	PRINT\$	
119*	L	A0,(PF 1,4,LINE4)	
120*	ER	PRINT\$	
121*	JZ	A5,STOP	
122*	L	A0,(PF 1,3,EOF)	
123*	ER	PRINT\$	
124*	ER	EABT\$	
125*	J	7,X11	
126*	PF	FORM 12,6,18	
127*	WRITE	001000000000	
128*	READ	002000000000	
129*	FIELD	060000000000	
130*	DEVICE	RES 1	
131*	BLANK	,	
132*	F	01300000000000	
133*	U	01100000000000	
134*	TYPE	0010012000000	
135*	LINE1	'XXXRD/WT ERROR IN FILE	
136*	LINE2	' CONTINGENCY TYPE	000'
137*	LINE3	' ERROR TYPE	000'
138*	LINE4	' ERROR CODE	000'
139*	EOF	' *END OF FILE*	
140*	NTOBIG	' ERR IN XXXRD/WT N.GT. 2**16-1'	
141*	LTOBIG	' ERR IN XXXRD/WT START ADDRESS .GT. 2**24-1'	
142*	FNNOGD	' ERR IN XXXRD/WT FN OUT OF RANGE'	
143*	10	RES 6	
144*		END	

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